



Elettra Sincrotrone Trieste

On ESS LWU quadrupoles QC6 and QC7: DC and pulsed mode evaluation, magnet design and power supplies

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- ✓ ***Introduction***
- ✓ ***Basic parameters and specifications***
- ✓ ***Pre-design***
- ✓ ***Design***
- ✓ ***All models***
- ✓ ***Magnetic simulation***
- ✓ ***Power Supplies Considerations***
- ✓ ***Conclusions***

Based on the ESS report “*On the feasibility of pulsing the ESS LWU Quadrupoles*” (ESS-0019925), with the most updated requirements on the magnets, this presentation shows a comparison among potential magnet designs for the LWU QC6 and QC7 quadrupoles operated either with DC or pulsed excitation.

The goal is to obtain some information about the:

- 1. *Feasibility***
- 2. *Performance***
- 3. *Power consumption***
- 4. *Overall dimensions***
- 5. *Cost considerations***

Real basic requirements

| Parameters | | QC6 | QC7 | unit |
|------------------------------|-----------------------|-------------|-------------|------|
| Number of required quads | n | 95 | 12 | # |
| Maximum integrated gradient | IntG _{Max} | 2.3 | 2.9 | T |
| Range of integrated gradient | IntG _{range} | 1.20 - 2.20 | 0.85 - 2.70 | T |
| Minimum magnetic length | L _{eff} | 275 | 275 | mm |
| Minimum bore diameter | Ø | 112 | 112 | mm |
| Maximum overall length | L _{Overall} | 350 | 350 | mm |

QC6 and QC7 have the same dimension but different nominal ranges

QC7 have a wider range of use (lower and upper values), but...

...there are many more QC6 than QC7 (95 vs. 12)

How to merge the two quadrupole families into one?

In the pre-design we decided to **fix** common parameters **for all** the possible models:

1. The maximum current (DC) equal to the maximum RMS current (pulsed)
2. The max current density (DC) and the max RMS current density (pulsed)
3. The bore diameter and pole width (the poles geometry)
4. The yoke length and the overall length (the maximum thickness of the coils)

The values are:

- Maximum Power Supply (PS) current, DC or RMS = **150 A**
- Maximum **water** cooled current density = **4 A/mm²** (*at max PS Current, DC or RMS*)
- Maximum **air** cooled current density = **1.1 A/mm²** (*at max PC Current, DC or RMS*)
- Bore diameter = **112 mm** (*equal to the min requested in order to reduce the ampere-turns*)
- Poles width = **70 mm** (*equal to the GFR in order to reduce the frame dimensions*)
- Yoke length = **240 mm**
- Overall Length = **350 mm** (*equal to the max value requested*)

The desired current densities are achieved with the following copper conductors:

- Air cooled:



$$OD = \mathbf{6.30} \times 20 \text{ mm}^2 (125.1 \text{ mm}^2)$$

$$\text{If } I_{\text{RMS}} = \mathbf{150} \text{ A} \rightarrow \rho_{\text{RMS}} = \mathbf{1.19} \text{ A/mm}^2$$

$$\text{else if } \rho_{\text{RMS}} < 1.10 \text{ A/mm}^2 \rightarrow I_{\text{RMS}} < \mathbf{137.6} \text{ A}$$

- Water cooled



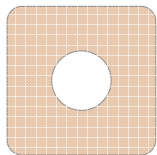
$$OD = \mathbf{6.35} \times 6.35 \text{ mm}^2 (32.3 \text{ mm}^2), ID = 3.15 \text{ mm}$$

$$\text{If } I_{\text{DC}} = \mathbf{150} \text{ A} \rightarrow \rho_{\text{DC}} = \mathbf{4.6} \text{ A/mm}^2$$

$$\text{else if } \rho_{\text{DC}} < 4.0 \text{ A/mm}^2 \rightarrow I_{\text{DC}} < \mathbf{129.2} \text{ A}$$

If we want to reduce the DC power, we must increase the conductor section, example:

- Water cooled



$$OD = 10.0 \times 10.0 \text{ mm}^2 (86.6 \text{ mm}^2), ID = 4.0 \text{ mm}$$

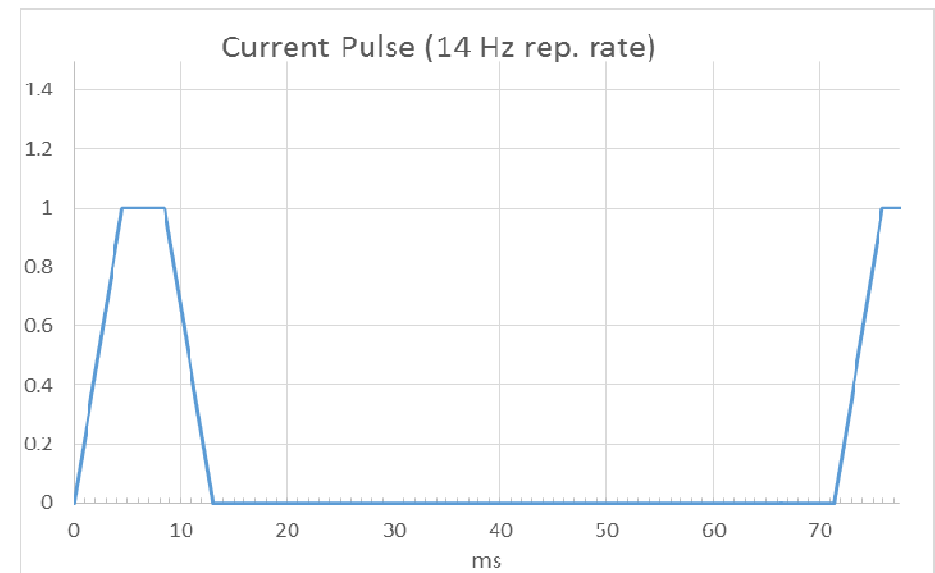
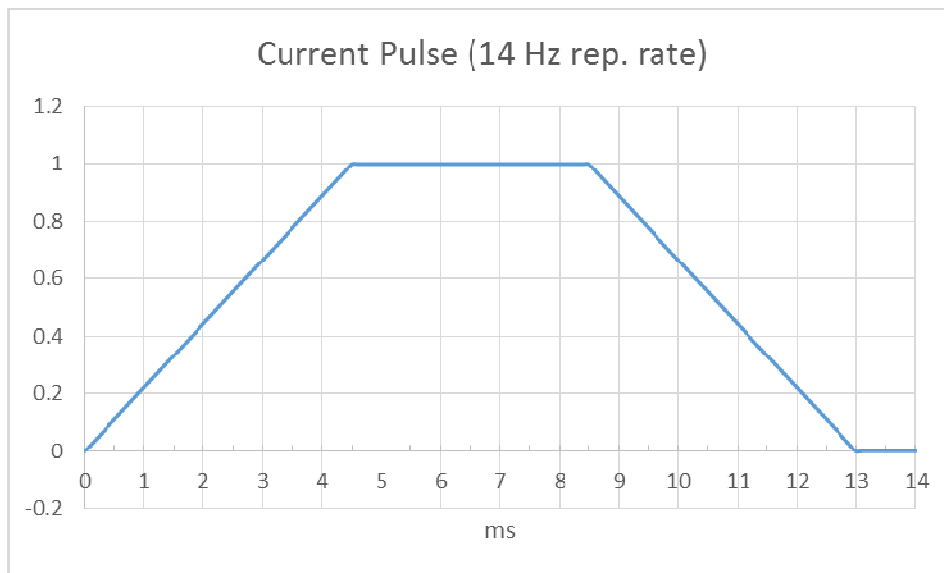
$$\text{If } I_{\text{DC}} = \mathbf{150} \text{ A} \rightarrow \rho_{\text{DC}} = \mathbf{1.7} \text{ A/mm}^2$$

$$\text{if } I_{\text{DC}} = \mathbf{129.2} \rightarrow \rho_{\text{DC}} = \mathbf{1.5} \text{ A/mm}^2$$

All the other parameters are calculated in the following excel sheets

For the pulsed excitation, two waveforms have been considered:

- Trapezoidal, 4.5 ms rise/fall, 4 ms flat-top, 14 Hz repetition rate (71.4 ms period)
- Trapezoidal, 8 ms rise/fall, 4 ms flat-top, 14 Hz repetition rate (71.4 ms period)

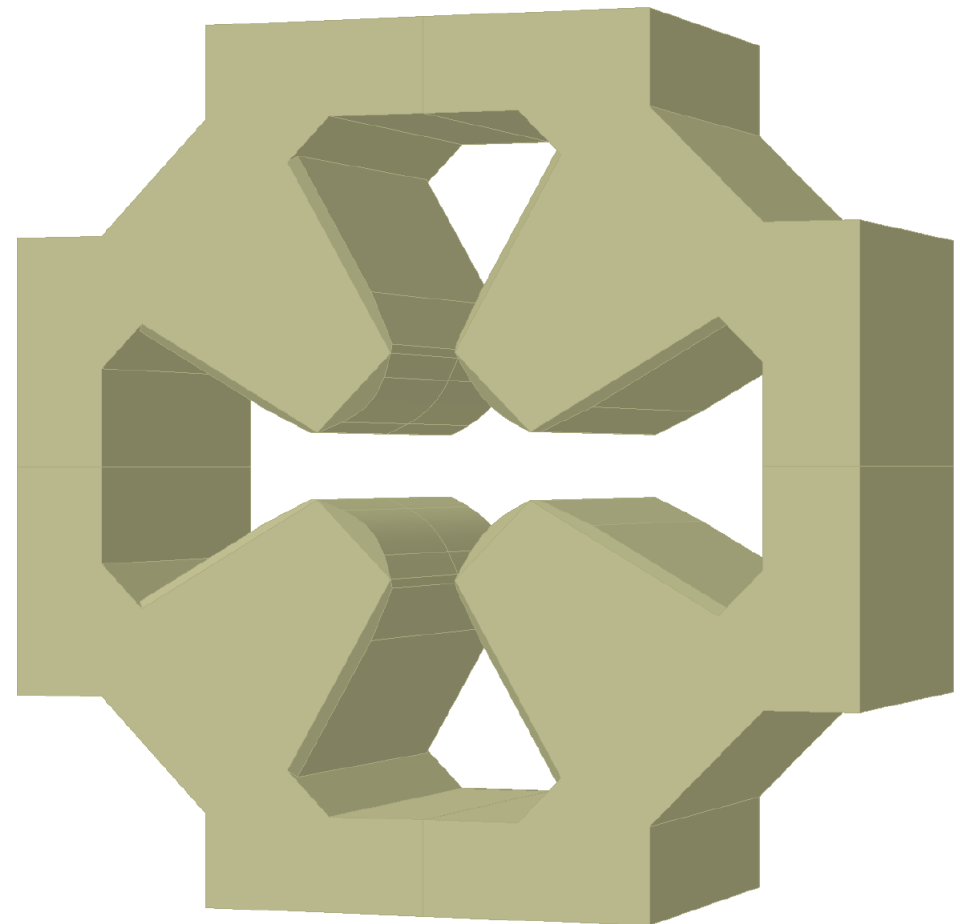
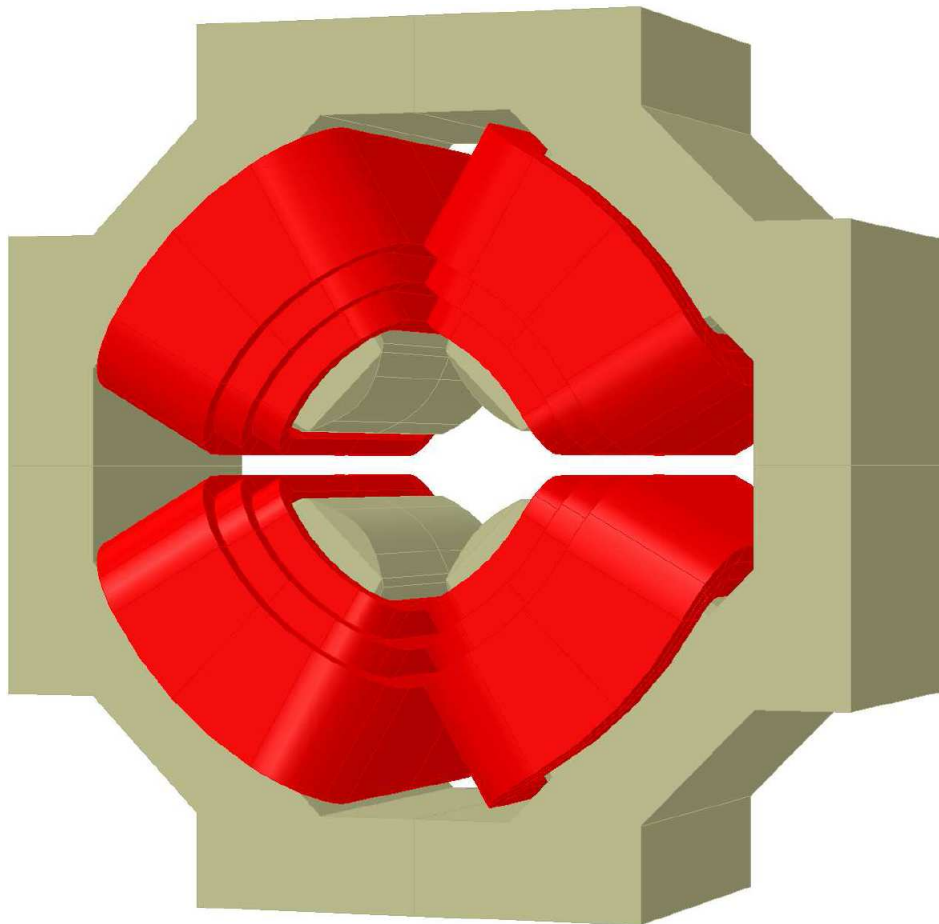


Current Pulse [4.5 – 4 – 4.5] ms

| | | | Pulsed | Pulsed | DC | DC | Pulsed | Pulsed | DC | DC | |
|-------------------------------------|---|--|--------|--------------------|-------|--------------------|--------|--------------------|--------|--------------------|---------------------|
| | | | QC6 | QC6 _{air} | QC6 | QC6 _{air} | QC7 | QC7 _{air} | QC7 | QC7 _{air} | unit |
| # of Quads | N | | 95 | 95 | 95 | 95 | 12 | 12 | 12 | 12 | |
| Expected total length | Z_{Tot} | | 350 | 350 | 350 | 350 | 350 | 350 | 350 | 350 | mm |
| Maximum Integrated Gradient | G_{Int} | | 2,30 | 2,30 | 2,30 | 2,30 | 2,90 | 2,90 | 2,90 | 2,90 | T |
| Maximum Nominal Integrated Gradient | G_{nom} | | 2,20 | 2,20 | 2,20 | 2,20 | 2,70 | 2,70 | 2,70 | 2,70 | T |
| Minimum Nominal Integrated Gradient | G_{NOM} | | 1,20 | 1,20 | 1,20 | 1,20 | 0,80 | 0,80 | 0,80 | 0,80 | T |
| Bore diameter | Ø | | 112 | 112 | 112 | 112 | 112 | 112 | 112 | 112 | mm |
| Pulse Frequency | Fr | | 14,0 | 14,0 | 14,0 | 14,0 | 14,0 | 14,0 | 14,0 | 14,0 | Hz |
| Pulse RiseTime | T_{up} | | 4,5 | 4,5 | 0,0 | 0,0 | 4,5 | 4,5 | 0,0 | 0,0 | msec |
| Pulse Flat TopTime | T_{flat} | | 4,0 | 4,0 | 71,4 | 71,4 | 4,0 | 4,0 | 71,4 | 71,4 | msec |
| Pulse Fall Time | T_{down} | | 4,5 | 4,5 | 0,0 | 0,0 | 4,5 | 4,5 | 0,0 | 0,0 | msec |
| Pulse RMS | I_{cRMS} | | 31,3 | 31,3 | 100,0 | 100,0 | 31,3 | 31,3 | 100,0 | 100,0 | % |
| Pole ampere-turns density | | | 0,36 | 0,36 | 0,36 | 0,36 | 0,46 | 0,46 | 0,46 | 0,46 | N-I/mm ² |
| Magnetic Length | L_{Mag} | | 275 | 275 | 275 | 275 | 275 | 275 | 275 | 275 | mm |
| Maximum Gradient | G_{Max} | | 8,364 | 8,364 | 8,364 | 8,364 | 10,545 | 10,545 | 10,545 | 10,545 | T/m |
| Field at pole tip radius | B_{Pole} | | 0,468 | 0,468 | 0,468 | 0,468 | 0,591 | 0,591 | 0,591 | 0,591 | T |
| Current-Turns (per Pole) + 0 % | N_{Tot} · I_{Coil} | | 10436 | 10436 | 10436 | 10436 | 13159 | 13159 | 13159 | 13159 | A-Turns |
| Turns per pole | N_{Tot} | | 24 | 24 | 78 | 78 | 30 | 30 | 96 | 96 | Turns |
| Number of turns for each layer | N_{L1} | | 10 | 5 | 18 | 14 | 12 | 6 | 21 | 17 | # |
| | N_{L2} | | 8 | 5 | 16 | 14 | 10 | 6 | 19 | 17 | # |
| | N_{L3} | | 6 | 4 | 14 | 13 | 8 | 5 | 17 | 16 | # |
| | N_{L4} | | 0 | 4 | 12 | 13 | 0 | 5 | 15 | 16 | # |
| | N_{L5} | | 0 | 3 | 10 | 12 | 0 | 4 | 13 | 15 | # |
| | N_{L6} | | 0 | 3 | 8 | 12 | 0 | 4 | 11 | 15 | # |
| Coils current at Max Int. Grad. | I_c | | 434,9 | 434,9 | 133,8 | 133,8 | 438,7 | 438,7 | 137,1 | 137,1 | A |
| RMS Coils current at Max Int. Grad. | I_{c RMS} | | 137 | 137 | 134 | 134 | 138 | 138 | 138 | 138 | A |

| | | | Pulsed | Pulsed | DC | DC | Pulsed | Pulsed | DC | DC | |
|---|-------------------------|--|--------|--------------------|--------|--------------------|--------|--------------------|--------|--------------------|-------------------|
| | | | QC6 | QC6 _{air} | QC6 | QC6 _{air} | QC7 | QC7 _{air} | QC7 | QC7 _{air} | unit |
| Conductor cross section width | W_{Cu} | | 6,35 | 6,30 | 6,35 | 6,30 | 6,35 | 6,30 | 6,35 | 6,30 | mm |
| Conductor cross section heigth | H_{Cu} | | 6,35 | 20,00 | 6,35 | 20,00 | 6,35 | 20,00 | 6,35 | 20,00 | mm |
| Conductor cross section dia bore | Ø_{Cu} | | 3,15 | 0,00 | 3,15 | 0,00 | 3,15 | 0,00 | 3,15 | 0,00 | mm |
| Conductor cross section smooth | r_{Cu} | | 0,500 | 0,500 | 0,500 | 0,500 | 0,500 | 0,500 | 0,500 | 0,500 | mm |
| Conductor cross section area | A_{Cu} | | 32,315 | 125,785 | 32,315 | 125,785 | 32,315 | 125,785 | 32,315 | 125,785 | mm ² |
| RMS current density = I _c / A _{Cu} | ρ_{Cu} | | 4,24 | 1,09 | 4,15 | 1,07 | 4,27 | 1,10 | 4,27 | 1,10 | A/mm ² |
| Conductor insulation thickness | T_{Cu} | | 1,00 | 1,00 | 0,20 | 0,20 | 1,00 | 1,00 | 0,20 | 0,20 | mm |
| Conductor cross section overall width | TW_{Cu} | | 7,35 | 7,30 | 6,55 | 6,50 | 7,35 | 7,30 | 6,55 | 6,50 | mm |
| Conductor cross section overall heigth | TH_{Cu} | | 7,35 | 21,00 | 6,55 | 20,20 | 7,35 | 21,00 | 6,55 | 20,20 | mm |
| Coil Heigth | H_{Coil} | | 73,5 | 504,0 | 117,9 | 282,8 | 88,2 | 126,0 | 137,6 | 343,4 | mm |
| Pole length | L_{Yoke} | | 240 | 240 | 240 | 240 | 240 | 240 | 240 | 240 | mm |
| Pole width (avg) | W_{Pole} | | 120 | 120 | 120 | 120 | 120 | 120 | 120 | 120 | mm |
| Coil inner straight length | L_{ci} | | 220 | 220 | 220 | 220 | 220 | 220 | 220 | 220 | mm |
| Coil inner width | W_{ci} | | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | mm |
| Single Coil conductor length | L_{Coil} | | 19,3 | 20,8 | 66,2 | 67,2 | 24,2 | 26,1 | 81,8 | 82,8 | m |
| Single Coil electric resistance at T _{ave} | R_{Coil} | | 10,30 | 2,88 | 36,52 | 9,30 | 12,95 | 3,61 | 45,77 | 11,46 | mΩ |
| Single Coil voltage drop at T _{ave} & I _c | V_{Coil} | | 4,48 | 1,25 | 4,89 | 1,24 | 5,68 | 1,58 | 6,27 | 1,57 | V |
| Magnet Inductance | L_H | | 8,2 | 8,2 | 0,0 | 0,0 | 10,3 | 10,3 | 0,0 | 0,0 | mH |
| Max Over Voltage L*dI/dt | V_{Rip} | | 792 | 792 | 0 | 0 | 1.004 | 1.004 | 0 | 0 | V |
| Overall Length | L_{Tot} | | 301,2 | 344,4 | 336,5 | 335,6 | 301,2 | 344,4 | 336,5 | 335,6 | mm |
| RMS Max PC current = I _c + 0 % | I_{PS} | | 136,1 | 136,1 | 133,8 | 133,8 | 137,3 | 137,3 | 137,1 | 137,1 | A |
| Magnet Power at I _{PS} and T _{ave} | P_{Mag} | | 0,76 | 0,21 | 2,62 | 0,67 | 0,98 | 0,27 | 3,44 | 0,86 | kW |

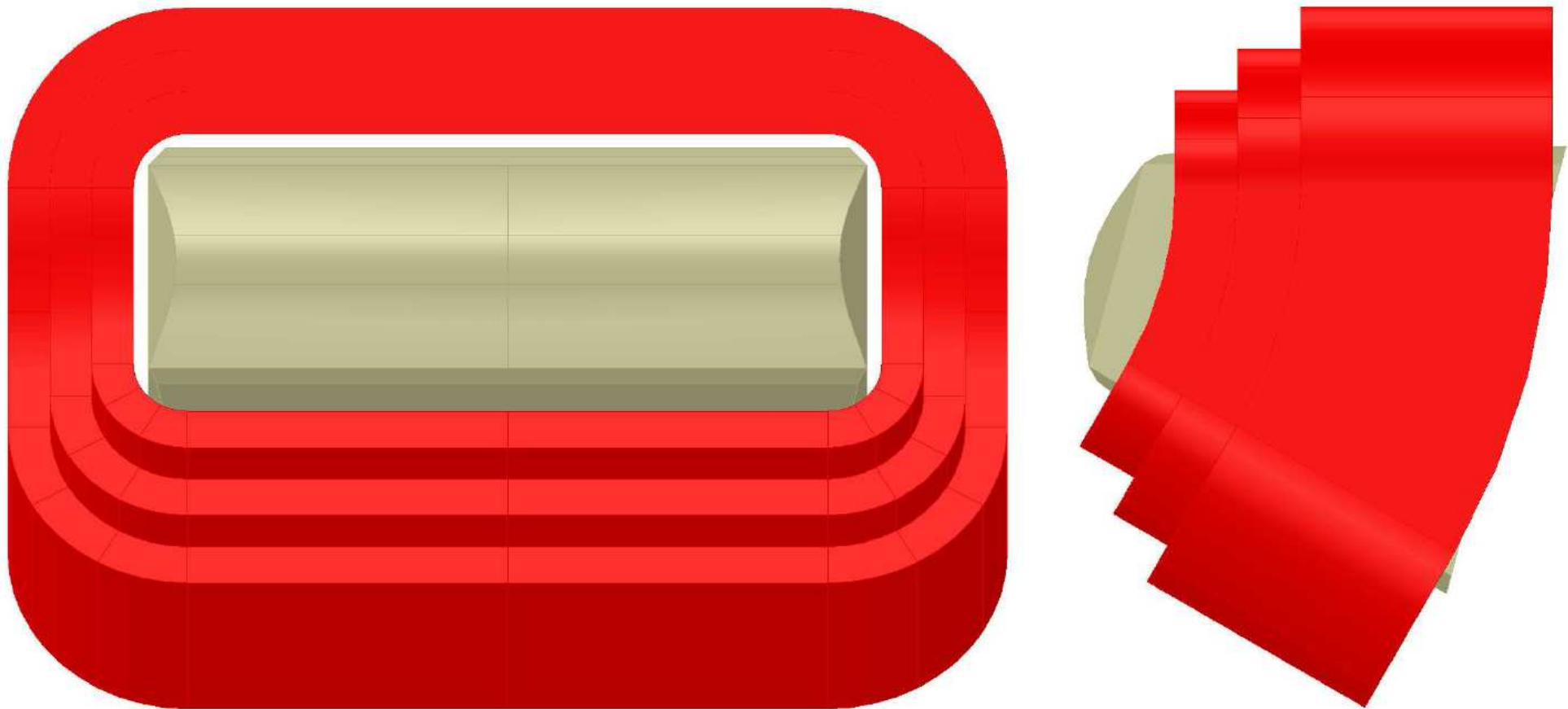
As the Good Field Region (GFR) is lower than the bore diameter, the idea is to use, for all the models, only one geometry of the pole profile, the width of the termination equals the diameter of the GFR. The coils are very close to the vacuum chamber and the frame is more compact.



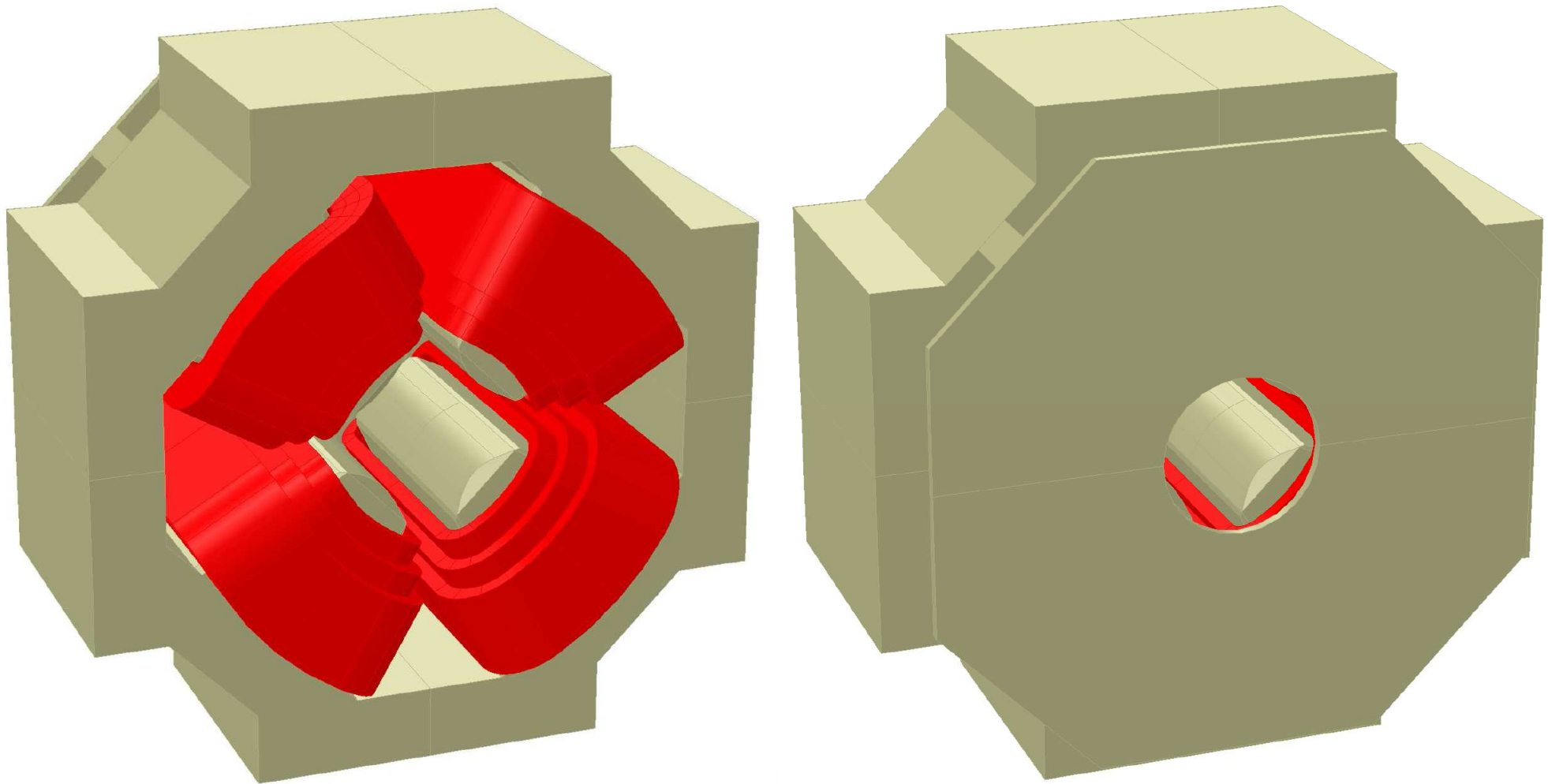
The poles edges are vertically chamfered to allow rounding the coils close to the pole itself...

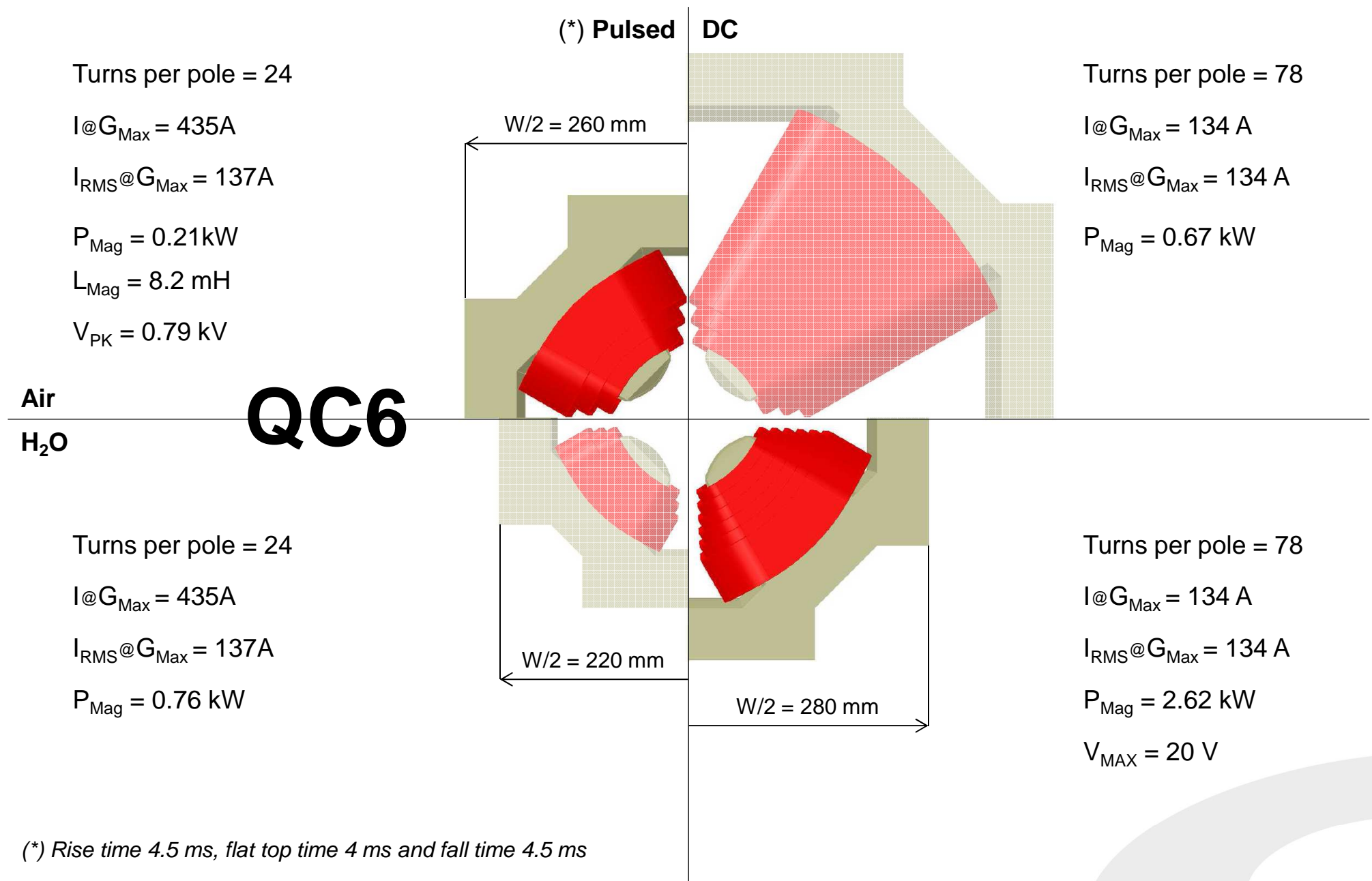
The pole transversal section is trapezoidal to reduce the saturation...

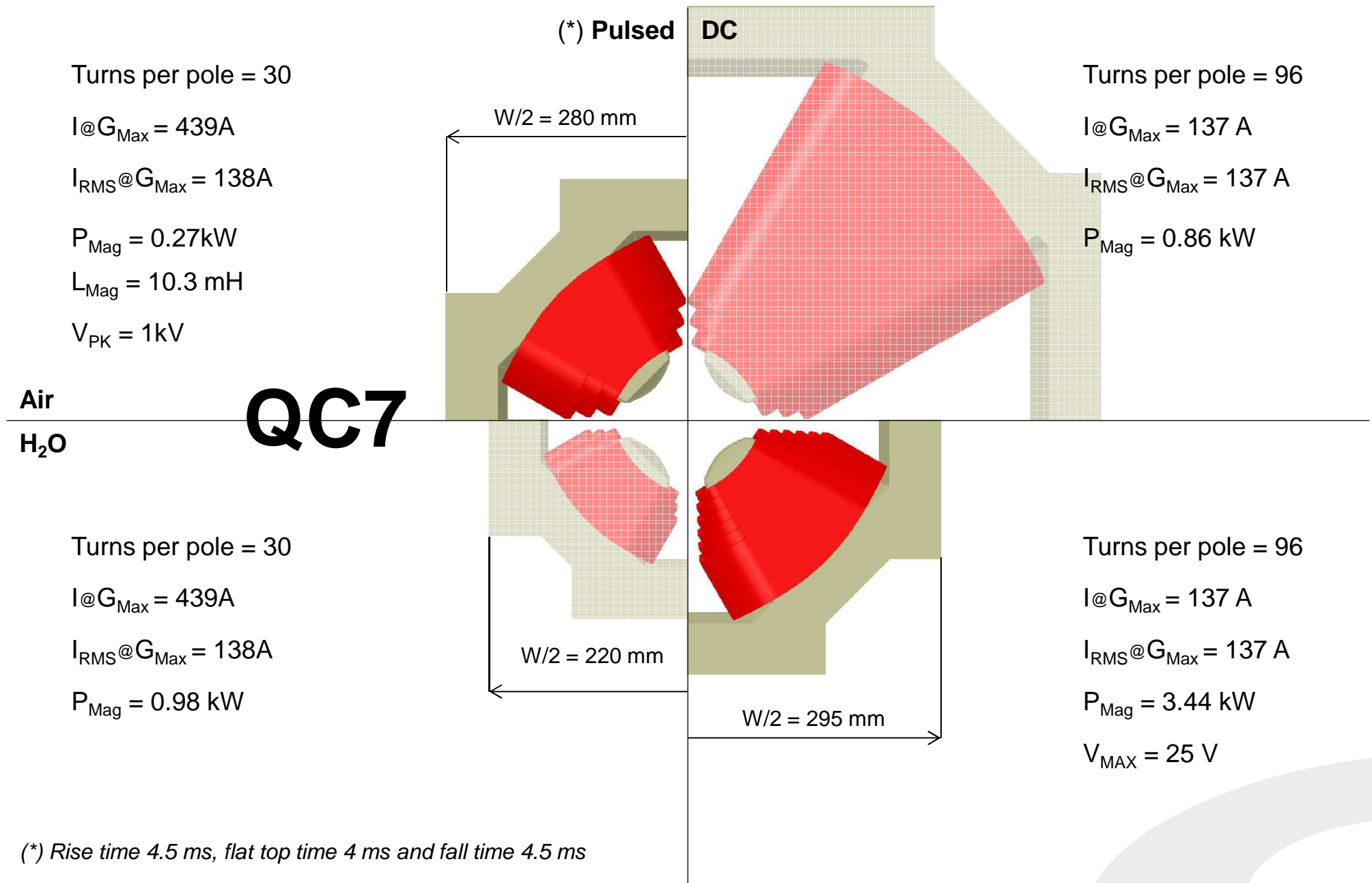
The coils are not simple racetrack, they are defined in Opera by straight and arc conductors



QC7 with 30 turns and coils made by solid copper... (shield shown on one side only)







QC6 QC7

Turns per pole = 24

$I@G_{Max} = 435A$

$I_{RMS}@G_{Max} = 137A$

$P_{Mag} = 0.21kW$

$L_{Mag} = 8.2 \text{ mH}$

$V_{PK} = 0.79 \text{ kV}$

Turns per pole = 30

$I@G_{Max} = 439 A$

$I_{RMS}@G_{Max} = 138 A$

$P_{Mag} = 0.27 \text{ kW}$

$L_{Mag} = 10.3 \text{ mH}$

$V_{PK} = 1kV$

Pulsed (*)

DC

Turns per pole = 78

$I@G_{Max} = 134 A$

$I_{RMS}@G_{Max} = 134 A$

$P_{Mag} = 2.62 \text{ kW}$

$V_{MAX} = 20 \text{ V}$

Turns per pole = 96

$I@G_{Max} = 137 A$

$I_{RMS}@G_{Max} = 137 A$

$P_{Mag} = 3.44 \text{ kW}$

$V_{MAX} = 25 \text{ V}$

(*) Rise time 4.5 ms, flat top time 4 ms and fall time 4.5 ms

QC6 QC7

Turns per pole = 24

$I@G_{Max} = 435A$

$I_{RMS}@G_{Max} = 137A$

$P_{Mag} = 0.21kW$

$L_{Mag} = 8.2\text{ mH}$

$V_{PK} = 0.79\text{ kV}$

Rise/Fall 4.5 ms

Rise/Fall 8.0 ms

Turns per pole = 30

$I@G_{Max} = 126\text{ A}$

$I_{RMS}@G_{Max} = 348\text{ A}$

$P_{Mag} = 0.23\text{ kW}$

$L_{Mag} = 10.3\text{ mH}$

$V_{PK} = 0.45\text{ kV}$

Turns per pole = 30

$I@G_{Max} = 439\text{ A}$

$I_{RMS}@G_{Max} = 138\text{ A}$

$P_{Mag} = 0.27\text{ kW}$

$L_{Mag} = 10.3\text{ mH}$

$V_{PK} = 1kV$

Turns per pole = 36

$I@G_{Max} = 133\text{ A}$

$I_{RMS}@G_{Max} = 366\text{ A}$

$P_{Mag} = 0.30\text{ kW}$

$L_{Mag} = 14.0\text{ mH}$

$V_{PK} = 0.64\text{ kV}$

QC6 QC7

Turns per pole = 30

$I@G_{Max} = 348 \text{ A}$

$I_{RMS}@G_{Max} = 126 \text{ A}$

$P_{Mag} = 0.23 \text{ kW}$

$L_{Mag} = 10.3 \text{ mH}$

$V_{PK} = 0.45 \text{ kV}$

Rise 8 ms (*)

DC

Turns per pole = 78

$I@G_{Max} = 134 \text{ A}$

$I_{RMS}@G_{Max} = 134 \text{ A}$

$P_{Mag} = 2.62 \text{ kW}$

$V_{MAX} = 20 \text{ V}$

Turns per pole = 36

$I@G_{Max} = 366 \text{ A}$

$I_{RMS}@G_{Max} = 133 \text{ A}$

$P_{Mag} = 0.30 \text{ kW}$

$L_{Mag} = 14.0 \text{ mH}$

$V_{PK} = 0.64 \text{ kV}$

Turns per pole = 96

$I@G_{Max} = 137 \text{ A}$

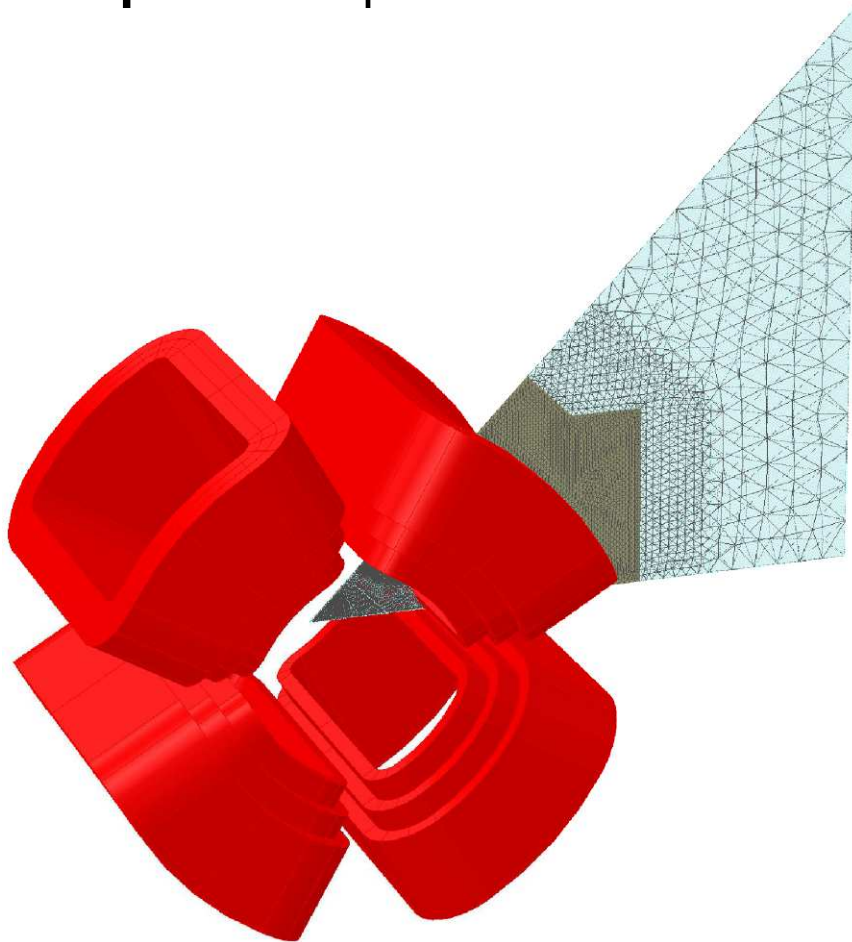
$I_{RMS}@G_{Max} = 137 \text{ A}$

$P_{Mag} = 3.44 \text{ kW}$

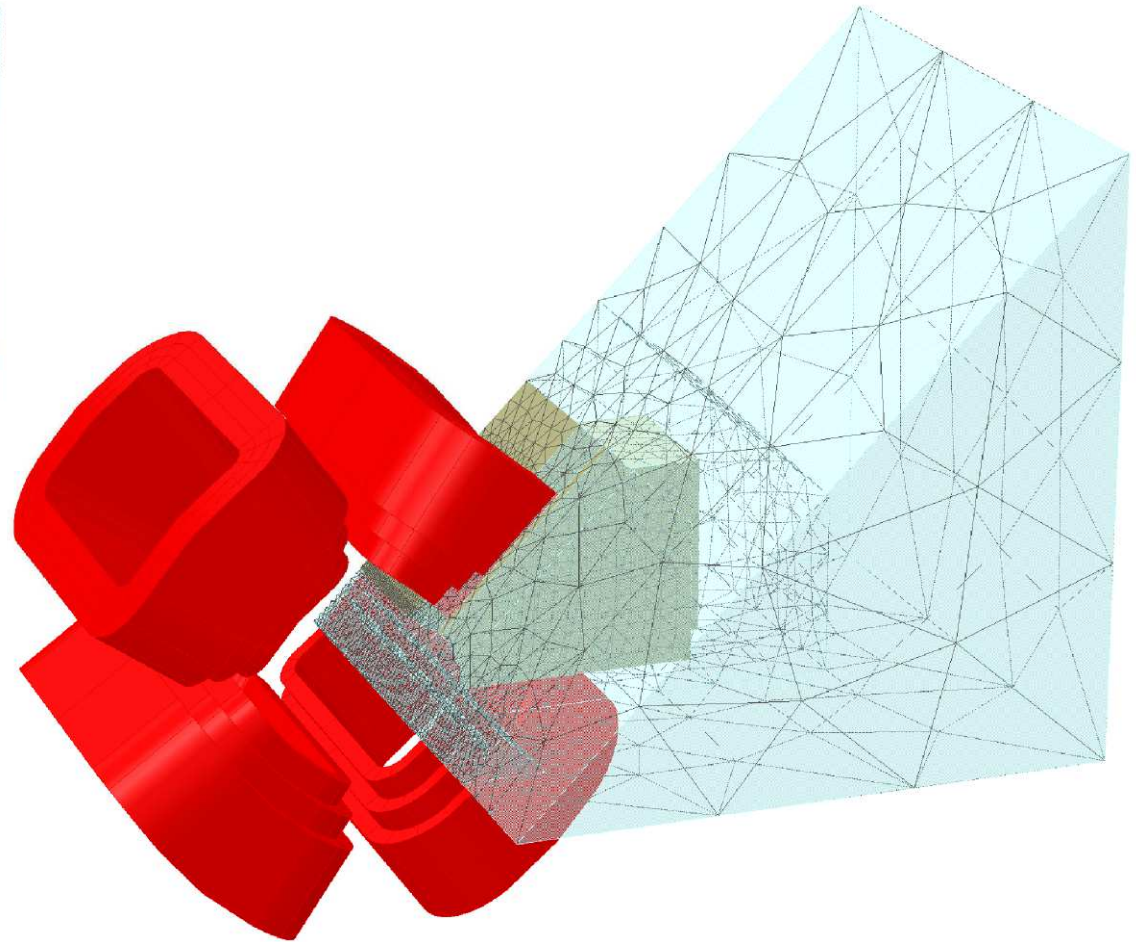
$V_{MAX} = 25 \text{ V}$

(*) Rise time 8.0 ms, flat top time 4 ms and fall time 8.0 ms

QC7 pulsed: Opera models



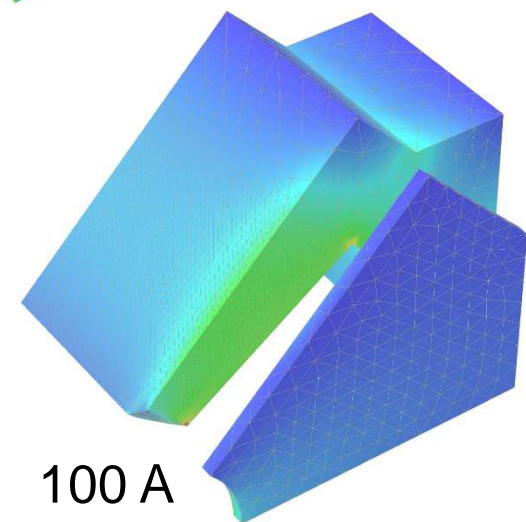
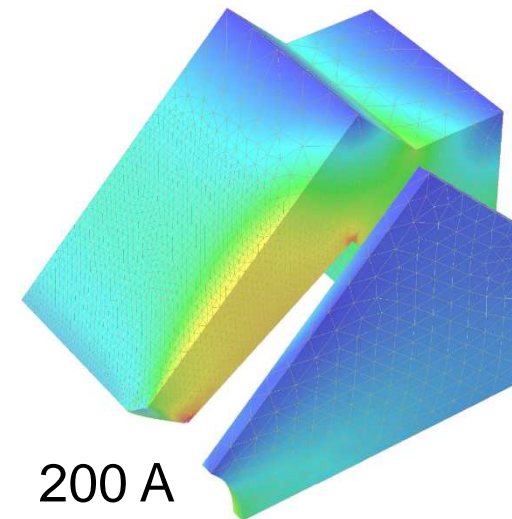
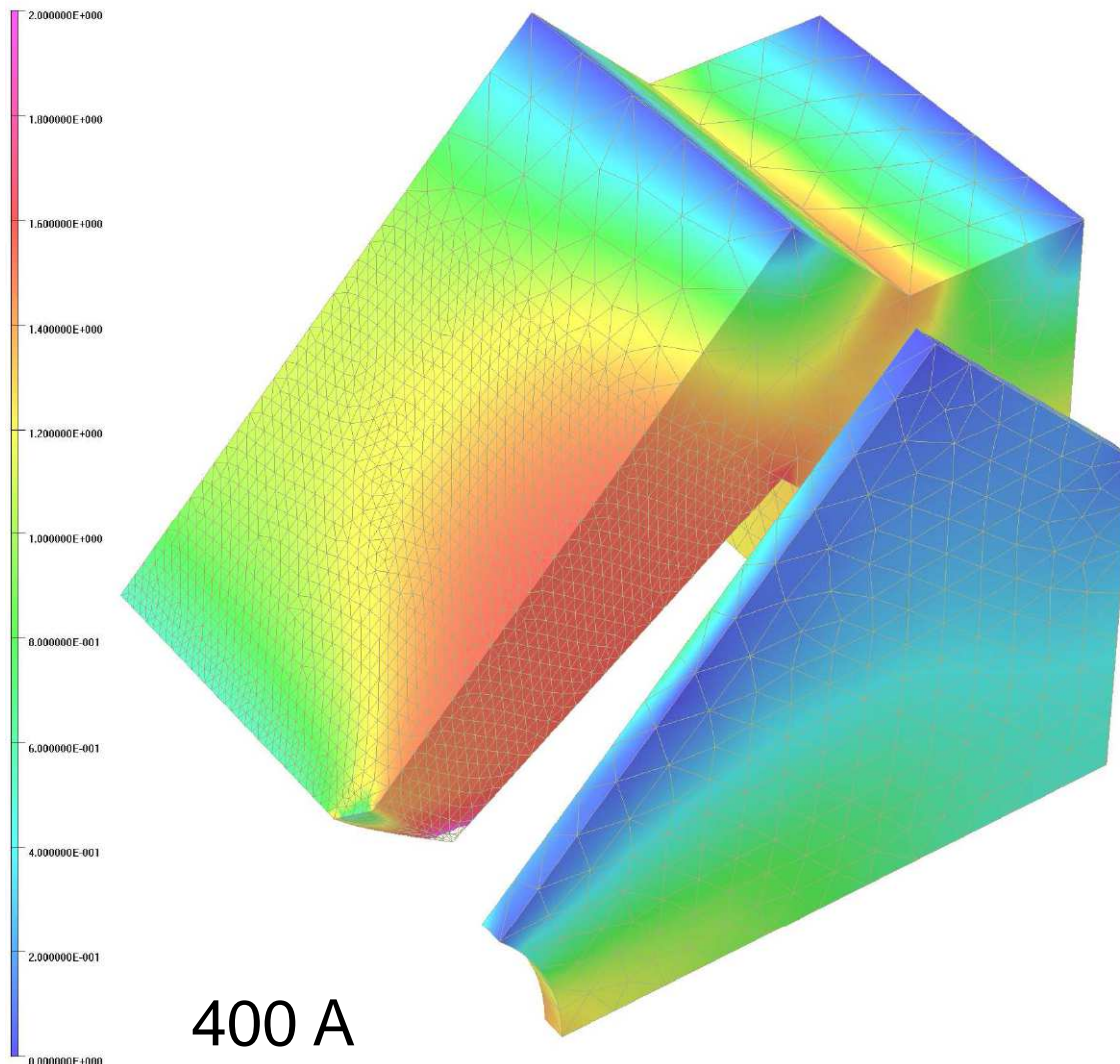
Single lamination model (2.5D)



3D model

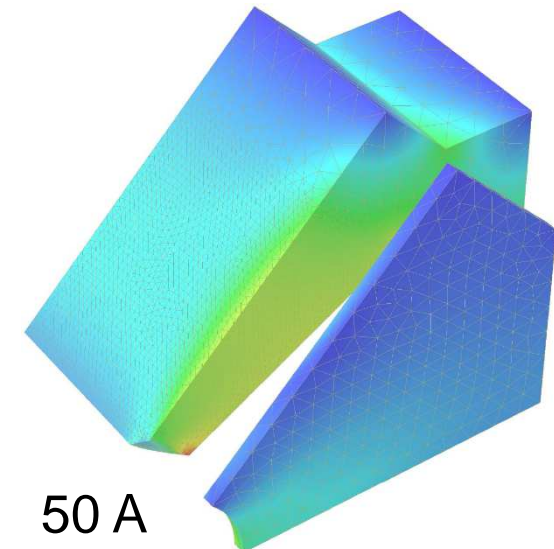
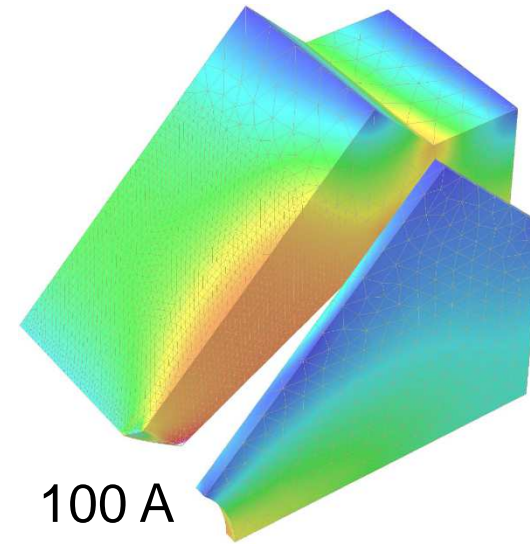
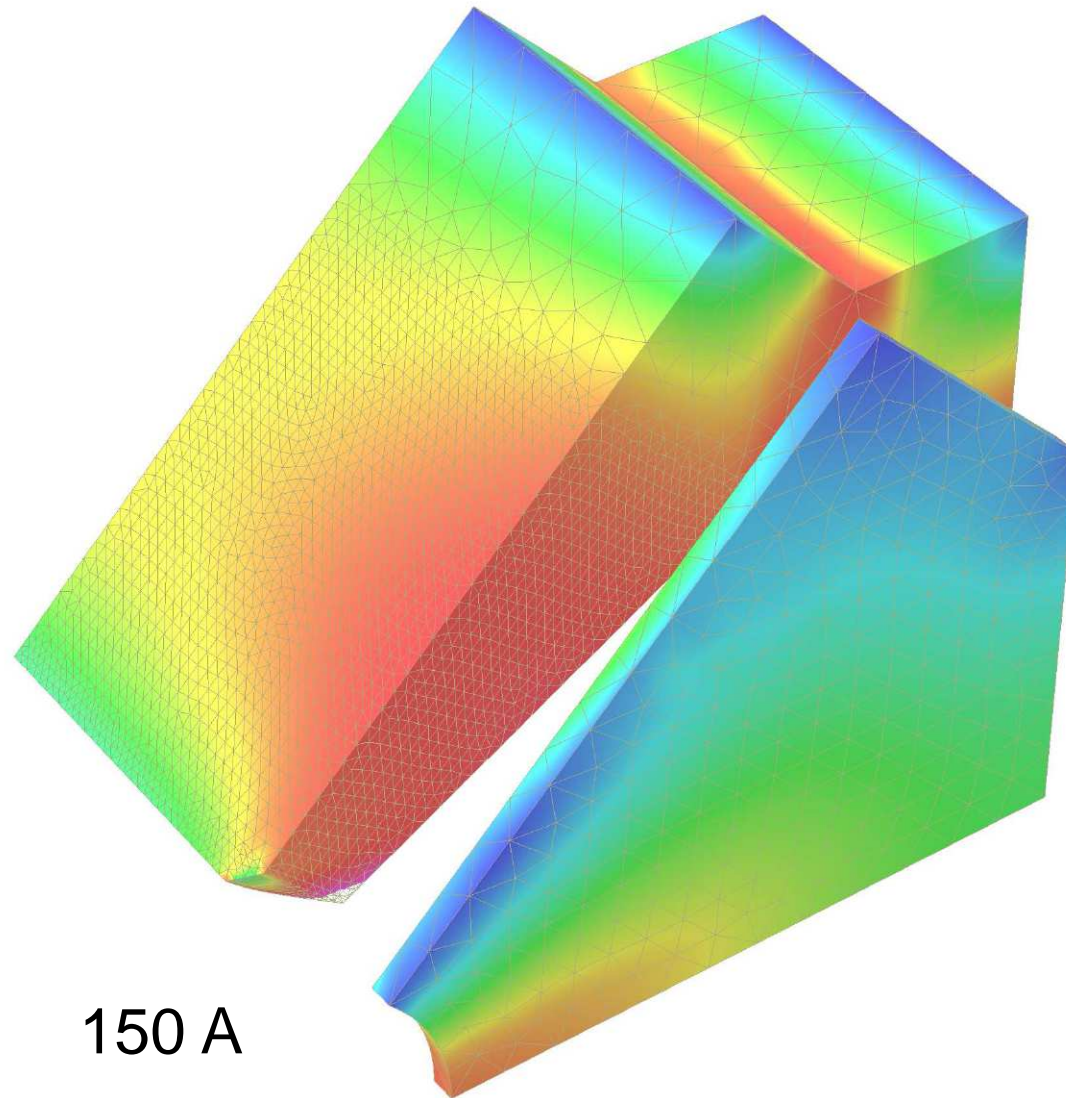
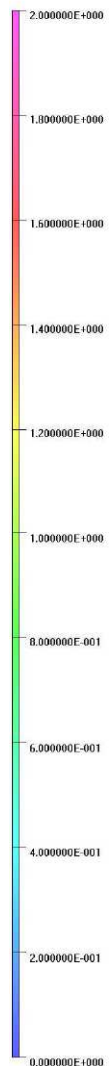
QC7 pulsed: Tosca simulations at:

Surface contours: BMOD



QC7 DC: Tosca simulations at:

Surface contours: BMOD

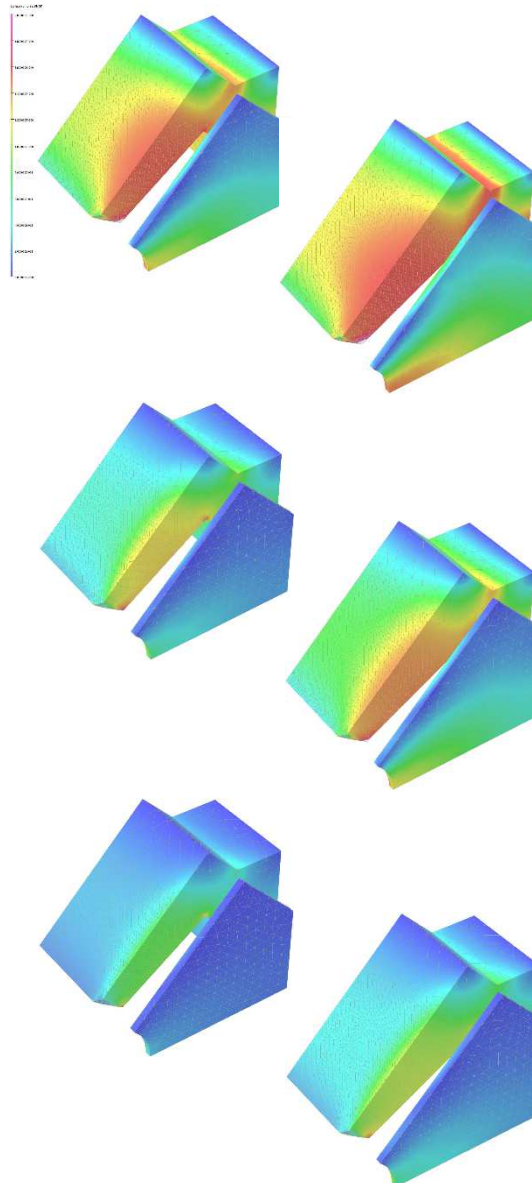


QC7 pulsed - Tosca results:

| Int.Gradient (at x = 35mm) at 400A; $G2_{sat} = -0.99\%$ | | |
|--|---------------|---------------|
| GN | G | G/G2 [%] |
| G2 [T/m] | 2.5671 | 100.00 |
| G4 [T/m ⁴] | 0.0001 | 0.0020 |
| G6 [T/m ⁶] | 0.0013 | 0.0510 |
| G8 [T/m ⁸] | 0.0001 | 0.0042 |
| G10 [T/m ¹⁰] | 0.0004 | 0.0141 |

| Int.Gradient (at x = 35mm) at 200A; $G2_{sat} = -0.06\%$ | | |
|--|---------------|---------------|
| GN | G | G/G2 [%] |
| G2 [T/m] | 1.2956 | 100.00 |
| G4 [T/m ⁴] | 0.0000 | 0.0021 |
| G6 [T/m ⁶] | 0.0006 | 0.0456 |
| G8 [T/m ⁸] | 0.0001 | 0.0042 |
| G10 [T/m ¹⁰] | 0.0002 | 0.0141 |

| Int.Gradient (at x = 35mm) at 100A; $G2_{sat} = ref(0\%)$ | | |
|---|---------------|---------------|
| GN | G | G/G2 [%] |
| G2 [T/m] | 0.6482 | 100.00 |
| G4 [T/m ⁴] | 0.0000 | 0.0021 |
| G6 [T/m ⁶] | 0.0003 | 0.0451 |
| G8 [T/m ⁸] | 0.0000 | 0.0042 |
| G10 [T/m ¹⁰] | 0.0001 | 0.0142 |



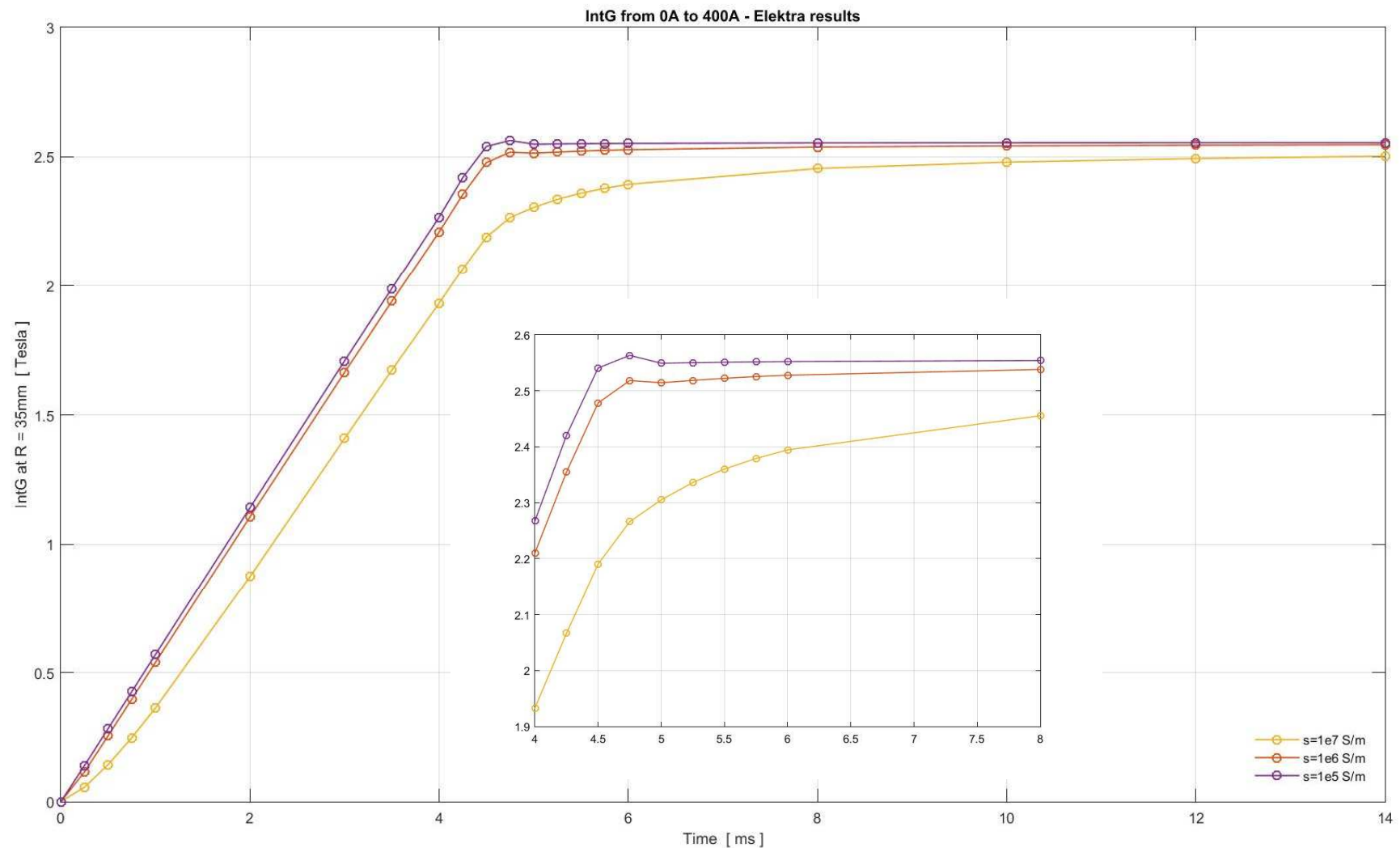
QC7 DC - Tosca results:

| Int.Gradient (at x = 35mm) at 150A; $G2_{sat} = -3.72\%$ | | |
|--|---------------|---------------|
| GN | G | G/G2 [%] |
| G2 [T/m] | 2.9937 | 100.00 |
| G4 [T/m ⁴] | 0.0001 | 0.0015 |
| G6 [T/m ⁶] | 0.0014 | 0.0461 |
| G8 [T/m ⁸] | 0.0001 | 0.0045 |
| G10 [T/m ¹⁰] | 0.0004 | 0.0141 |

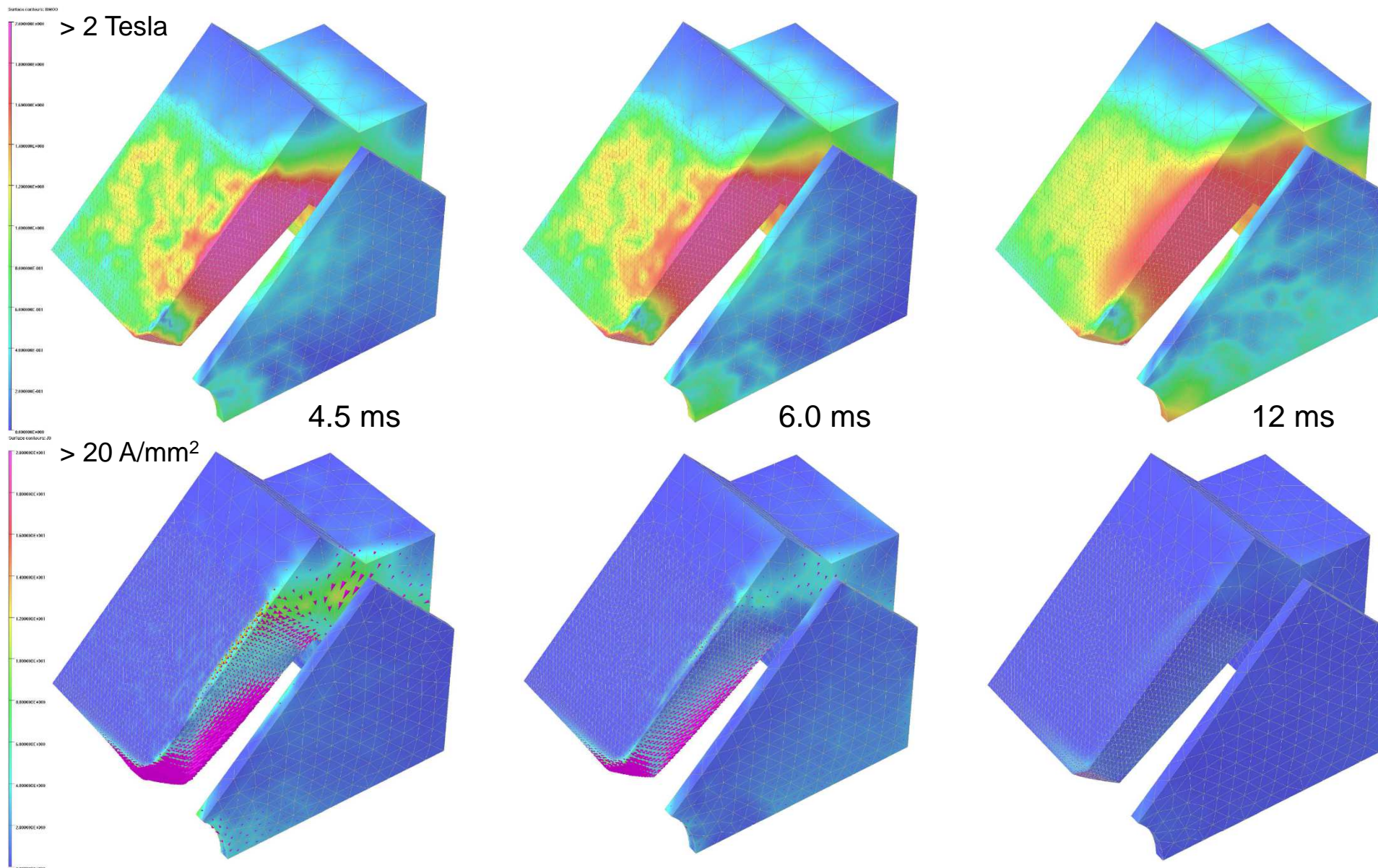
| Int.Gradient (at x = 35mm) at 100A; $G2_{sat} = -0.43\%$ | | |
|--|---------------|---------------|
| GN | G | G/G2 [%] |
| G2 [T/m] | 2.0639 | 100.00 |
| G4 [T/m ⁴] | 0.0000 | 0.0016 |
| G6 [T/m ⁶] | 0.0008 | 0.0389 |
| G8 [T/m ⁸] | 0.0001 | 0.0045 |
| G10 [T/m ¹⁰] | 0.0003 | 0.0141 |

| Int.Gradient (at x = 35mm) at 50A; $G2_{sat} = ref(0\%)$ | | |
|--|---------------|---------------|
| GN | G | G/G2 [%] |
| G2 [T/m] | 1.0365 | 100.00 |
| G4 [T/m ⁴] | 0.0000 | 0.0017 |
| G6 [T/m ⁶] | 0.0004 | 0.0368 |
| G8 [T/m ⁸] | 0.0000 | 0.0045 |
| G10 [T/m ¹⁰] | 0.0001 | 0.0141 |

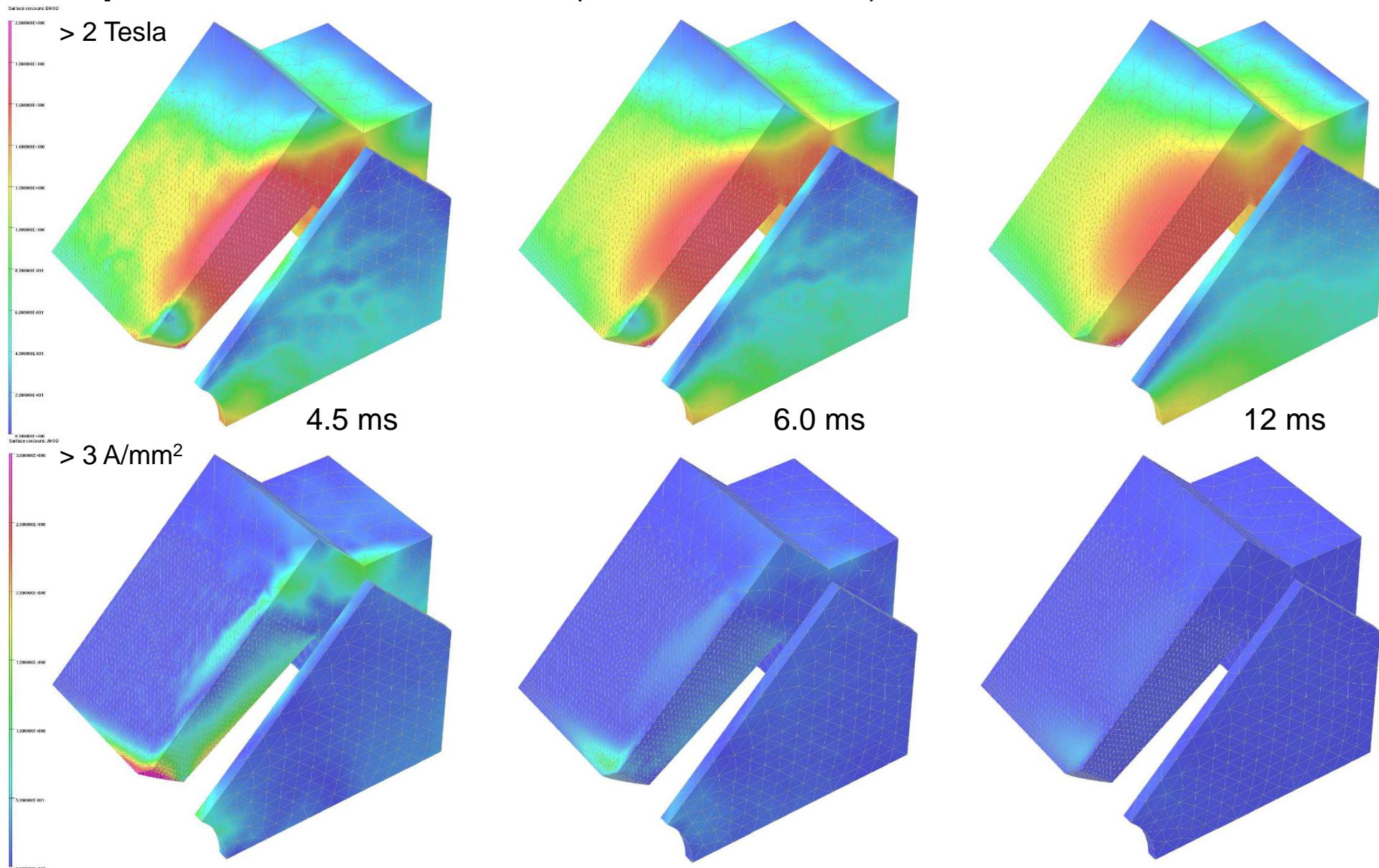
QC7 pulsed - *Elektra* results:



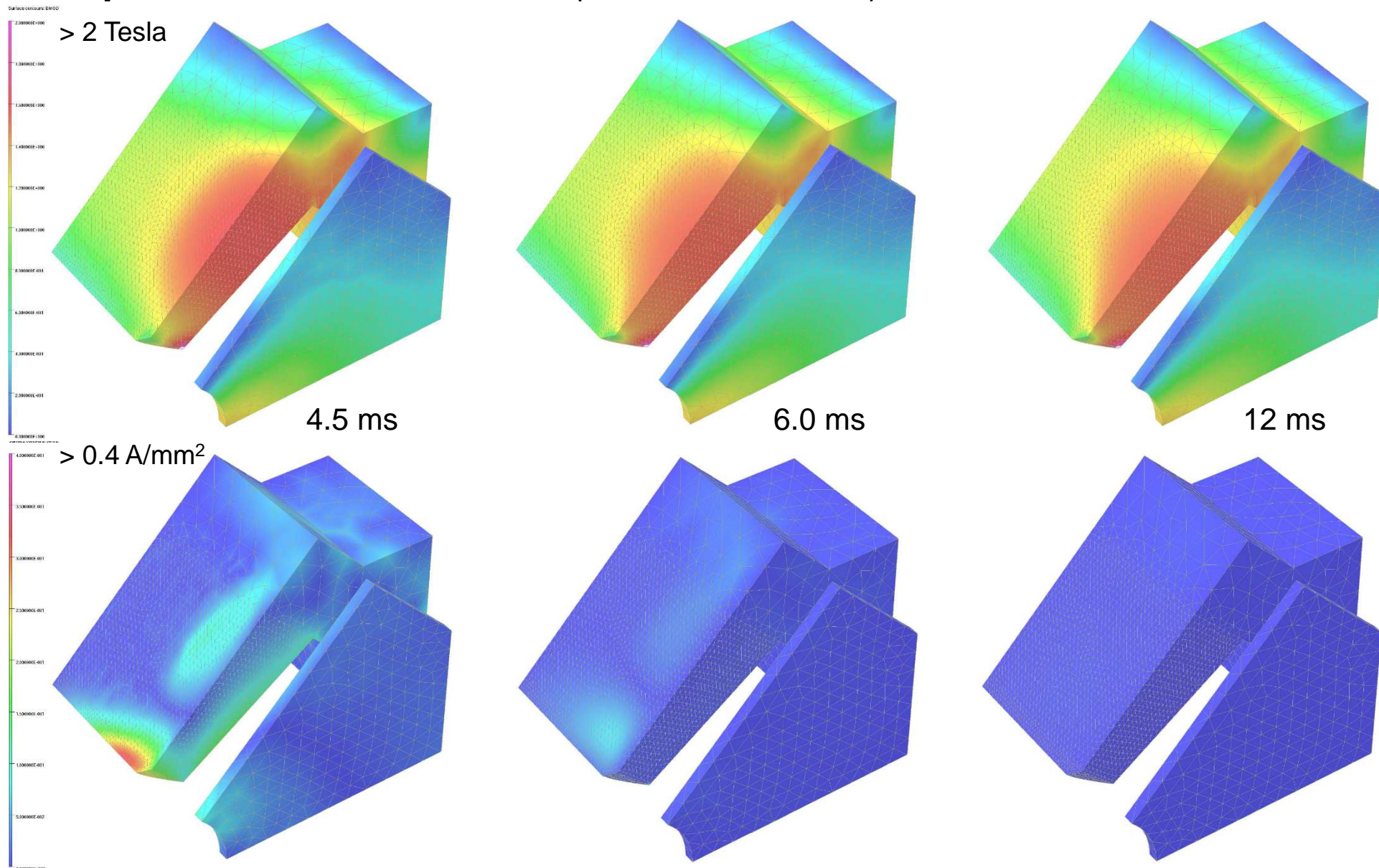
QC7 pulsed - Elektra simulation (iron $\sigma = 1e7$ S/m)



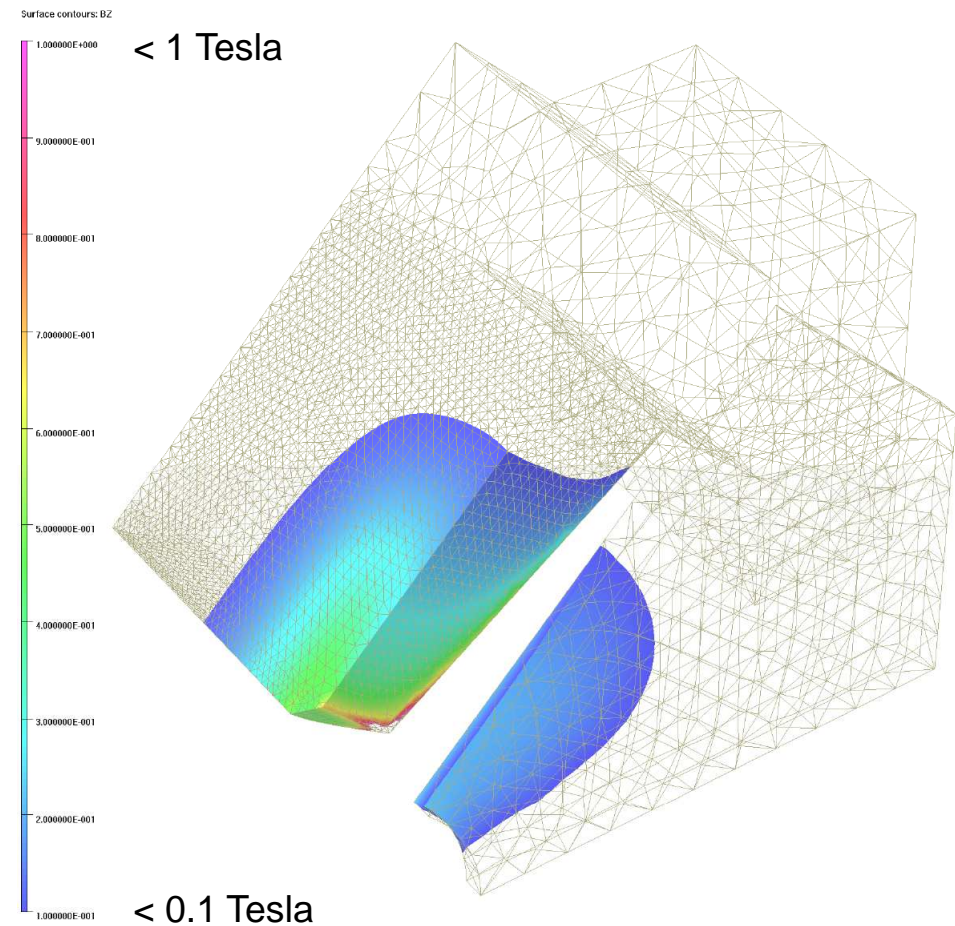
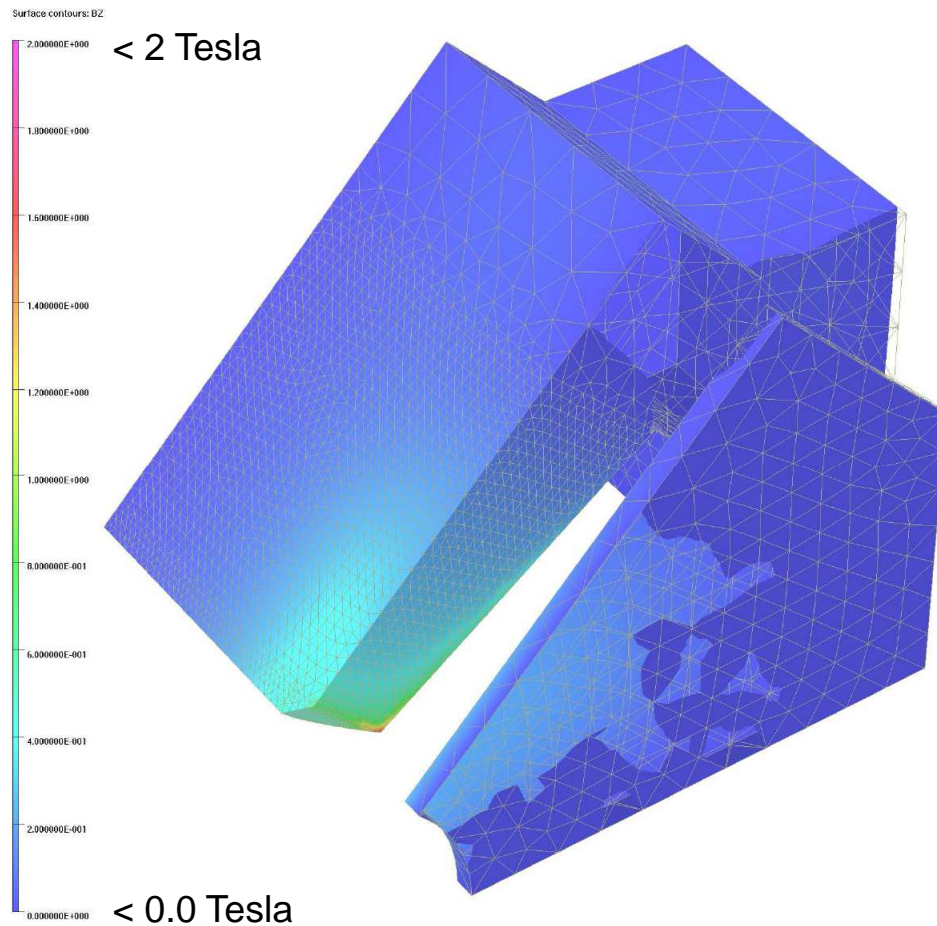
QC7 pulsed - Elektra simulation (iron $\sigma = 1e6$ S/m)



QC7 pulsed - Elektra simulation (iron $\sigma = 1e5$ S/m)



Big aperture magnets → B_z distribution



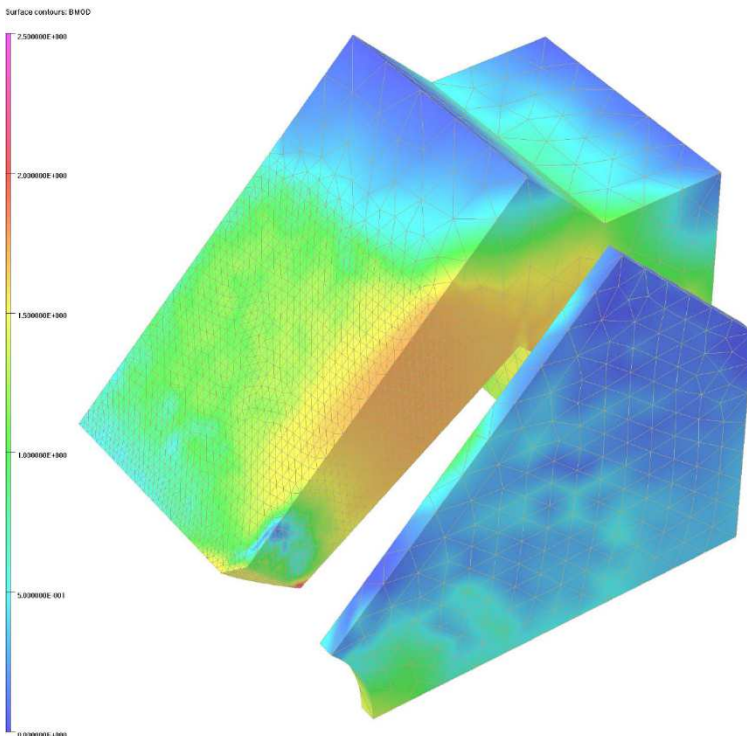
> The Yoke must be realized by 0.35 mm lamination of Fe-Si 3-3.5%

QC7 pulsed **with shields**

| <i>Int.Gradient (at x = 35 mm) at 400 A (T = 12 ms);</i> | | |
|--|---------------|---------------|
| GN | G | G/G2 [%] |
| G2 [T/m] | 2.4981 | 100.00 |
| G4 [T/m ⁴] | 0.0002 | 0.0075 |
| G6 [T/m ⁶] | 0.0032 | 0.1278 |
| G8 [T/m ⁸] | 0.0031 | 0.1230 |
| G10 [T/m ¹⁰] | 0.0005 | 0.0190 |

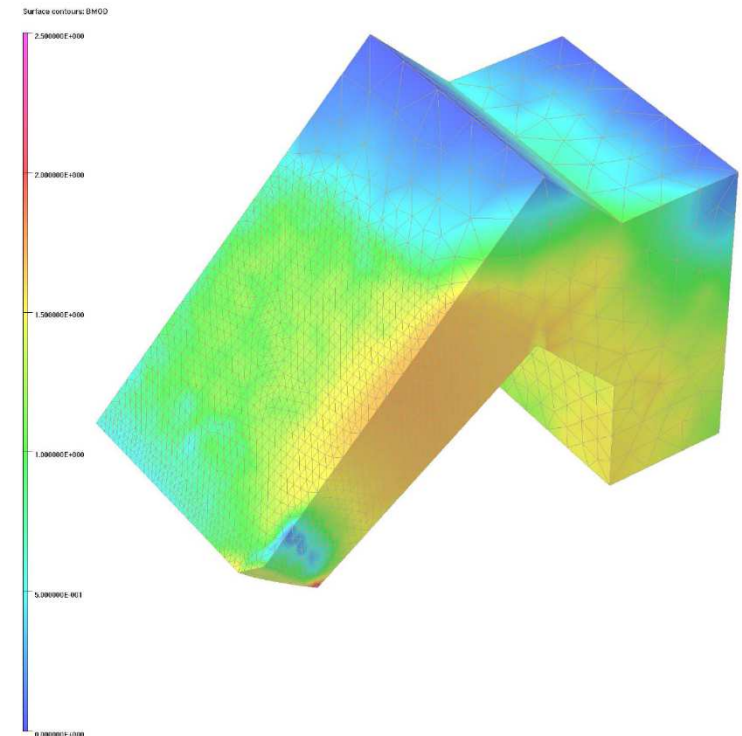
2.50 T/m Vs 2.65 T/m

⇒ **+6%**



QC7 pulsed **without shields**

| <i>Int.Gradient (at x = 35 mm) at 400 A (T = 12 ms);</i> | | |
|--|---------------|---------------|
| GN | G | G/G2 [%] |
| G2 [T/m] | 2.6486 | 100.00 |
| G4 [T/m ⁴] | 0.0002 | 0.0057 |
| G6 [T/m ⁶] | 0.0028 | 0.1071 |
| G8 [T/m ⁸] | 0.0034 | 0.1276 |
| G10 [T/m ¹⁰] | 0.0006 | 0.0214 |



Required stability: ± 100 ppm vs. nominal DC (i.e. ± 15 mA)

1. DC

- Estimated max voltage drop on cable (@ 150 A) = **5 V**
- Unify the PS type for both QC6 & QC7: **35 V / 150 A**
- Unify the remote control interface **FOR ALL PS** (not only QC6 & QC7)
- Large number of PS for QC6 & QC7: **120 PS** (incl. 10% spare)
- Stability higher than “average commercial”

Custom-made solution could be economically comparable to “Commercial”

AND

tailored to actual needs

Required stability: ± 100 ppm vs. nominal on Flat-Top of the pulse (i.e. ± 45 mA)

Additional requirement: Output voltage and internal DC-Link voltage < 1 kV

2. Pulsed “4.5” – peak current $450 A_{PK}$, rms current $140 A_{RMS}$

- Estimated max **resistive** voltage drop on cable (@ 450 A) = **11 V**
- Different PS types for QC6 & QC7: **850 V_{PK} / 450 A_{PK}** (QC6) & **1050 V_{PK} / 450 A_{PK}** (QC7)
- Unify the remote control interface **FOR ALL PS** (not only QC6 & QC7)
- Large number of PS for QC6: **105 PS** (incl. 10% spare)
- Small number of PS for QC7: **14 PS** (incl. 15% spare)
- Various topologies are possible and available, to be further investigated

Custom-made solution is needed to meet the actual needs

Required stability: ± 100 ppm vs. nominal on Flat-Top of the pulse (i.e. ± 40 mA)

Additional requirement: Output voltage and internal DC-Link voltage < 1 kV

3. Pulsed “8.0” – peak current $400 A_{PK}$, rms current $130 A_{RMS}$

- Estimated max **resistive** voltage drop on cable (@ 400 A) = **11 V**
- Similar PS types for QC6 & QC7: **$500 V_{PK} / 400 A_{PK}$** (QC6) & **$700 V_{PK} / 400 A_{PK}$** (QC7)
- Unify the PS for both QC6 & QC7: **$700 V_{PK} / 400 A_{PK}$**
- Unify the remote control interface **FOR ALL PS** (not only QC6 & QC7)
- Large number of PS for QC6 & QC7: **120 PS** (incl. 10% spare)
- Various topologies are possible and available, to be further investigated

Custom-made solution is needed to meet the actual needs

From our experience on Elettra and FERMI:

1. Power is always paid twice: for generating it, and removing it
2. Keep the peak voltage on PS and magnets <1 kV \Rightarrow avoid MV-rated components, cables, rules,...
3. Minimize the number of different types of PS (operation, maintenance, spares,...)
4. Unify interfaces PS-RCS and PS-PSS+MPS⁽⁺⁾ among PS types/families
5. Minimize use of water cooling both on magnets and PS
 - Plant \Rightarrow de-ionized water, radiation resistant rubber pipes for magnets,...
 - Operation \Rightarrow integration into MPS,...
 - Reliability \Rightarrow risk of leakages, clogging of coils,...
 - Maintenance \Rightarrow operate close or over delicate equipment,...

⁽⁺⁾RCS = Remote Control System; PSS = Personnel Safety System; MSS = Machine Protection System

Compared several design for magnets QC6 and QC7, both in DC and Pulsed

1. DC is a standard, well-known solution:

- ✗ Power consumption \Rightarrow 2.4 kW for each QC6; 3.5 kW for each QC7
- ✗ Water cooling of magnets \Rightarrow de-ionized water plant,...
- ✓ “Low Power” but stable power supplies (\sim 5 kW)

2. Pulsed excitation is a less common solution:

- ✓ Power consumption \Rightarrow significantly more efficient than DC
- ✓ Air cooling of magnets \Rightarrow no piping, etc. but heat to environment
 - High peak output voltage \Rightarrow risk of exceeding 1 kV (design & operations)
 - Shape of the pulse is important (e.g. rise time: 8.0 ms vs. 4.5 ms)

3. Costs considerations for magnets:

- QC6 and QC7 could be the same model with and without the shields
- Both DC and Pulsed could have the same yoke geometry
- ❖ Pulsed mode yoke must be realized with Fe-Si 3-3.5%, lamination 0.35 mm
- Both DC and Pulsed have the same coils dimension
- ❖ DC coils are water-cooled

⇒ **The total costs could be comparable for both types**

4. Costs considerations for power supplies:

- Custom PS (either DC or Pulsed)
- Pulsed PS are more powerful (peak) than DC, more expensive

5. Potential savings with Pulsed Solution:

- No need of de-ionized water (plant installation and running)
- Reduced electrical power consumption (mains and dissipation)
- Reliability of operations and reduced maintenance

Thank You!