

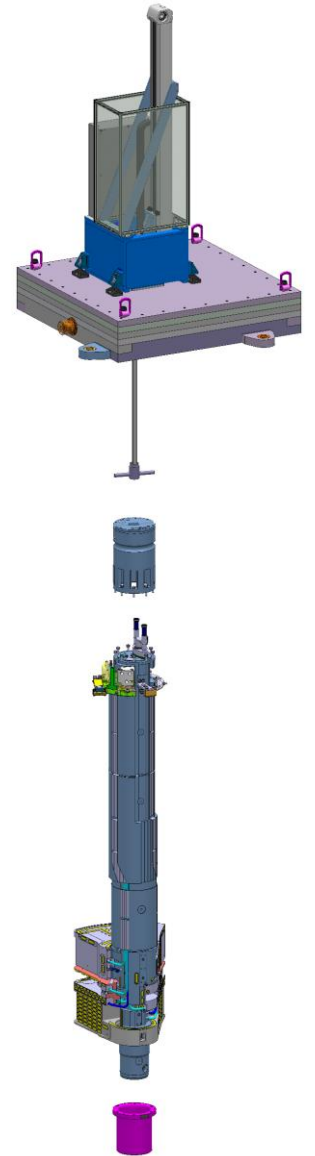
Status of development and production of second ESS Moderator & Reflector Plug (MRP-II)

ICANS XXV, Malmö, Sweden

2025-04-15 | Y. BEßLER, C. HAPPE, P. SCHUMACHER, U. PABST, S. SCHÖNEN, J. WOLTERS, G. NATOUR

CONTENT

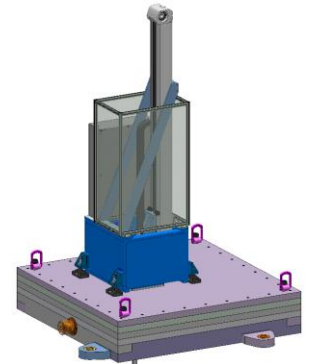
1. Overview
2. Cold Moderator
3. Irradiation Module
4. Thermal Moderator
5. Vacuum Jackets & Vacuum Chamber
6. Beryllium Reflector
7. MRP Support Structure
8. Main Assembly
9. Production status
10. Summary & Outlook



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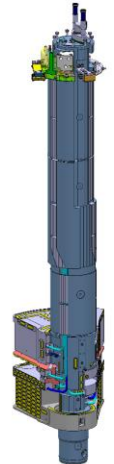
Handling Tool
"Rotation Unit"



Lifting & rotation
Adapter "Crown"



MRP-II

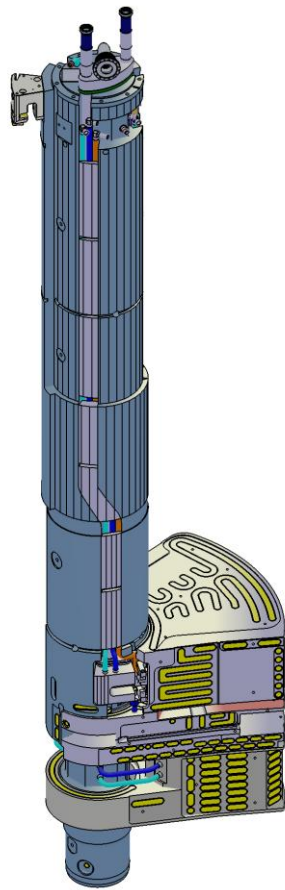


MRP
"Bucket"

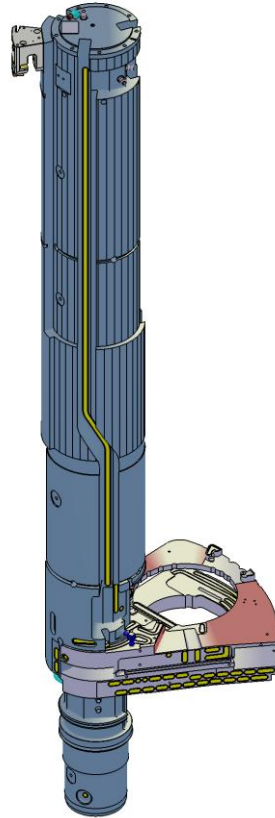
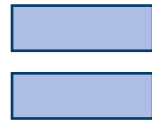


DESIGN SOLUTION MRP-II

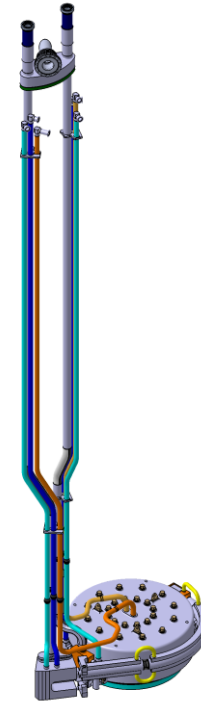
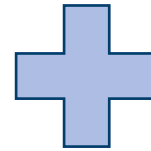
Overview



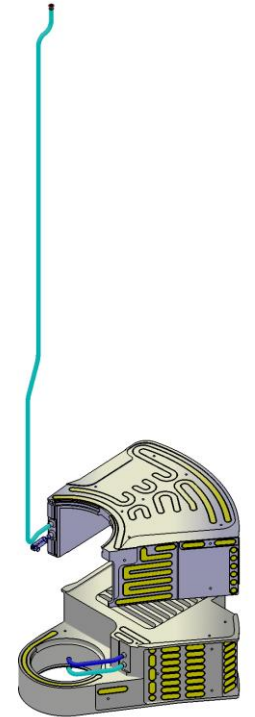
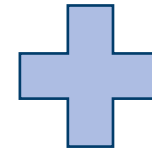
MRP 2



MRP Support Structure



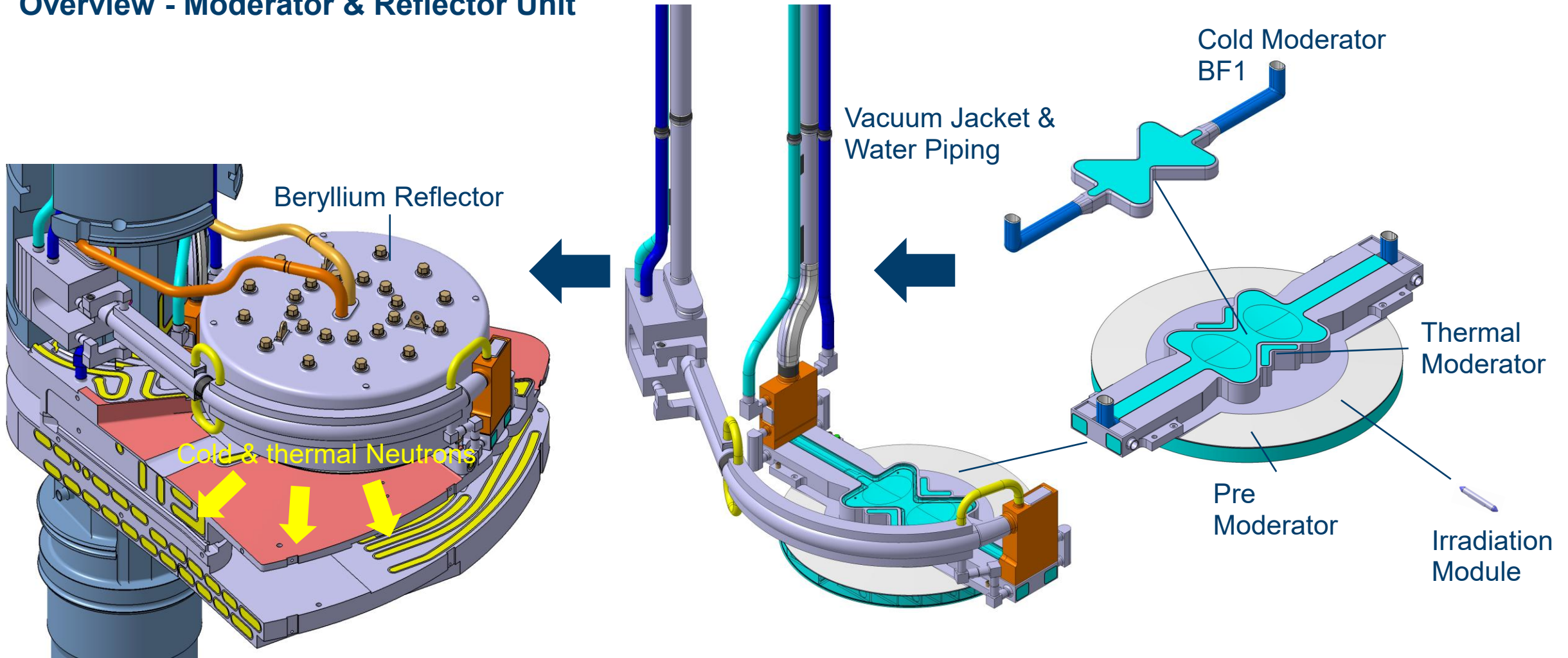
Moderator & Reflector
Unit



Outer Frame / Reflector

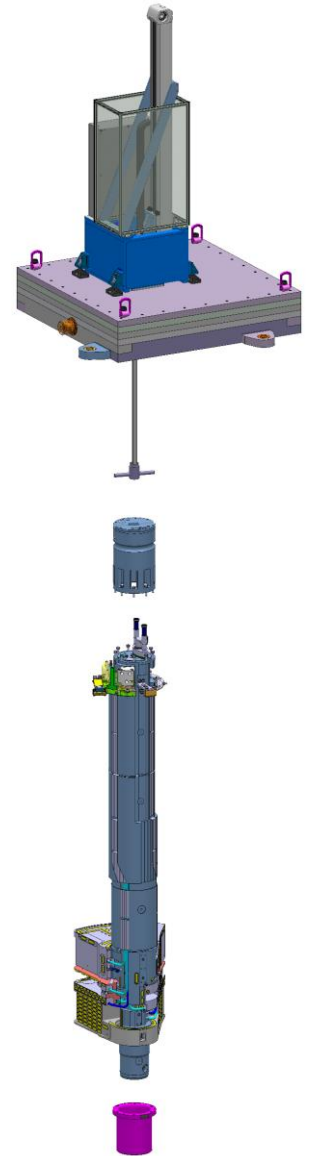
DESIGN SOLUTION MRP-II

Overview - Moderator & Reflector Unit



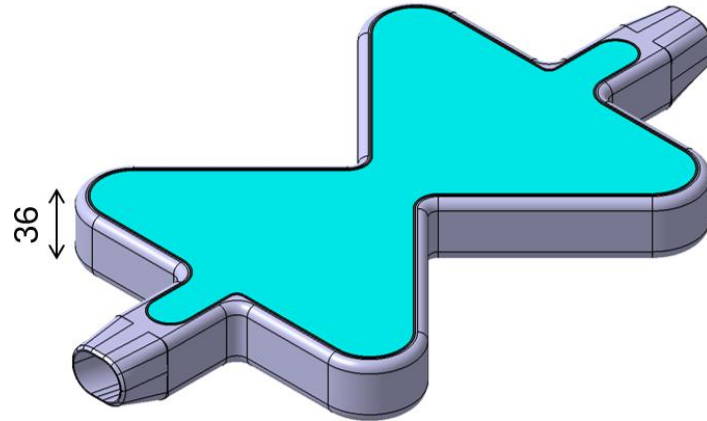
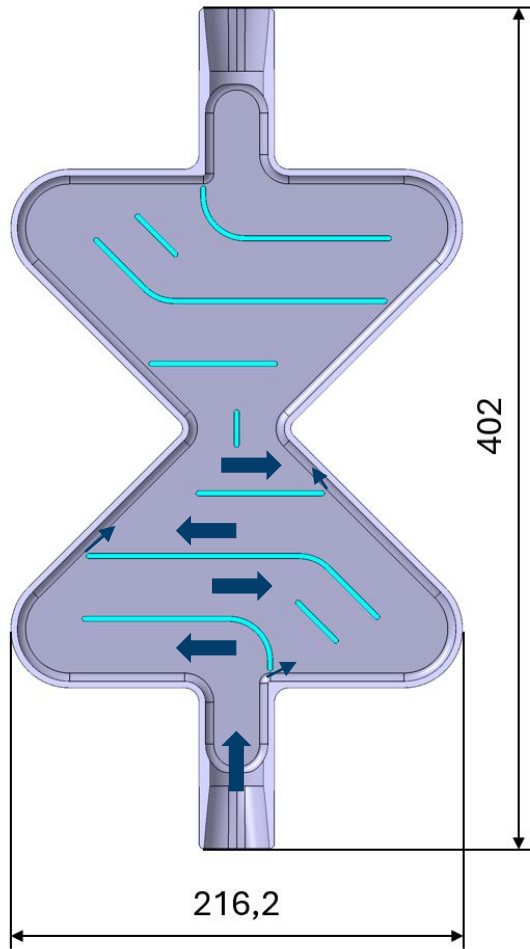
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DESIGN SOLUTION MRP-II

Cold Moderator BF1 – Overview

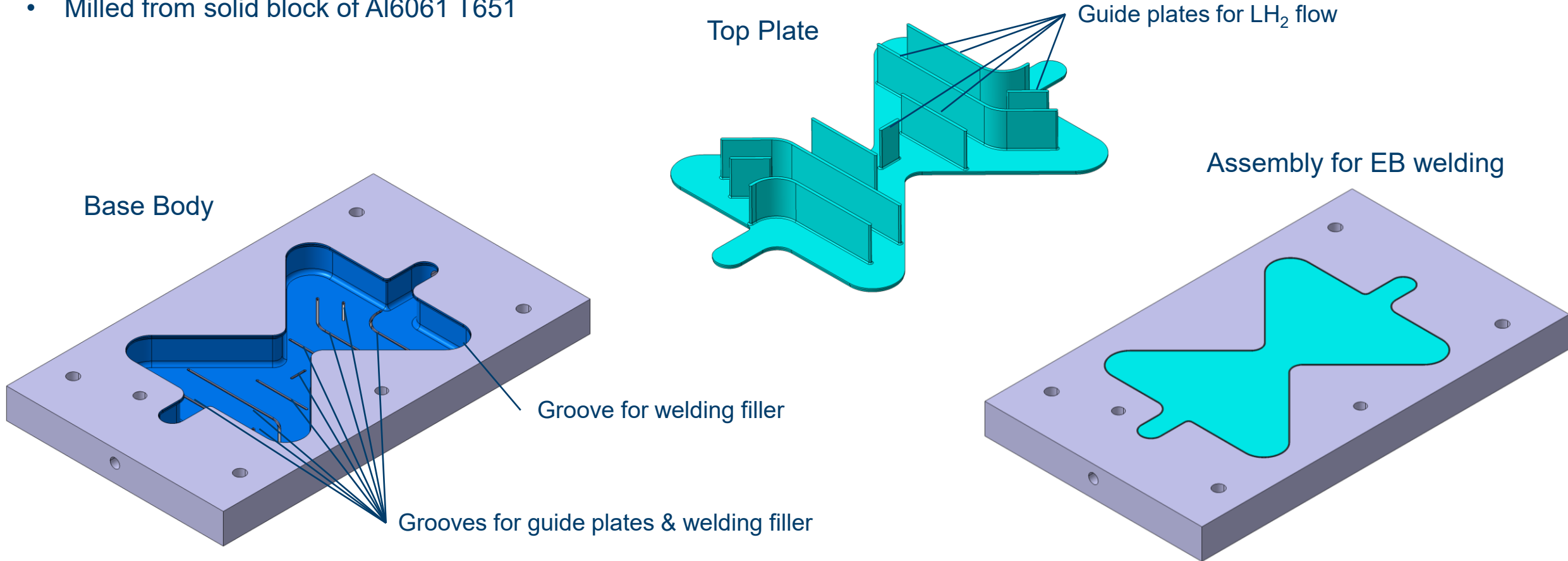


- Pressure vessel made of Al6061 T651
- Electron-Beam (EB) welded with filler material Al4047
- Liquid Hydrogen at an inlet temp. of $T_{in} = 17.5$ K with a temp. increase of $dT \leq 3$ K
- Design pressure 17 bar
- Operating pressure 10 bar
- Heat deposition of ca. 7.1 kW
- $m_{Al} = 1.15$ kg (without LH₂ inventory)
- $V_{LH_2} \sim 1$ l
- 3 mm wall thickness

DESIGN SOLUTION MRP-II

Cold Moderator BF1 – Manufacturing

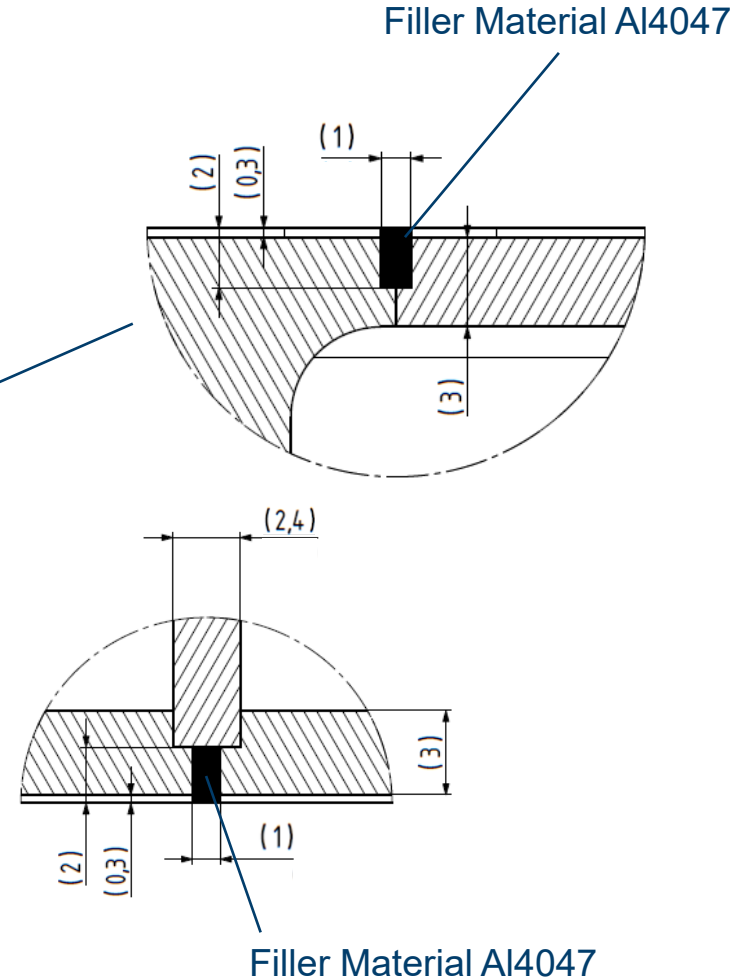
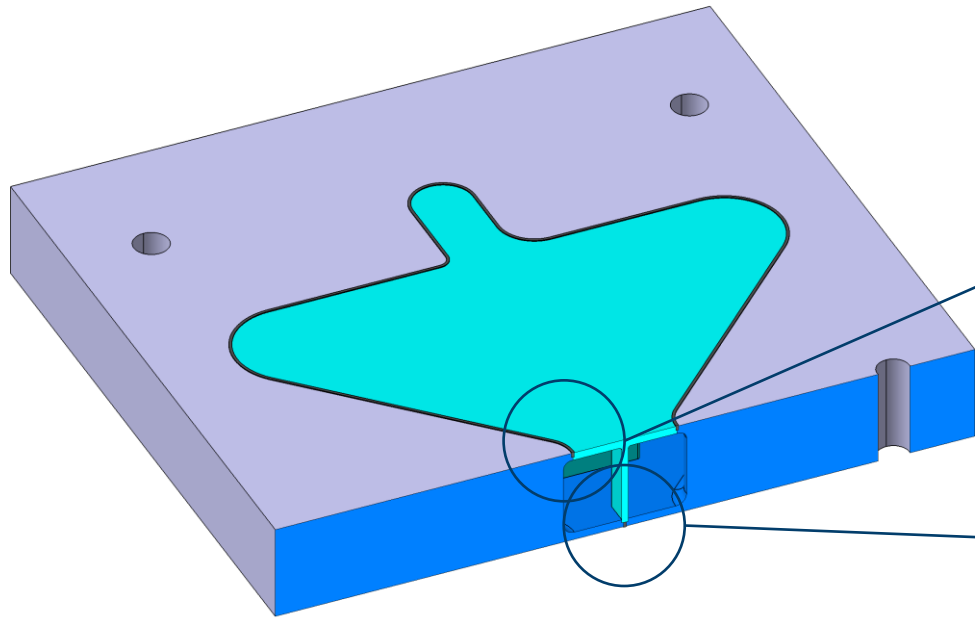
- Milled from solid block of Al6061 T651



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Cold Moderator BF1 – Manufacturing

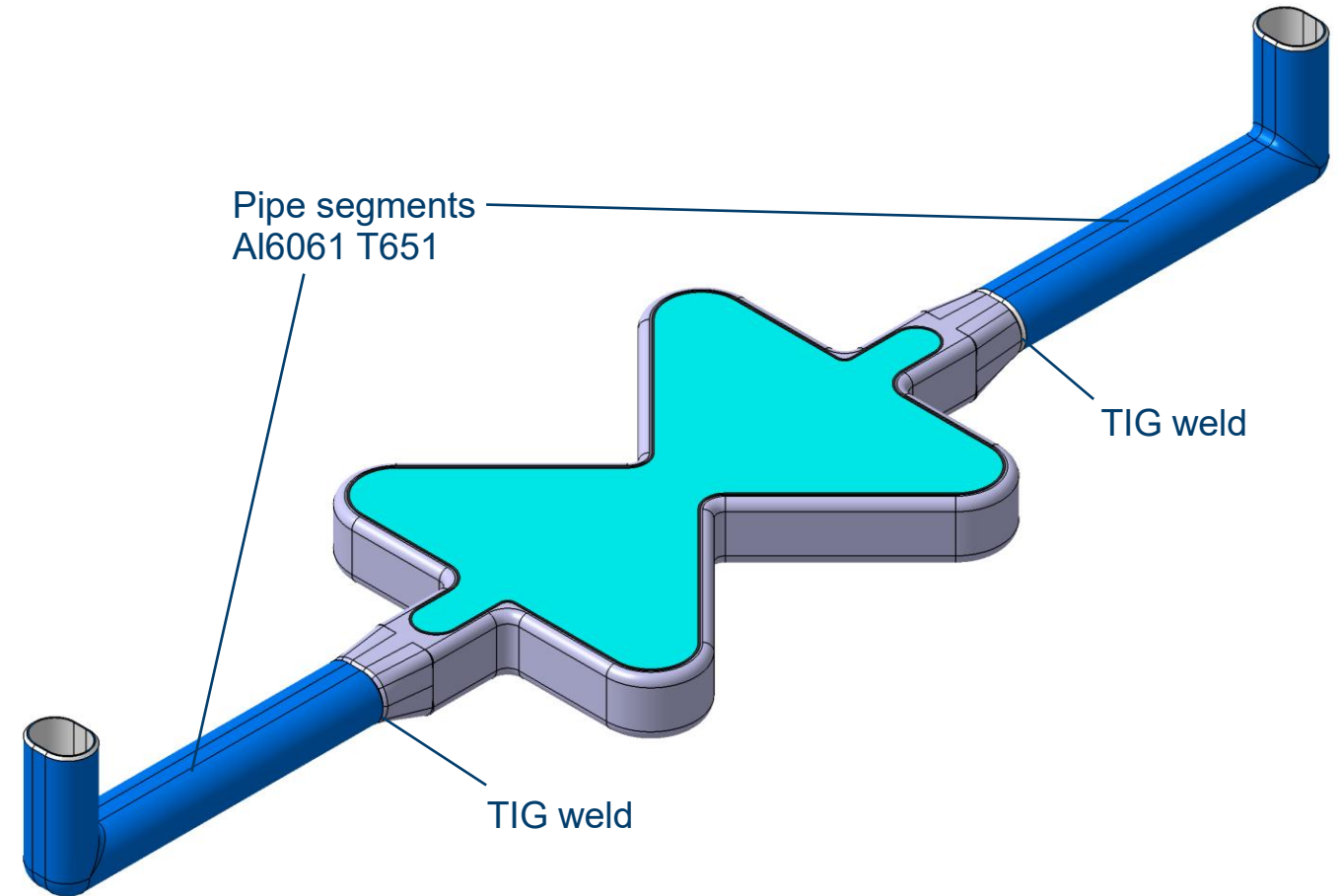
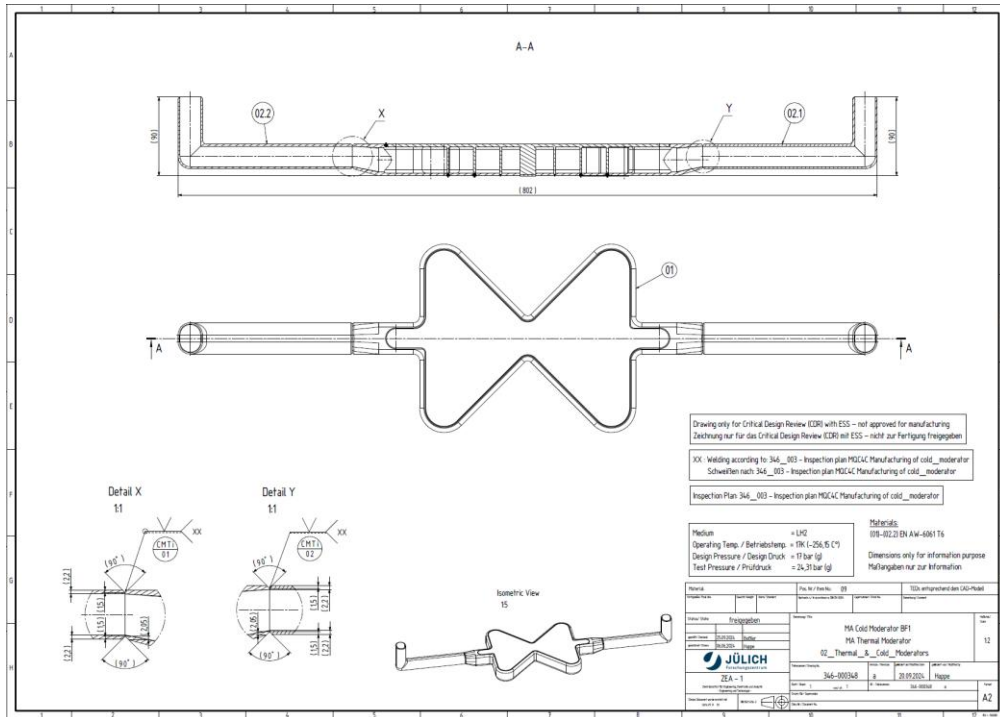
- EB welding circumferential at the top side
- EB welding of the flow guides at the bottom



DESIGN SOLUTION MRP-II

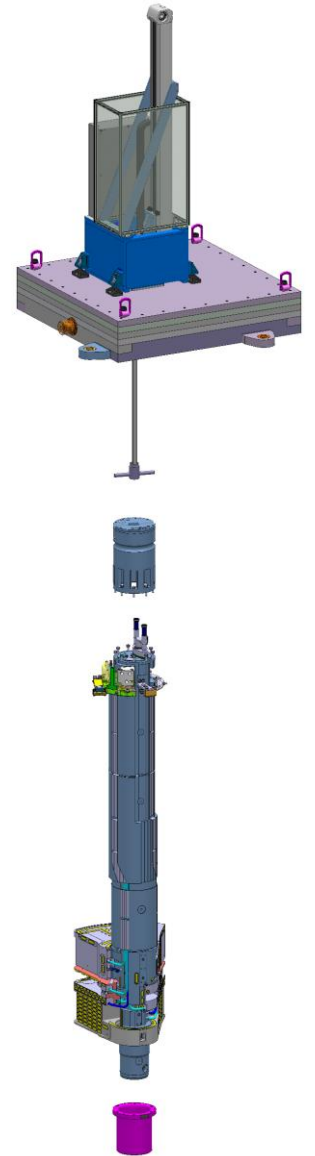
Cold Moderator BF1 – Manufacturing

- TIG welding of pipe connections



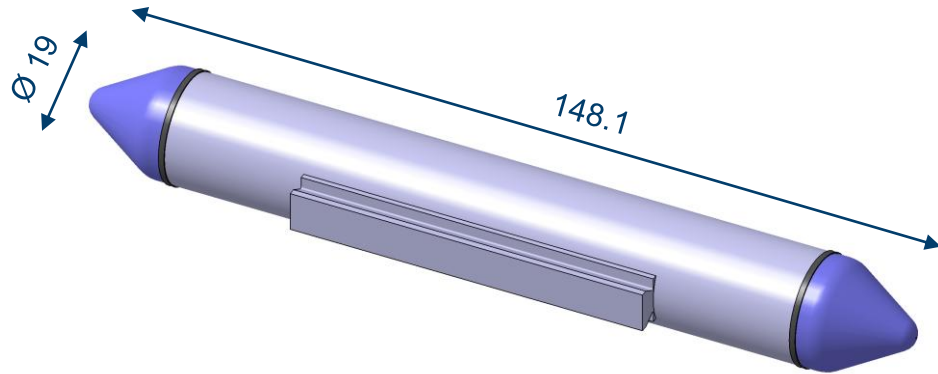
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DESIGN SOLUTION MRP-II

Irradiation Module – Overview

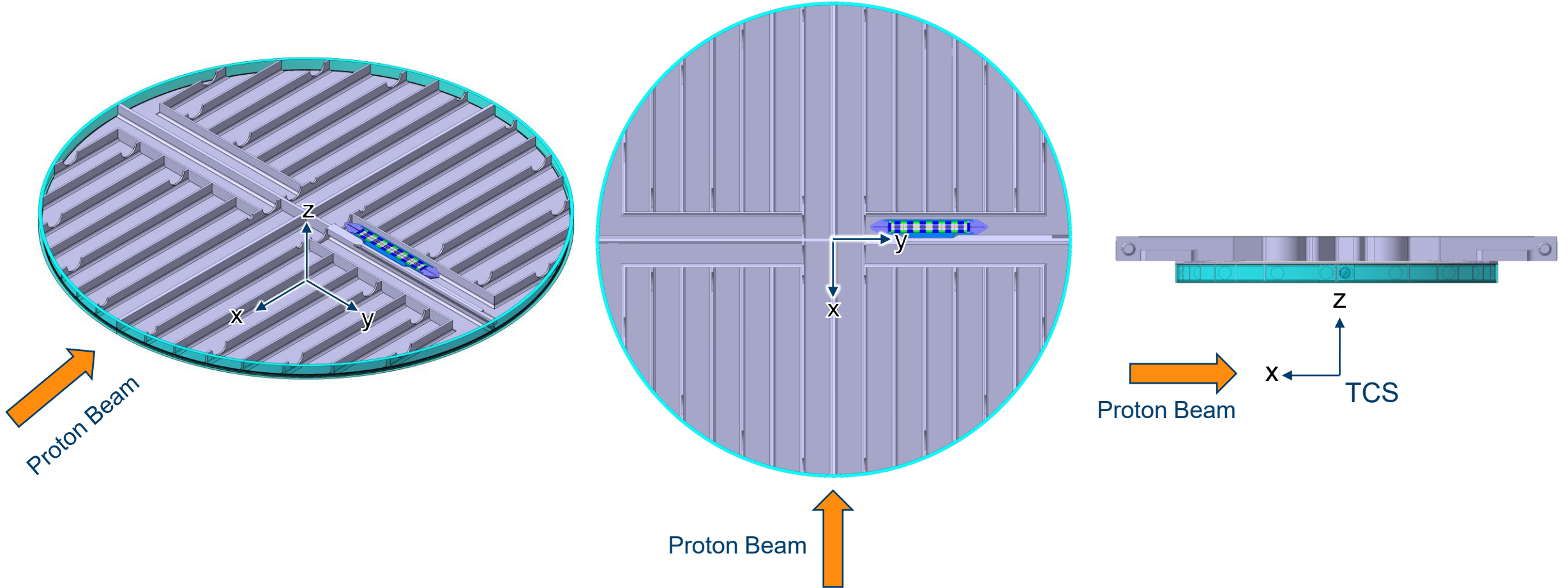


- Small vessel installed inside the Thermal Moderator
- Passively cooled by the Thermal Moderator water flow
- Exposed to fast & thermal neutrons and dedicated to the study of radiation damage of the enclosed materials
- Filled with helium (He) at a pressure of 1 bar to increase the thermal conductivity
- $m = 120$ g

DESIGN SOLUTION MRP-II

Irradiation Module – Overview

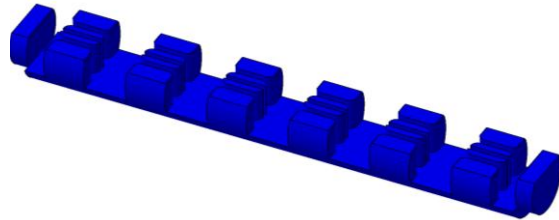
- Location inside the Thermal Moderator Water Disc in relation to the TCS of $X=-16$ mm; $Y=120$ mm; $Z=96$ mm



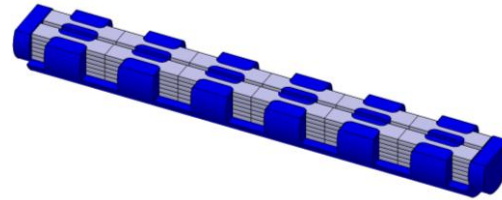
DESIGN SOLUTION MRP-II

Irradiation Module – Assembly

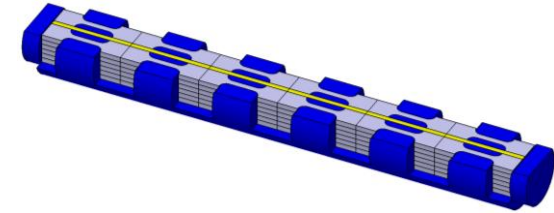
Specimen Holder Al5083



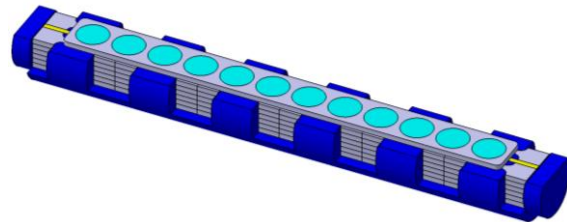
12 x 6 Tensile Specimen



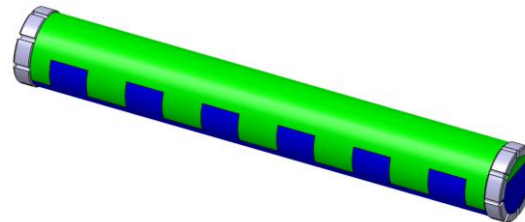
6 x 6 EC Samples



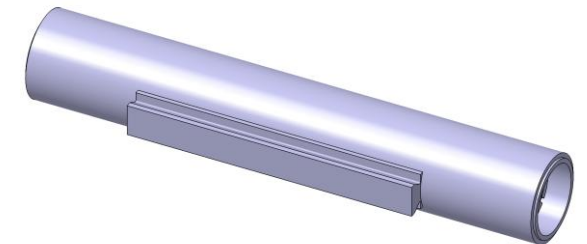
3 x 4 LFA Samples



Closing of Sample Holder Al5083



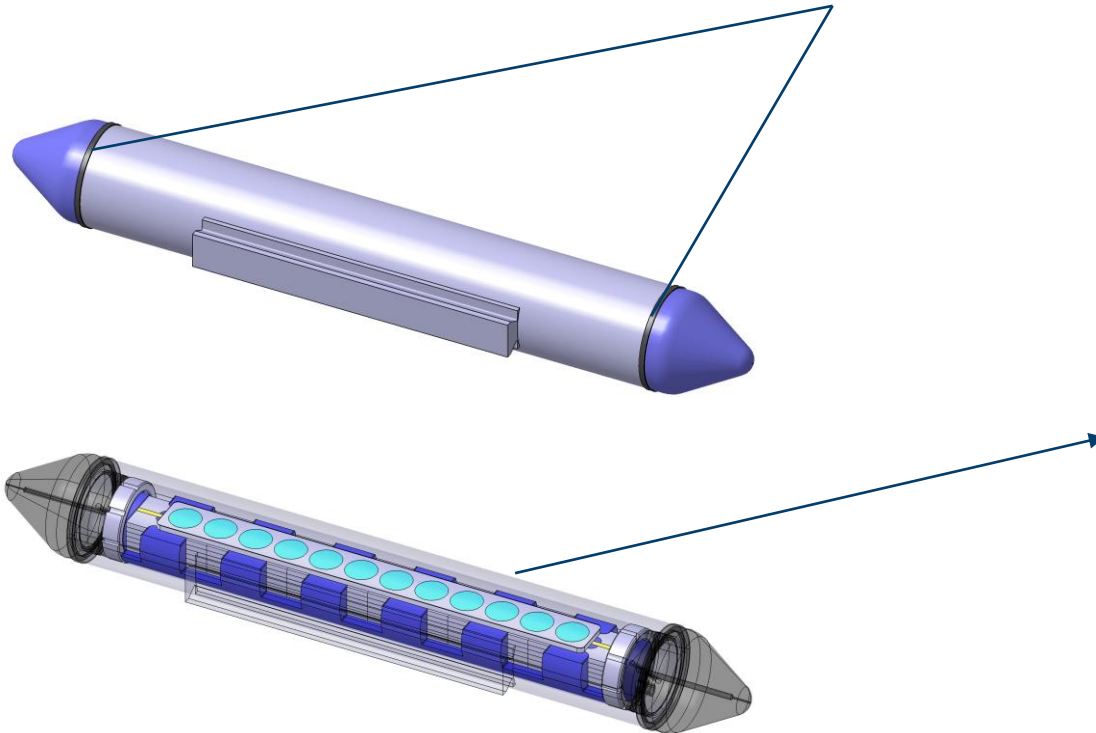
Insertion in Outer Vessel Al6061 T651



DESIGN SOLUTION MRP-II

Irradiation Module – Assembly

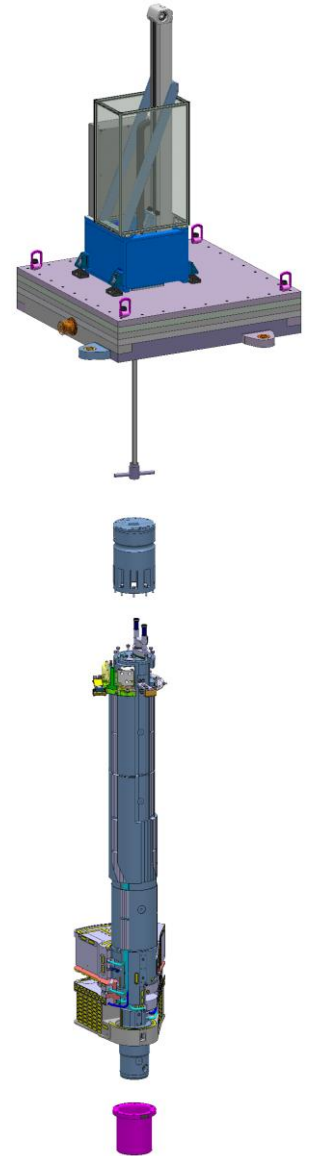
- EB welding of Vessel Tips Al6061 T651 and Al4047 Filler



Material	Number of samples	ID	Laser Marking
Tensile samples			
Al6061 T651	6	Mat-01	20.1 – 20.6
Al5754 O	6	Mat-02	21.1 - 21.6
Al6061 T651 with filler material Al4047	6	Mat-03	28.1 – 28.6
Inconel 718	6	Mat-04	32.1 – 32.6
Ti6Al4V	6	Mat-05	29.1 – 29.6
3D printed Al6061 T6	6	Mat-06	25.1 – 25.6
Stainless Steel 304L	6	Mat-07	22.1 – 22.6
Stainless Steel 316L	6	Mat-08	23.1 – 23.6
1.3912+Al6061 (friction welded)	6	Mat-09	33.1 – 33.6
Invar 36 (1.3912)	6	Mat-10	34.1 – 34.6
3D printed AL	6	Mat-11	24.1 – 24.6
Al6061 T651	6	Mat-12	20.7 – 20.12
EC samples			
EC samples Al6061 T651	6	Mat-01	40.1 – 40.6
EC samples Al5754 O	6	Mat-02	41.1 – 41.6
EC samples SS316L	6	Mat-08	42.1 – 42.6
Silicon Carbide Temperature Monitors	18	Mat-13	43.1 – 43.18
LFA samples			
LFA Al6061 T651	4	Mat-01	50.1 – 50.4
LFA Al5754 O	4	Mat-02	51.1 – 51.4
LFA SS316L	4	Mat-08	52.1 – 52.4

CONTENT

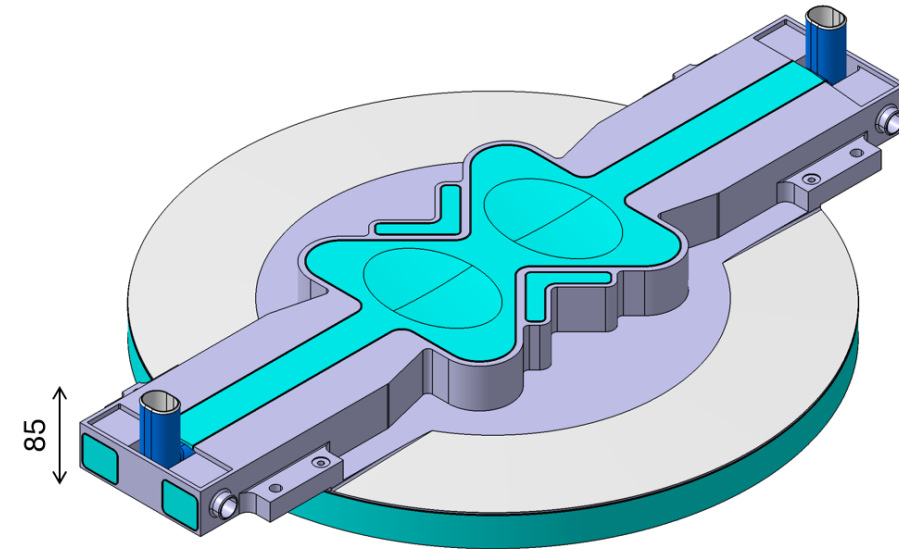
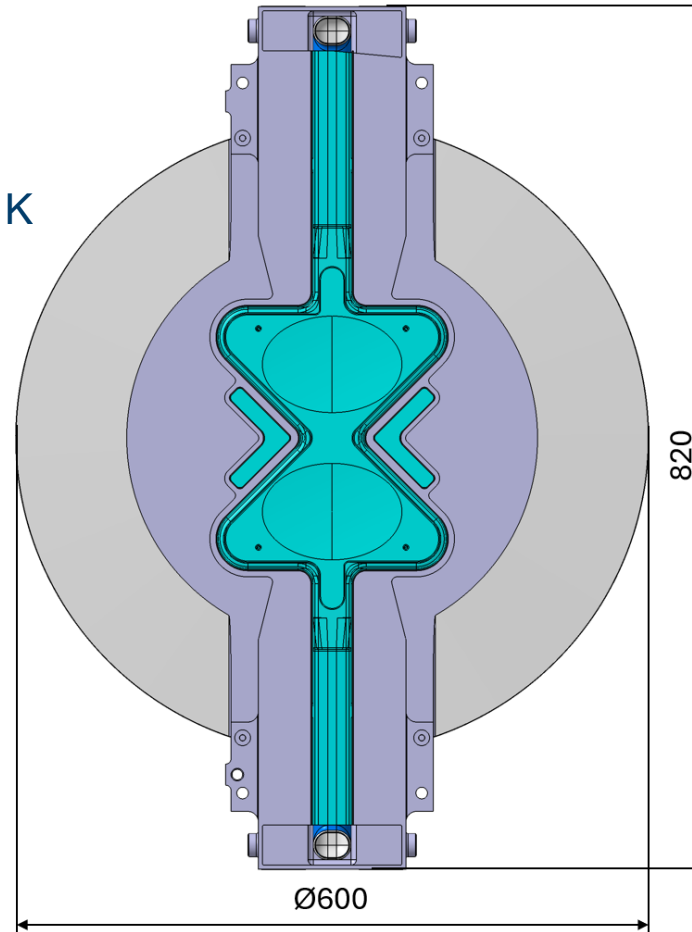
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DESIGN SOLUTION MRP-II

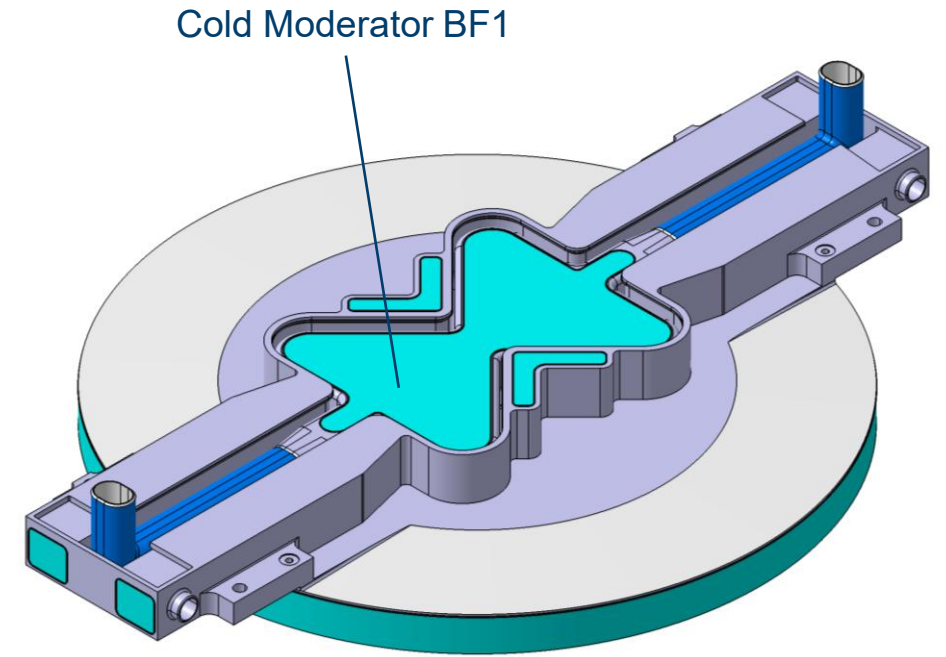
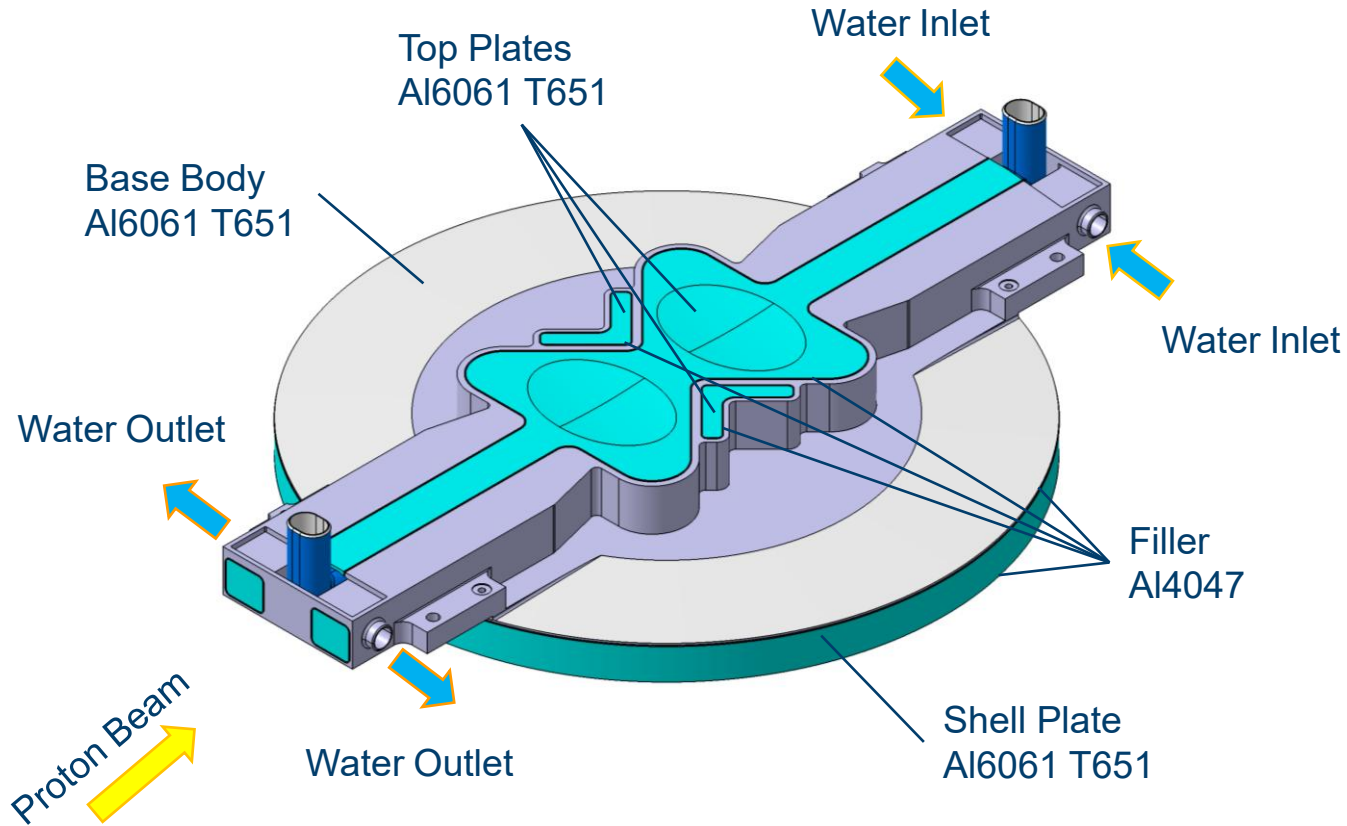
Thermal Moderator – Overview

- Pressure vessel made of Al6061 T651
- EB welded with filler material Al4047
- Light water at an inlet temp. of $T_{in} = 293.15 \text{ K}$ with a temp. increase of $dT \leq 16 \text{ K}$
- Design pressure 5 bar
- Operating pressure 4 bar
- Heat deposition of ca. 79 kW
- $m_{Al} = 12.5 \text{ kg}$ (without CM & water)
- Mostly 3 & 4 mm wall thickness



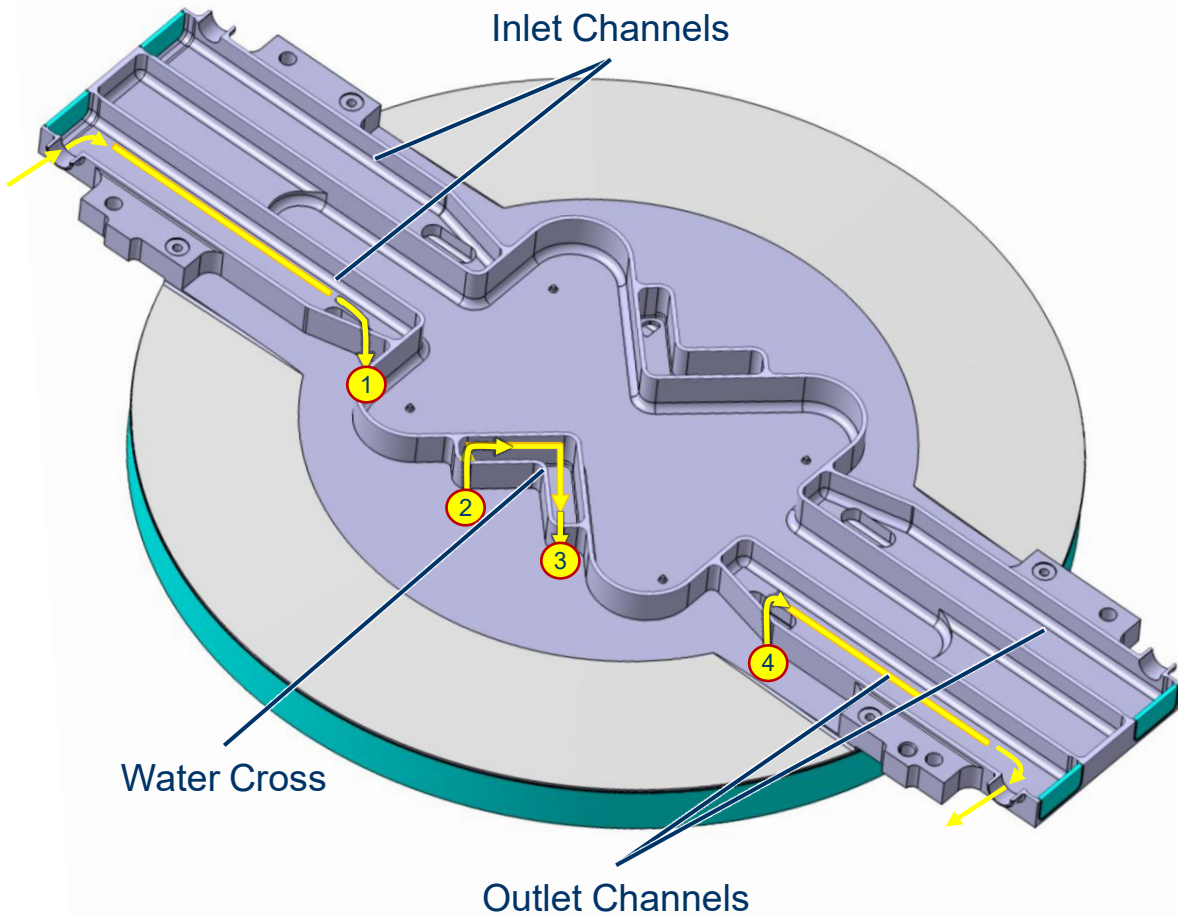
DESIGN SOLUTION MRP-II

Thermal Moderator – Overview

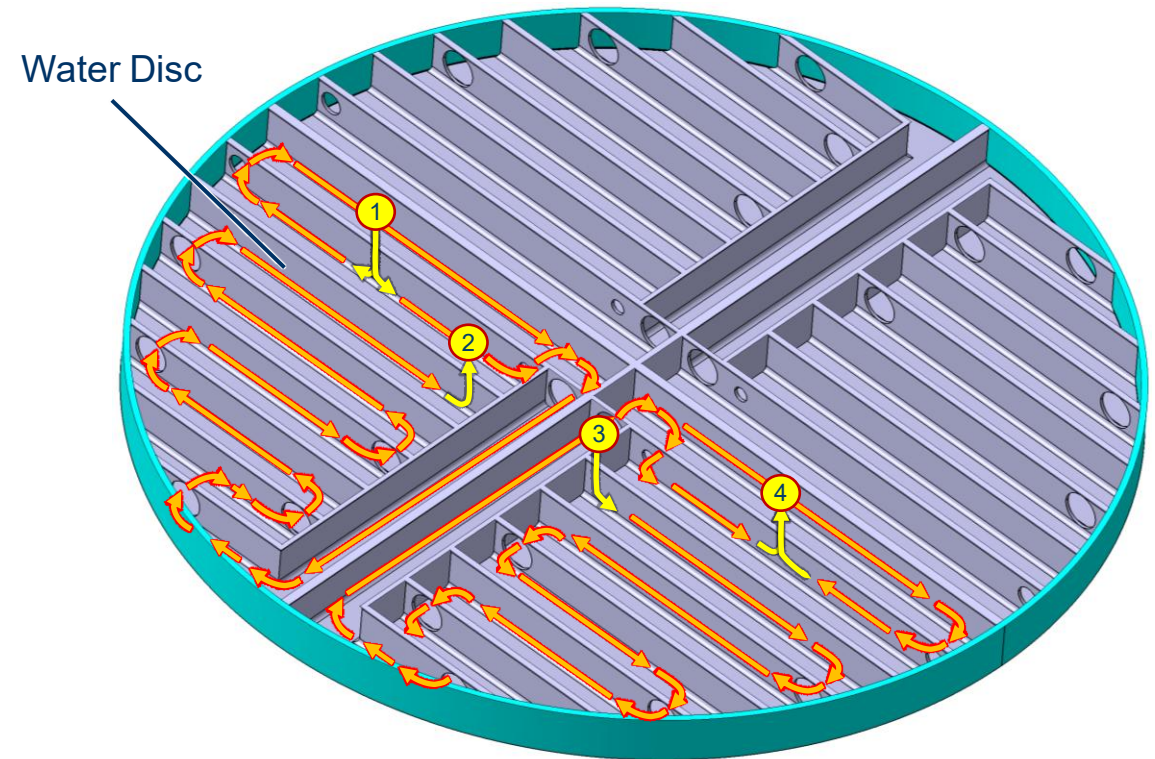


DESIGN SOLUTION MRP-II

Thermal Moderator – Waterflow



- ① From Inlet Channels down to Water Disc
- ② From Water Disc up to Water Cross
- ③ From Water Cross down to Water Disc
- ④ From Water Disc up to Outlet Channels



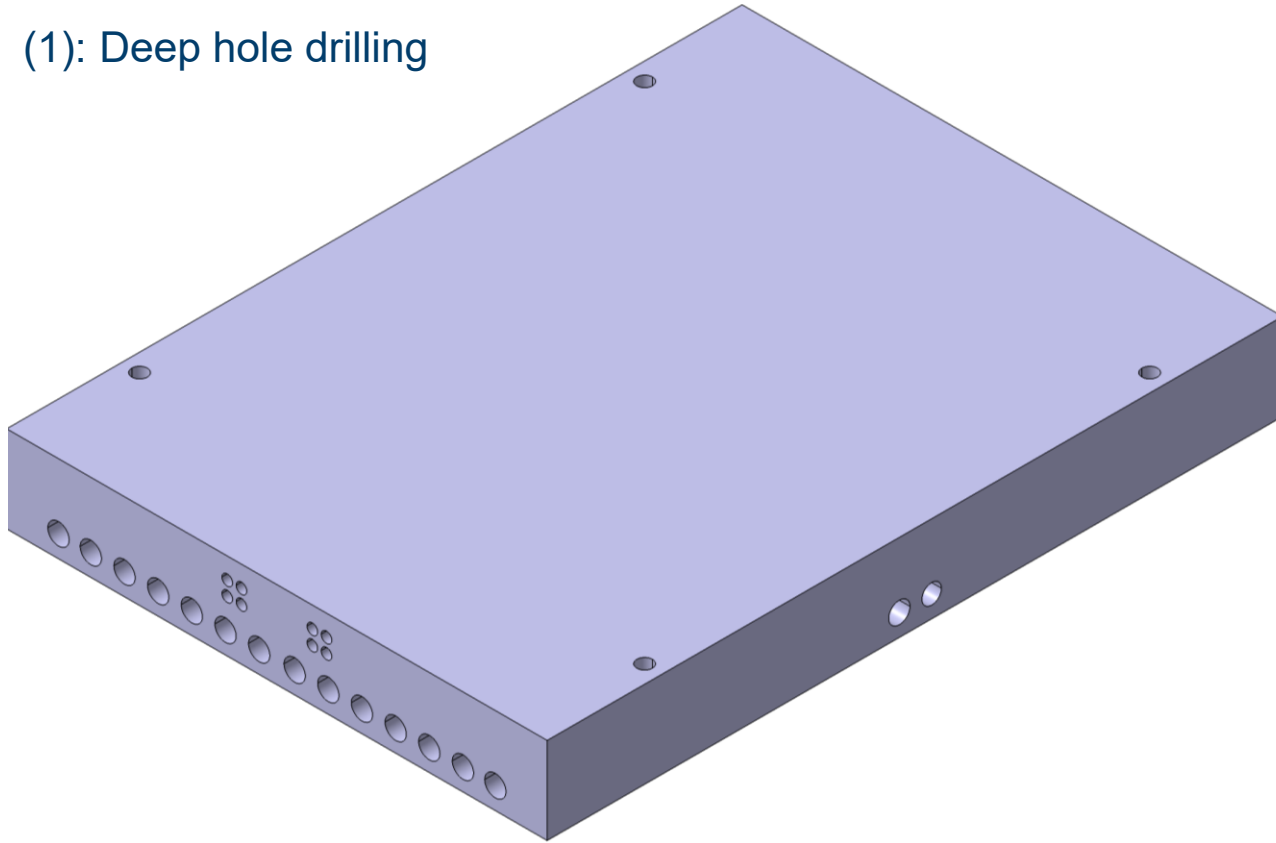
Original schematics: 6-346-PPT-20241015-YBessler-JWolters-Thermal-Hydraulic and Thermo-Mechanical Design of the Thermal Moderator

DESIGN SOLUTION MRP-II

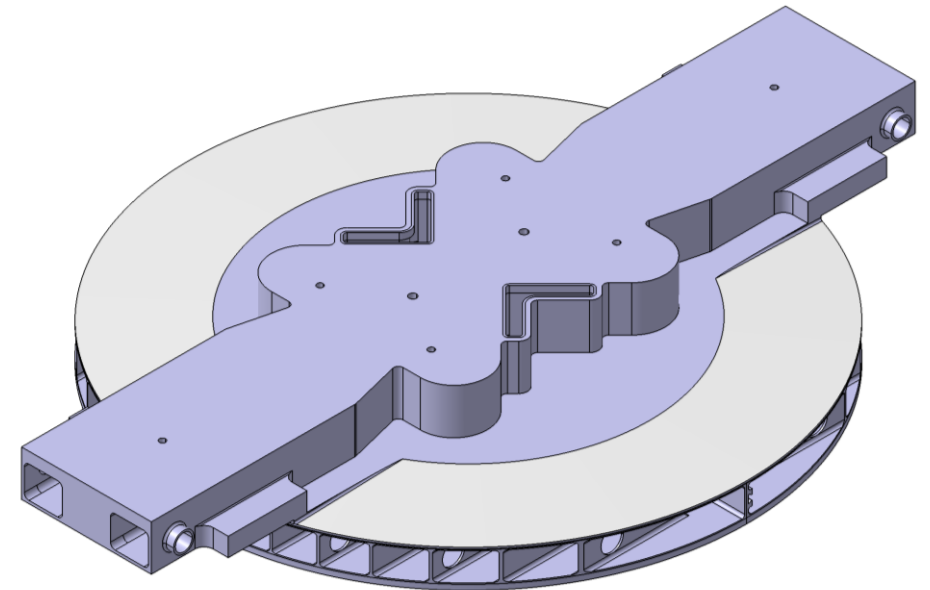
Thermal Moderator – Manufacturing

- Solid block Al6061 T651
- 7 main manufacturing steps for final product

(1): Deep hole drilling



(2): Milling of the outer contour
(3): EDM of water channels

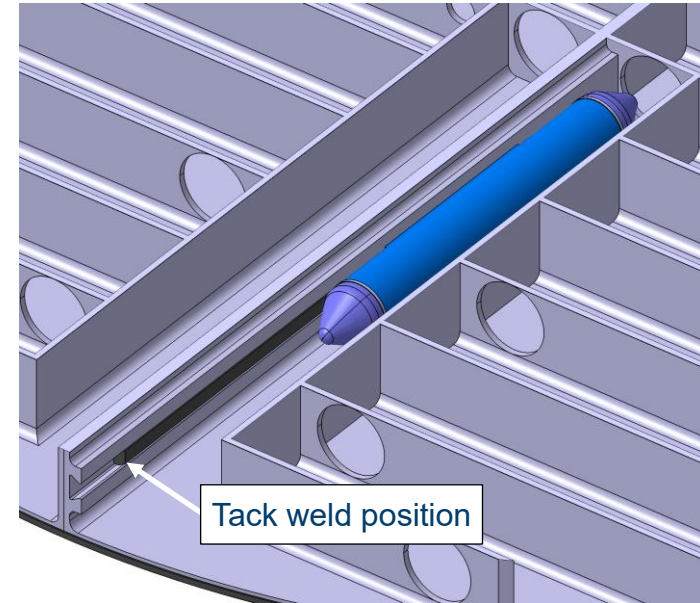
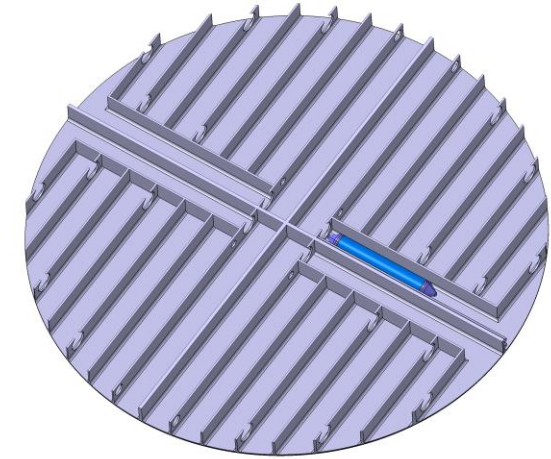
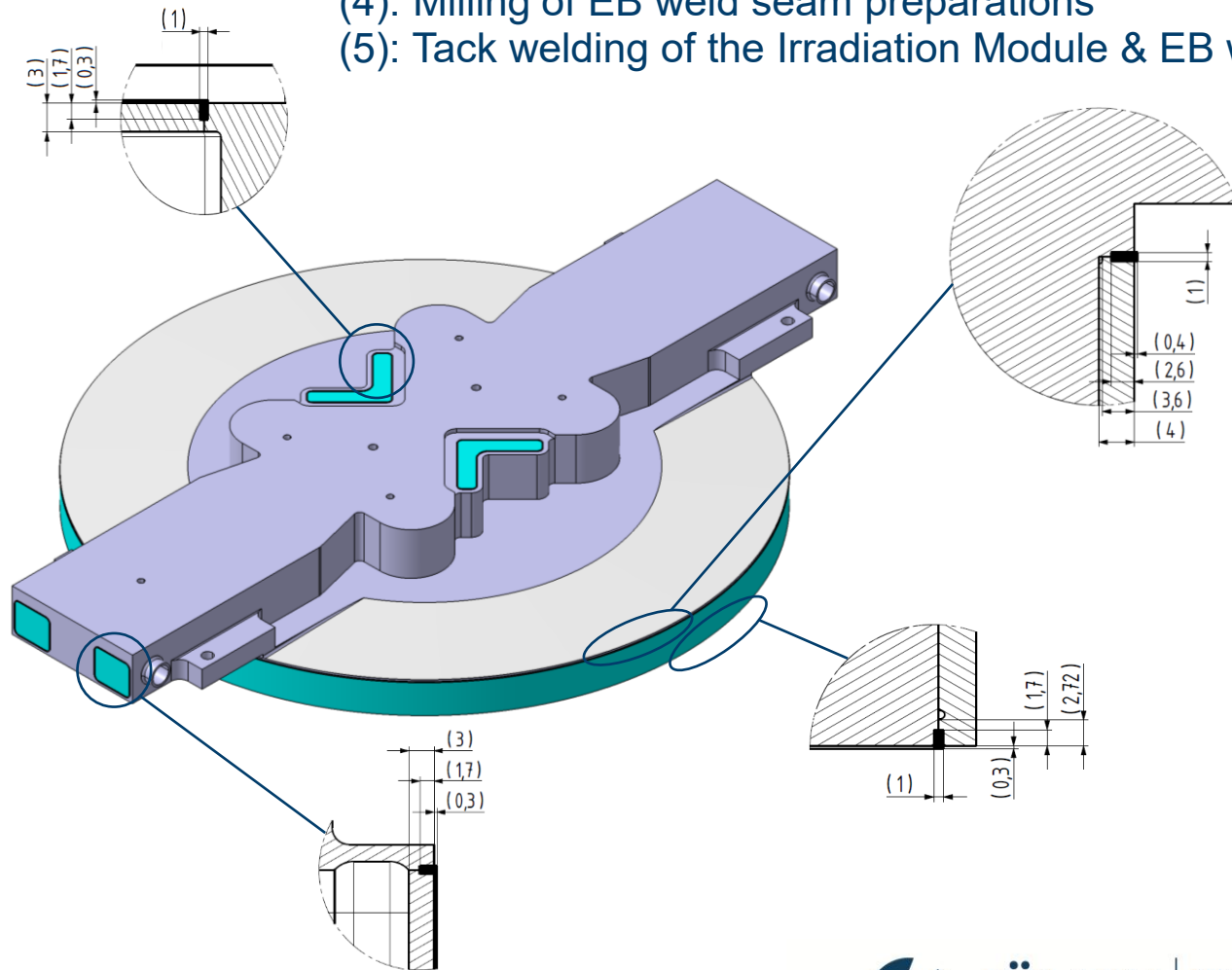


DESIGN SOLUTION MRP-II

Thermal Moderator – Manufacturing

(4): Milling of EB weld seam preparations

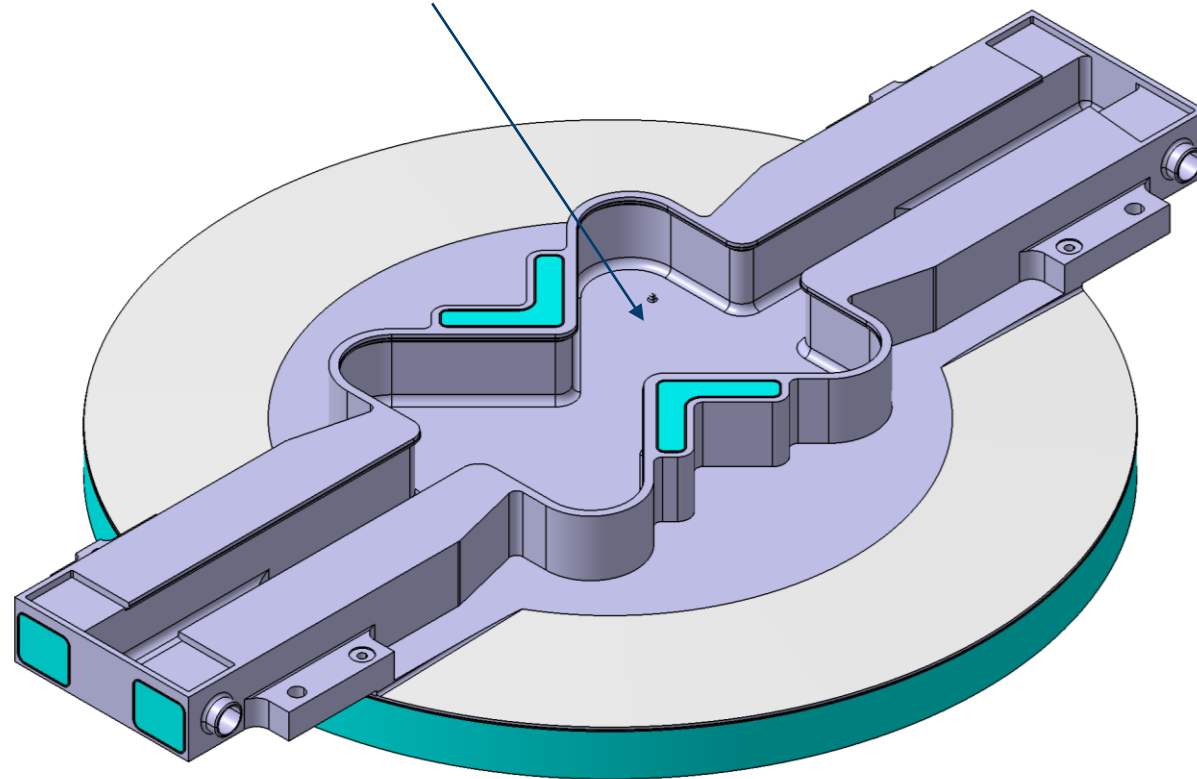
(5): Tack welding of the Irradiation Module & EB welding of water channels



DESIGN SOLUTION MRP-II

Thermal Moderator – Manufacturing

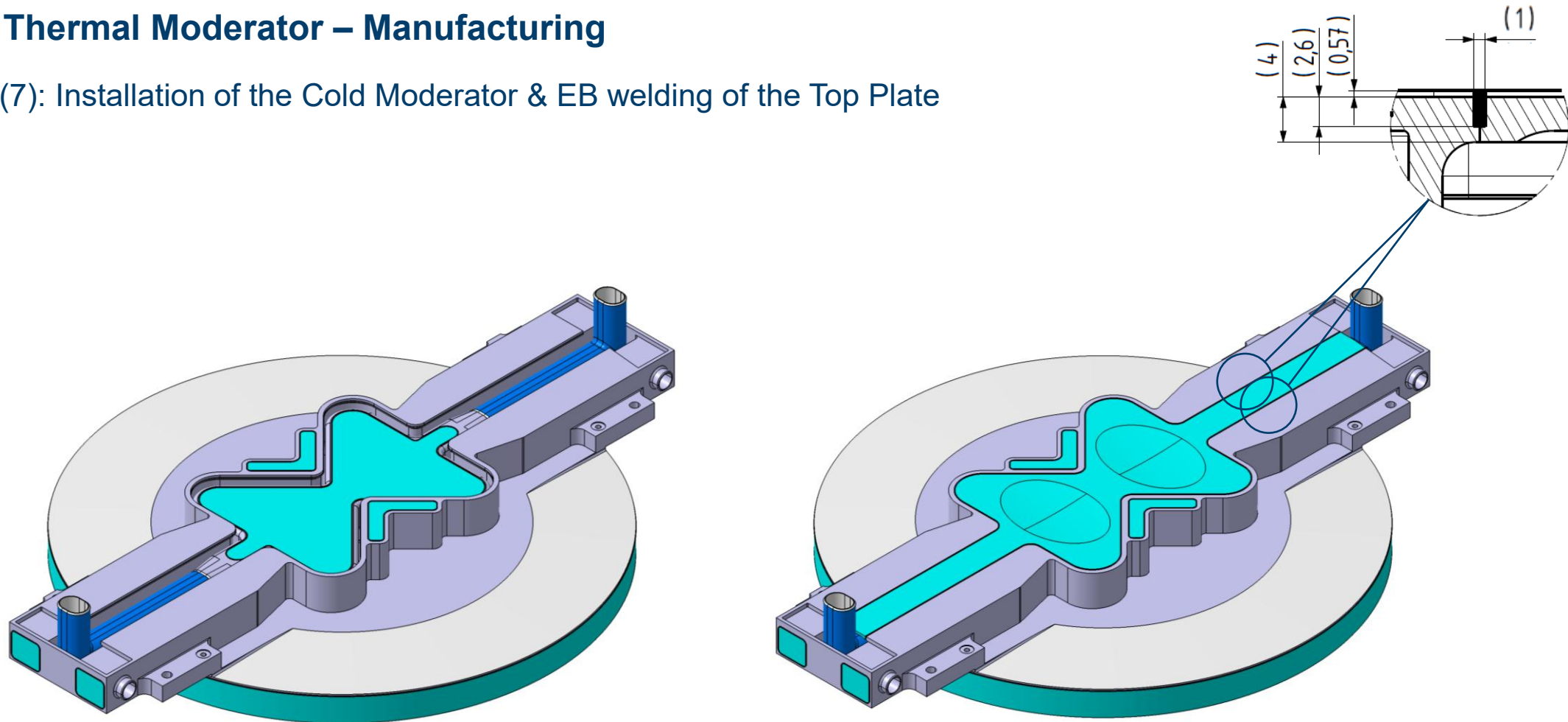
(6): Final milling of inner cavity for the Cold Moderator



DESIGN SOLUTION MRP-II

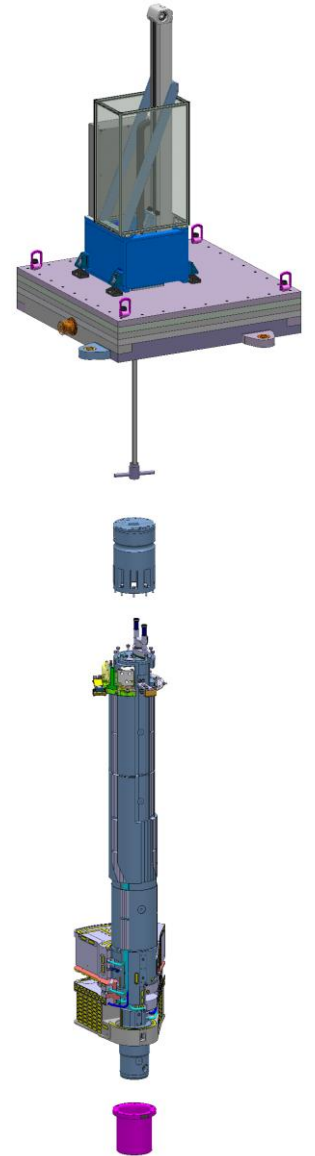
Thermal Moderator – Manufacturing

(7): Installation of the Cold Moderator & EB welding of the Top Plate



CONTENT

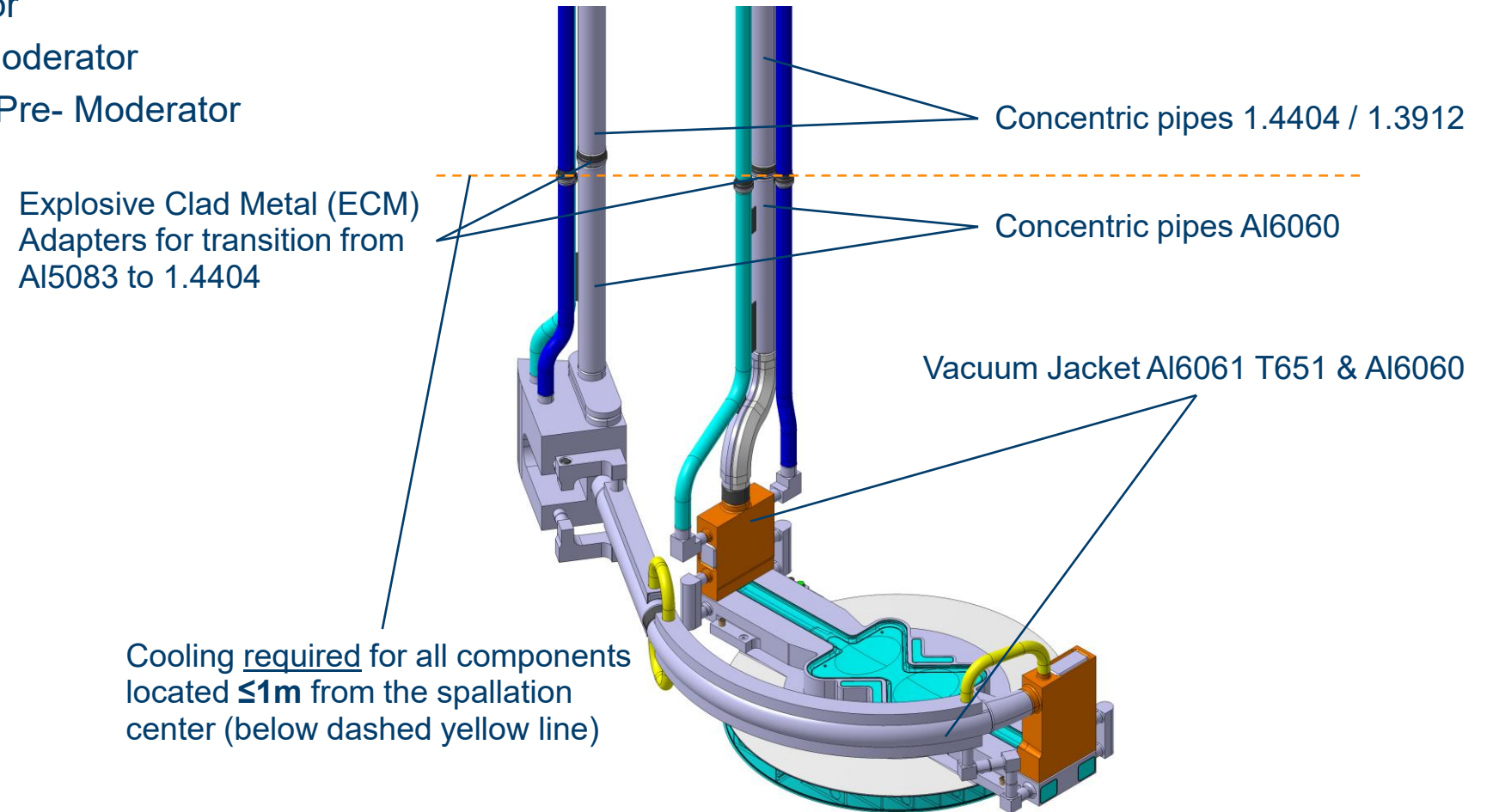
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DESIGN SOLUTION MRP-II

Vacuum Jackets & Vacuum Chamber

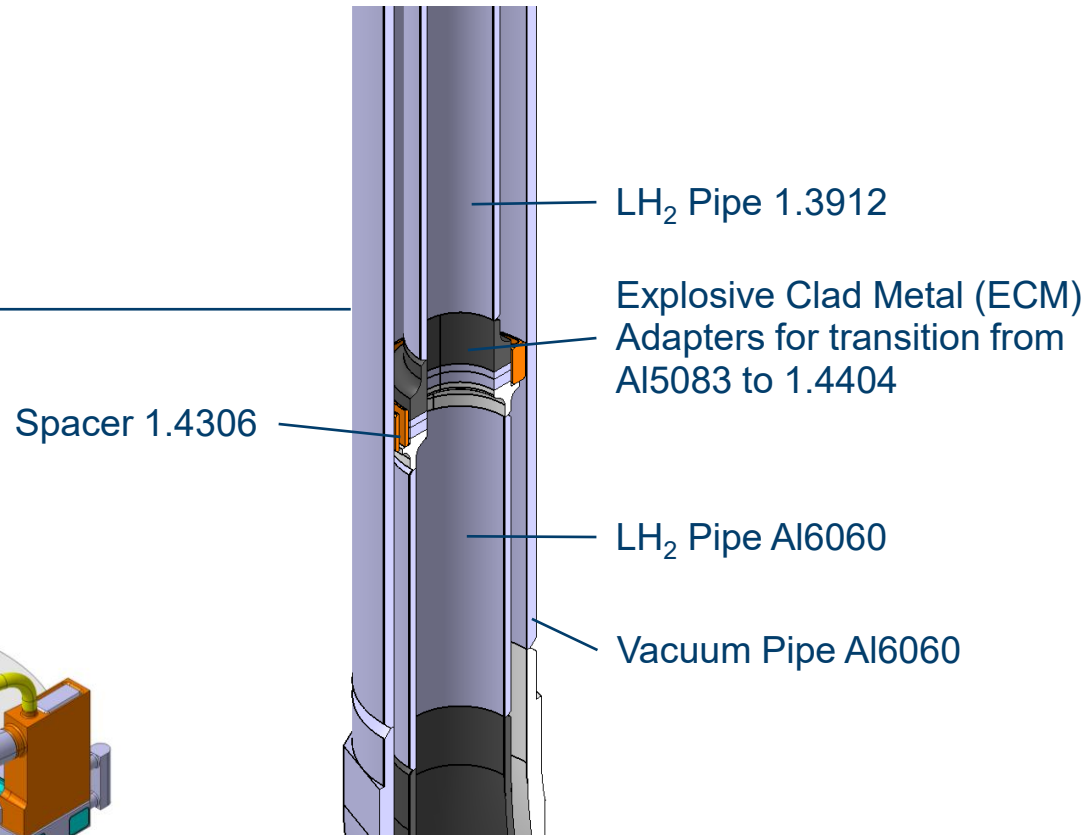
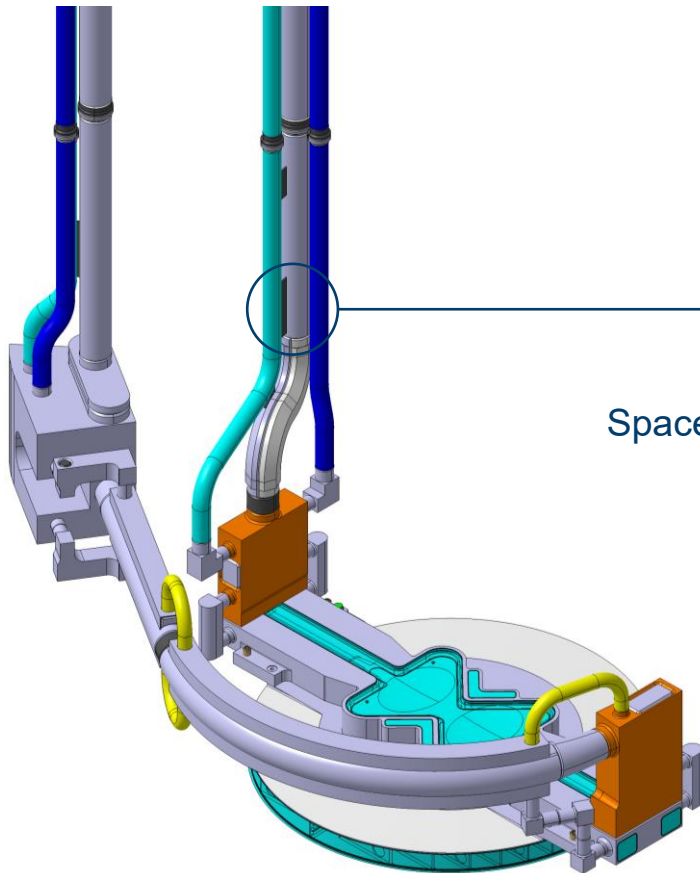
- LH₂ supply for Cold Moderator
- Insulation vacuum for Cold Moderator
- Water supply for Thermal- & Pre- Moderator



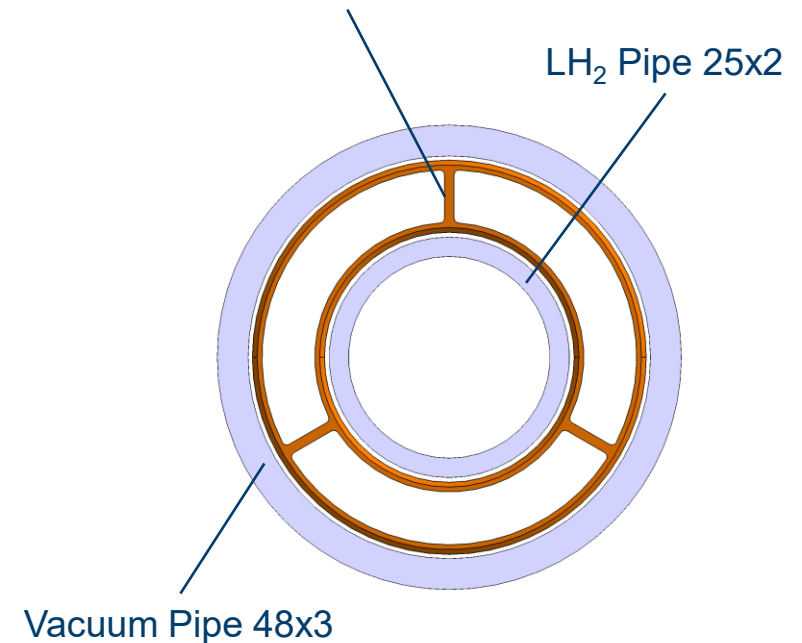
DESIGN SOLUTION MRP-II

Vacuum Jackets & Vacuum Chamber

- Concentric pipes with spacers to center the position of the inner pipe
- Optimized heat transfer by minimized usage of material for the spacers
- Explosion Clad Adapters used for the transition from SS or Invar to Al



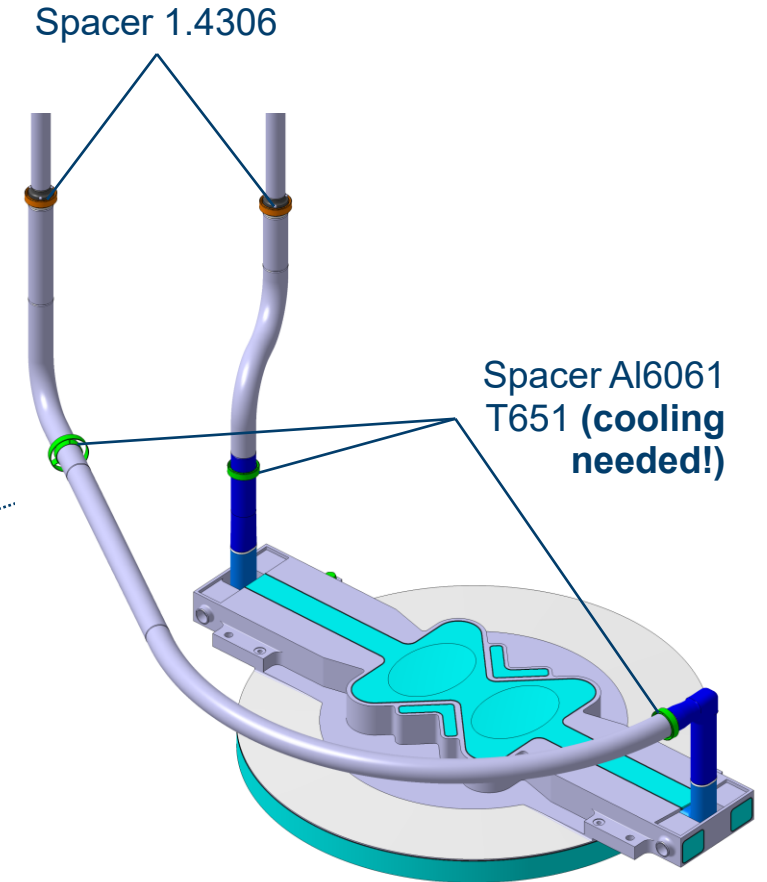
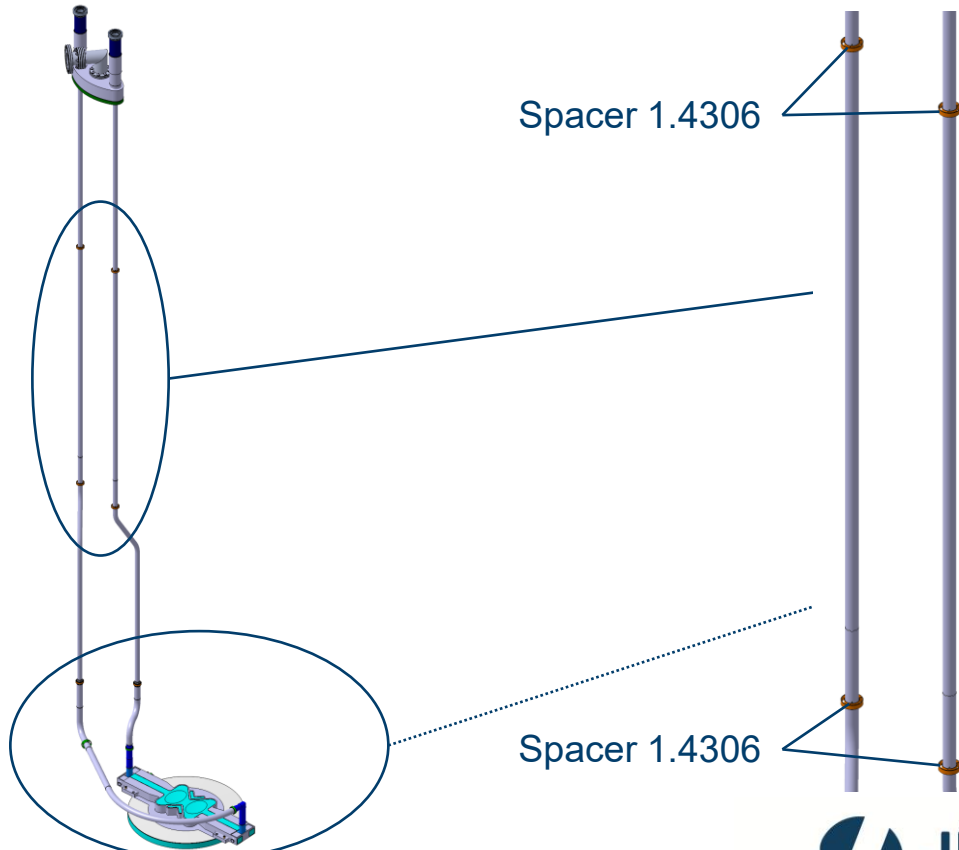
Spacer 1.4306 / Al6061 T651 (see next slide)



DESIGN SOLUTION MRP-II

Vacuum Jackets & Vacuum Chamber

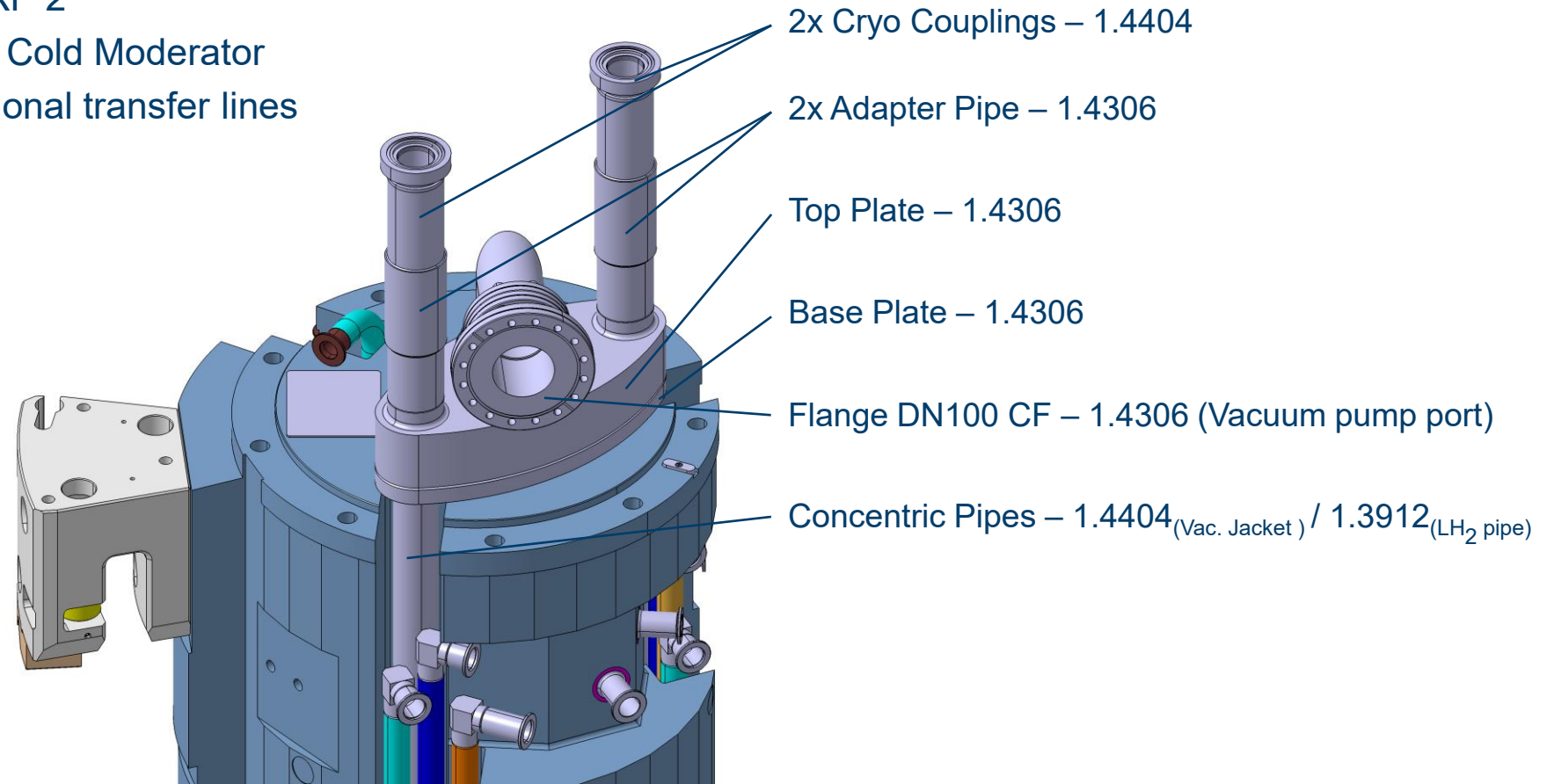
- Reduced heat transfer with stainless steel spacers (orange, no cooling needed)
- Al spacers are used close to the spallation center to reduce particle heat input
- Al spacers (green) are tack welded to the LH₂ pipes to avoid overheating



DESIGN SOLUTION MRP-II

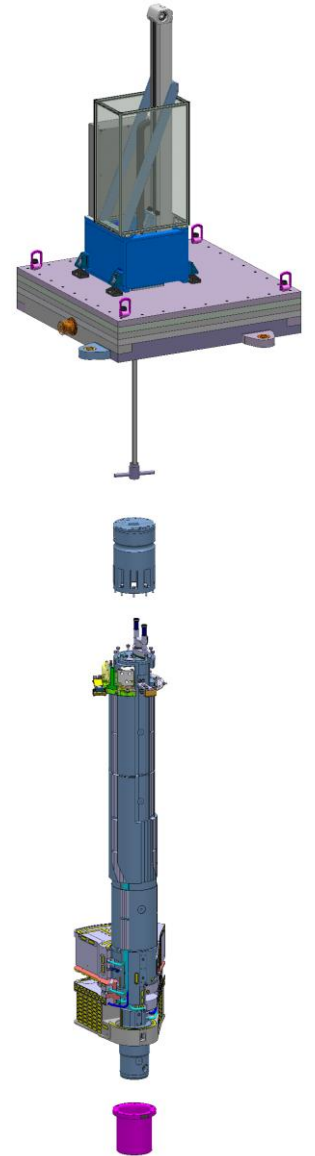
Vacuum Jackets & Vacuum Chamber

- Vacuum Chamber on top of MRP 2
- Provides insulation vacuum for Cold Moderator
- Connection to the LH₂ conventional transfer lines via Cryo Couplings
- m ~ 25 kg



CONTENT

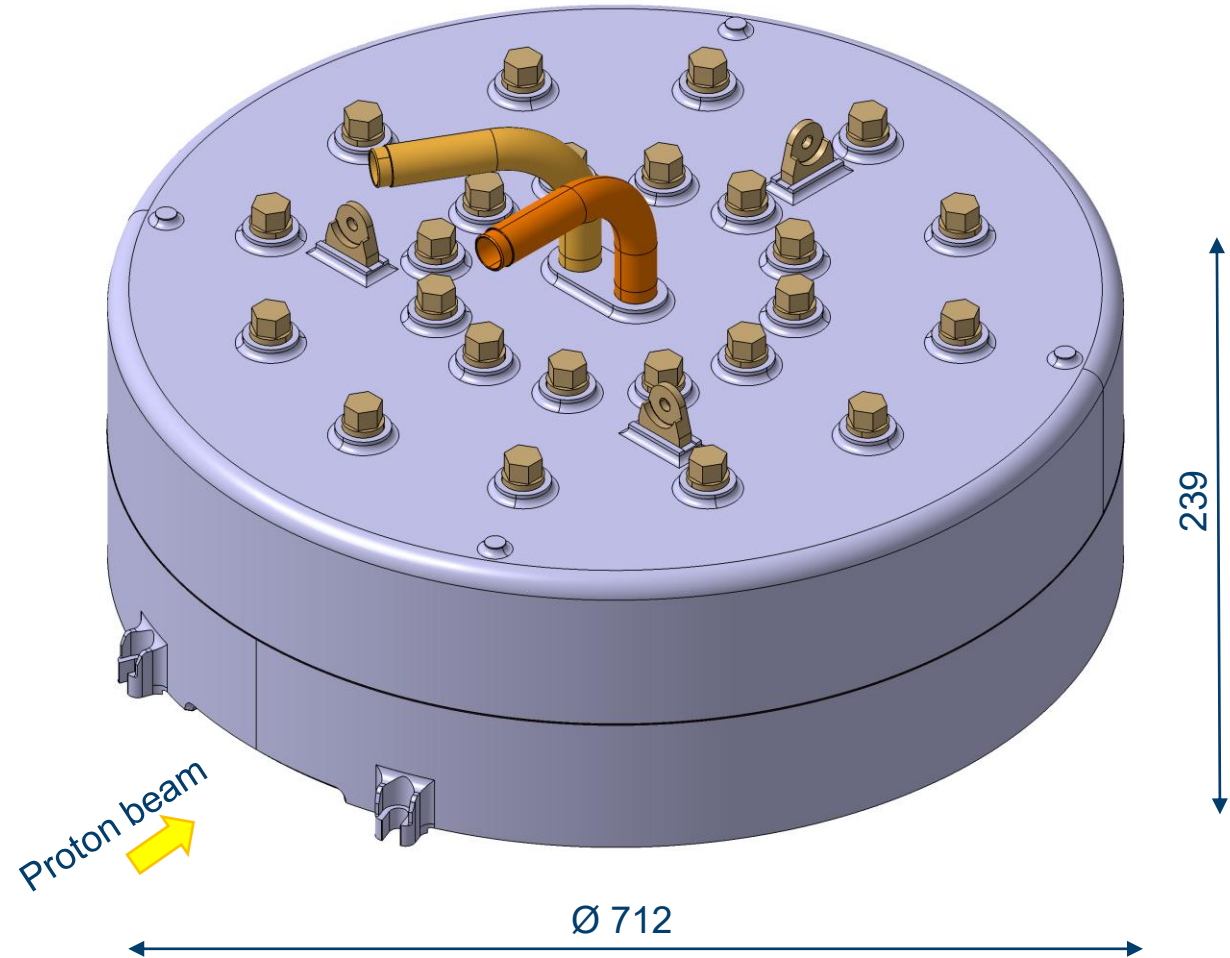
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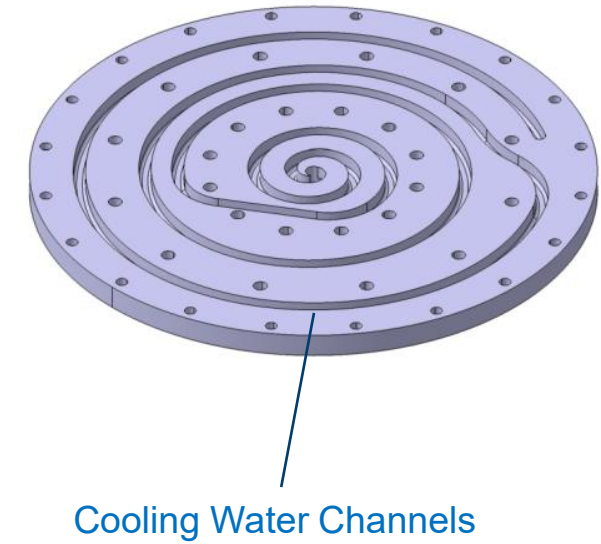
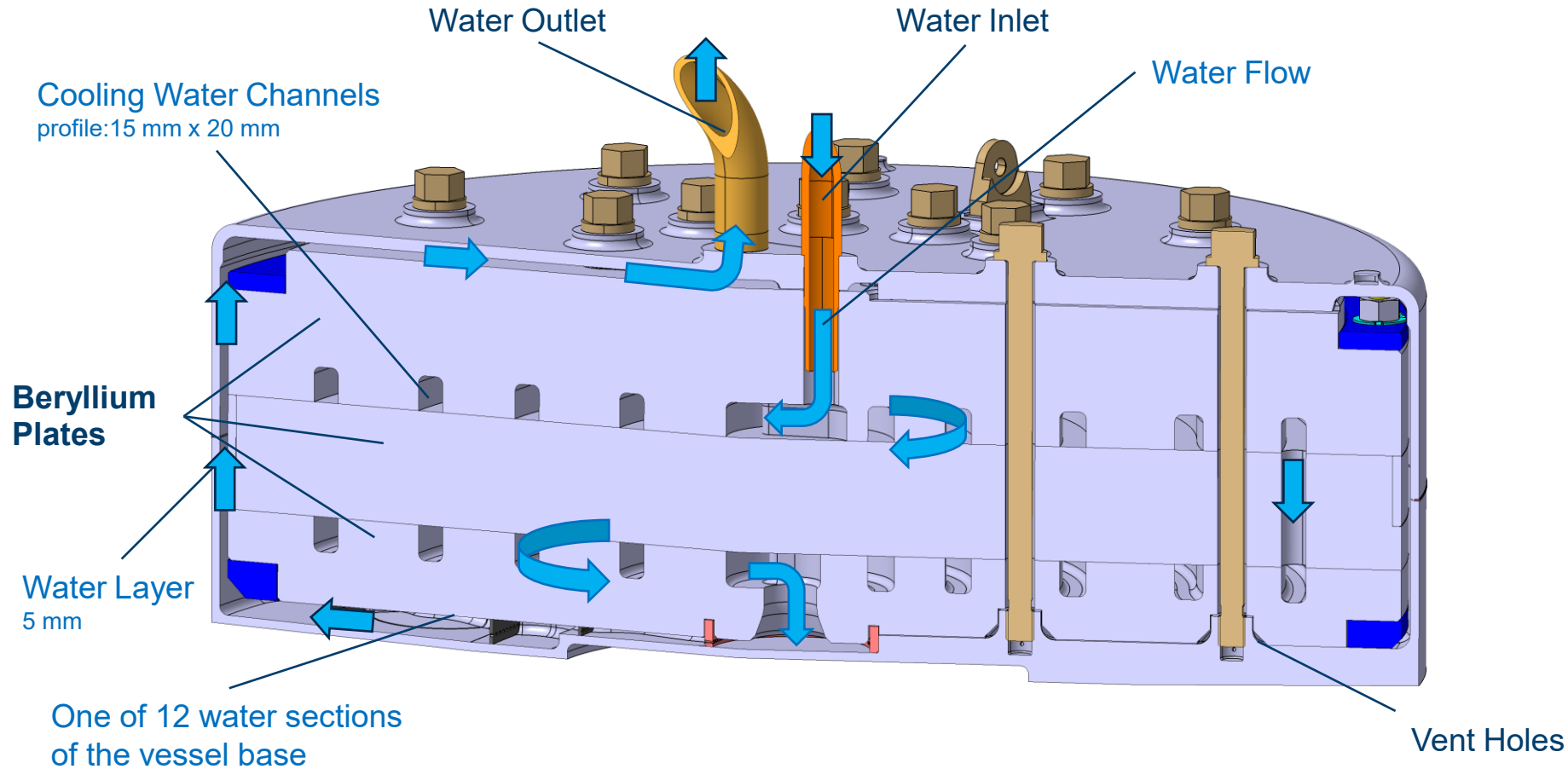
Beryllium Reflector – Overview

- Pressure vessel made of Al6061 T651
- EB welded with filler material Al4047
- Light water at an inlet temp. of $T_{in} = 293.15$ K with a temp. increase of $dT \leq 42$ K
- Design pressure 5 bar
- Operating pressure 4 bar
- Heat deposition of ca. 118 kW
- $m = 177.6$ kg (without water)



DESIGN SOLUTION MRP-II

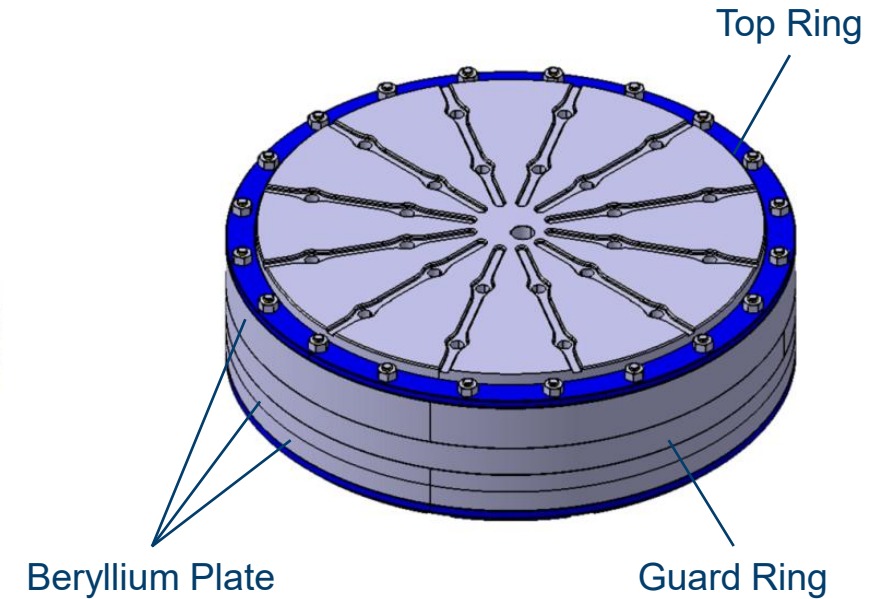
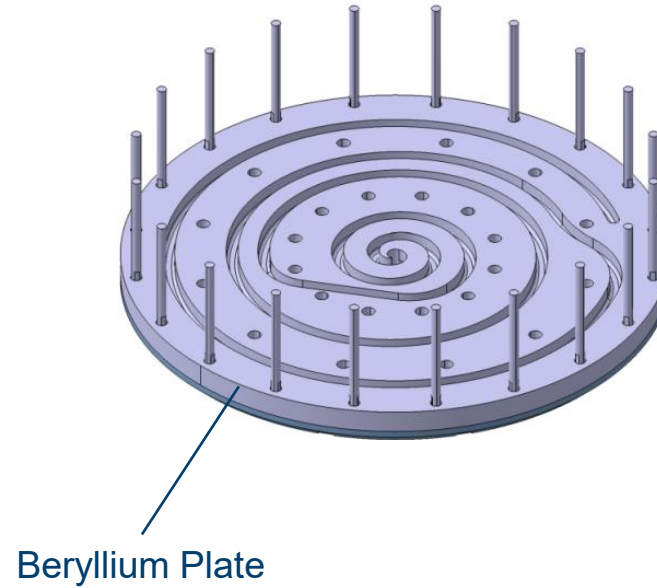
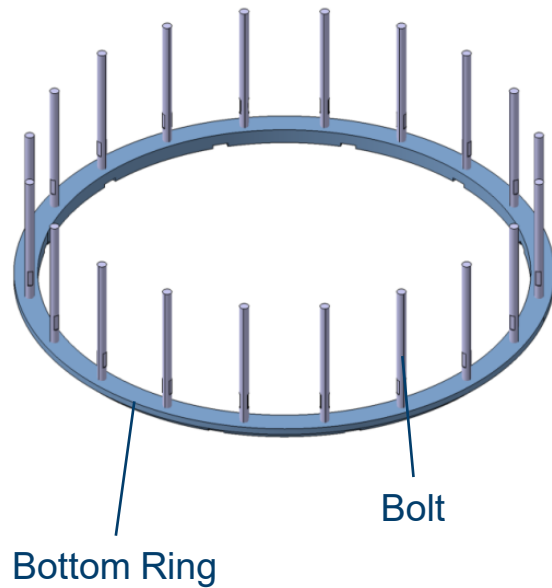
Beryllium Reflector – Waterflow



DESIGN SOLUTION MODERATOR-REFLECTOR SYSTEM

Beryllium Reflector – Assembly

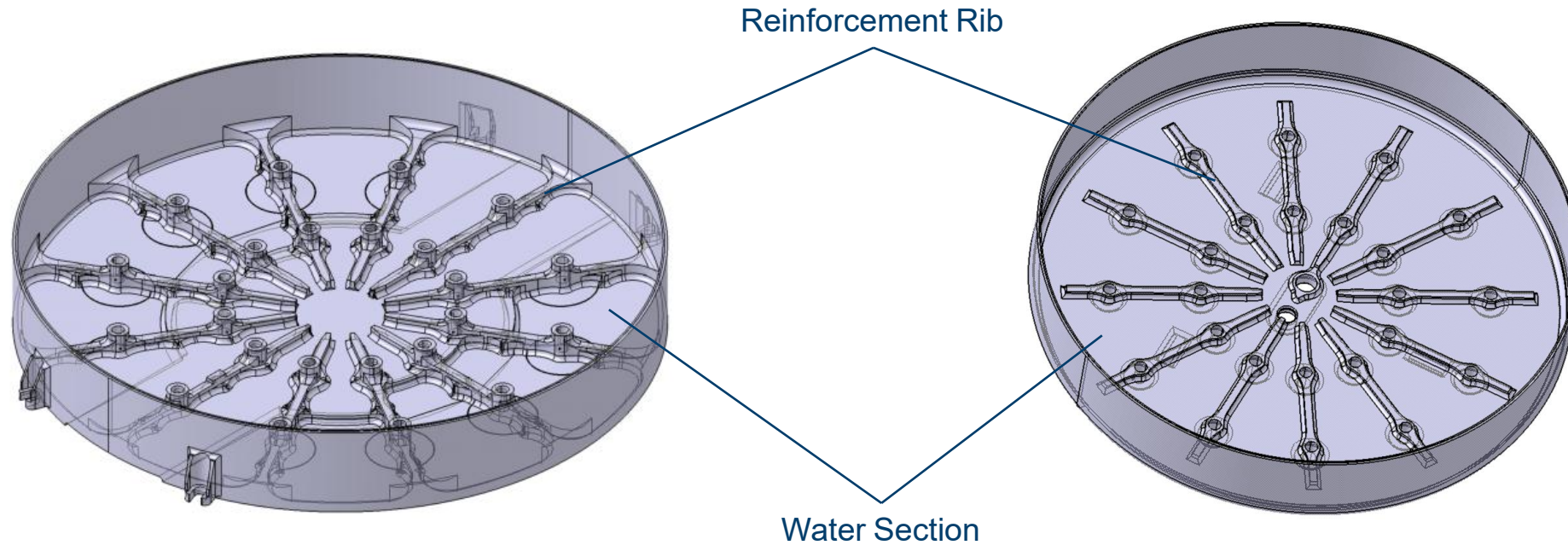
- Stacking of 3 Beryllium Plates
- Guard Ring of Al6061 T651 – protects the Beryllium Plate during EB welding from being hit by the electron-beam
- Stack secured by bolted Bottom & Top Ring



DESIGN SOLUTION MRP-II

Beryllium Reflector – Assembly

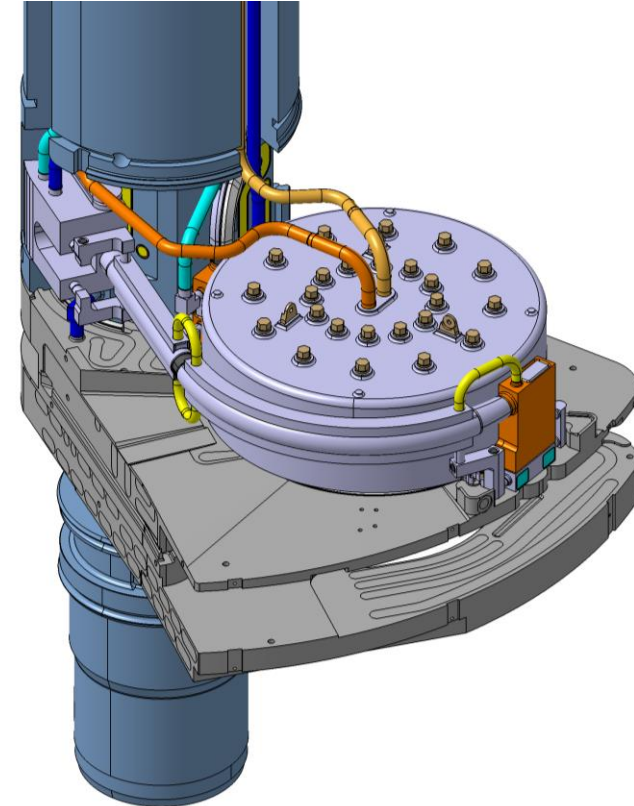
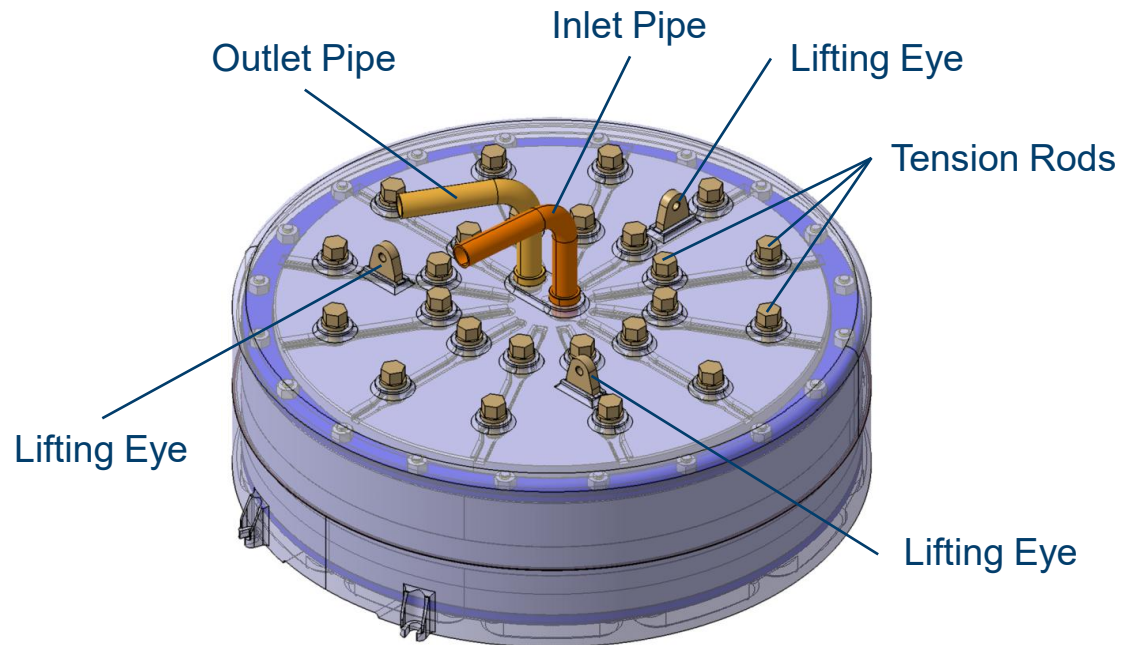
- Vessel Top and Bottom milled from a solid Block of Al6061 T651
- Split into 12 water section by reinforcement ribs



DESIGN SOLUTION MRP-II

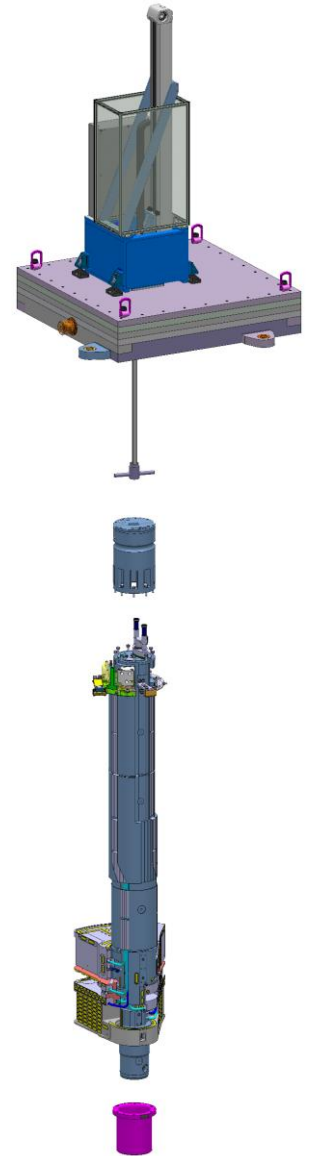
Beryllium Reflector – Assembly

- TIG welding of the 24 tension rods to ensure vessel leak tightness
- TIG welding of the 3 lifting eyes
- TIG welding of the Inlet & Outlet pipes
- Ready for installation to the Main Assembly with Shaft & MS



CONTENT

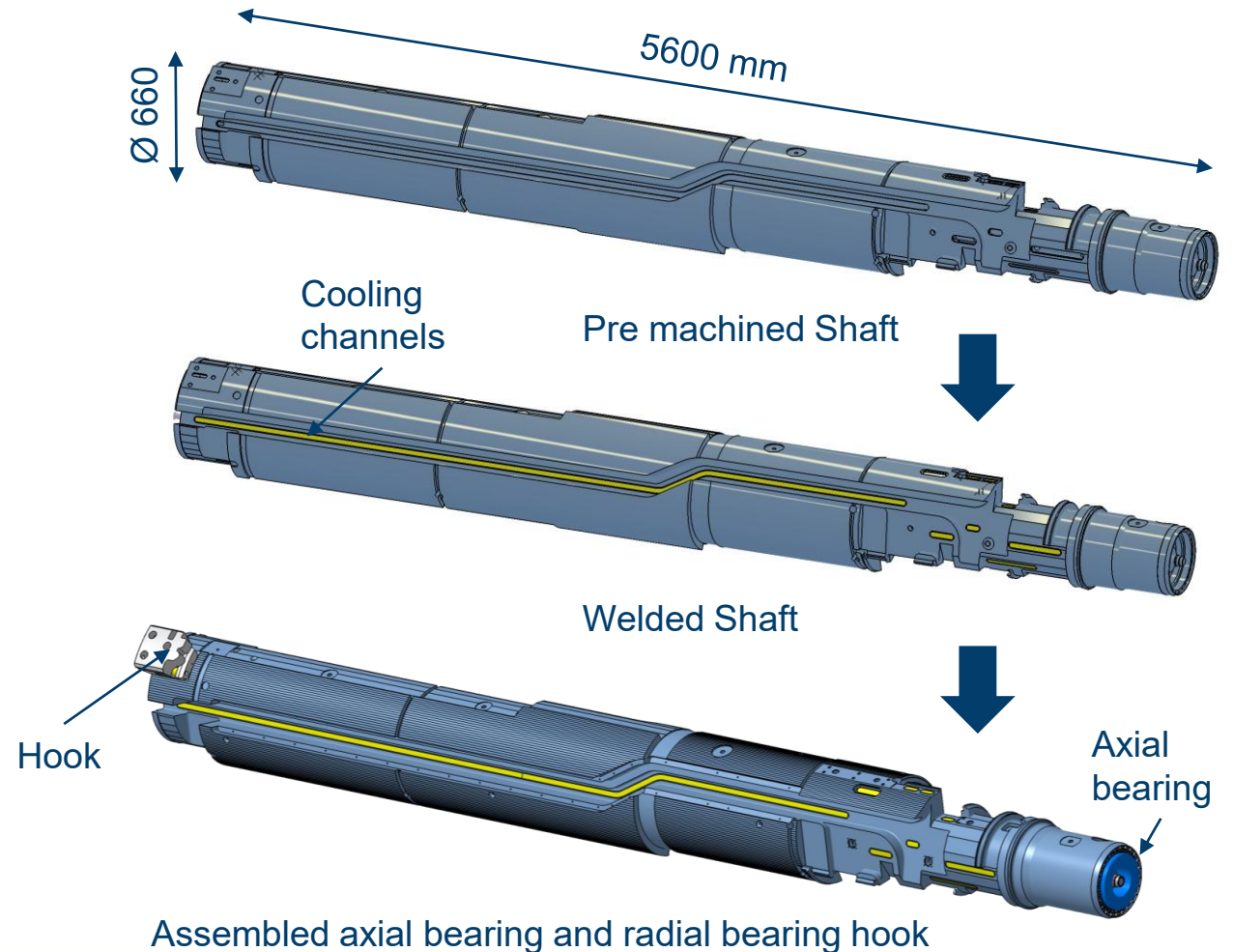
1. Overview
2. Cold Moderator
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4. Thermal Moderator
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7. **MRP Support Structure**
8. Main Assembly
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DESIGN SOLUTION MRP-II

Shaft assembly – Overview

- *Stepped Shaft for guiding the pipework to the components to be cooled & as a rotation axis to “twist” the MRP into operation or lifting position*
- Pressure vessel made of low-Co stainless steel 304l
- TIG & MAC welded cooling channel covers (yellow)
- Light water at an inlet temp. of $T_{in} = 308\text{ K}$
- Design pressure 10 bar
- Operating pressure 8 bar
- $m = 7150\text{ kg}$ (without water)

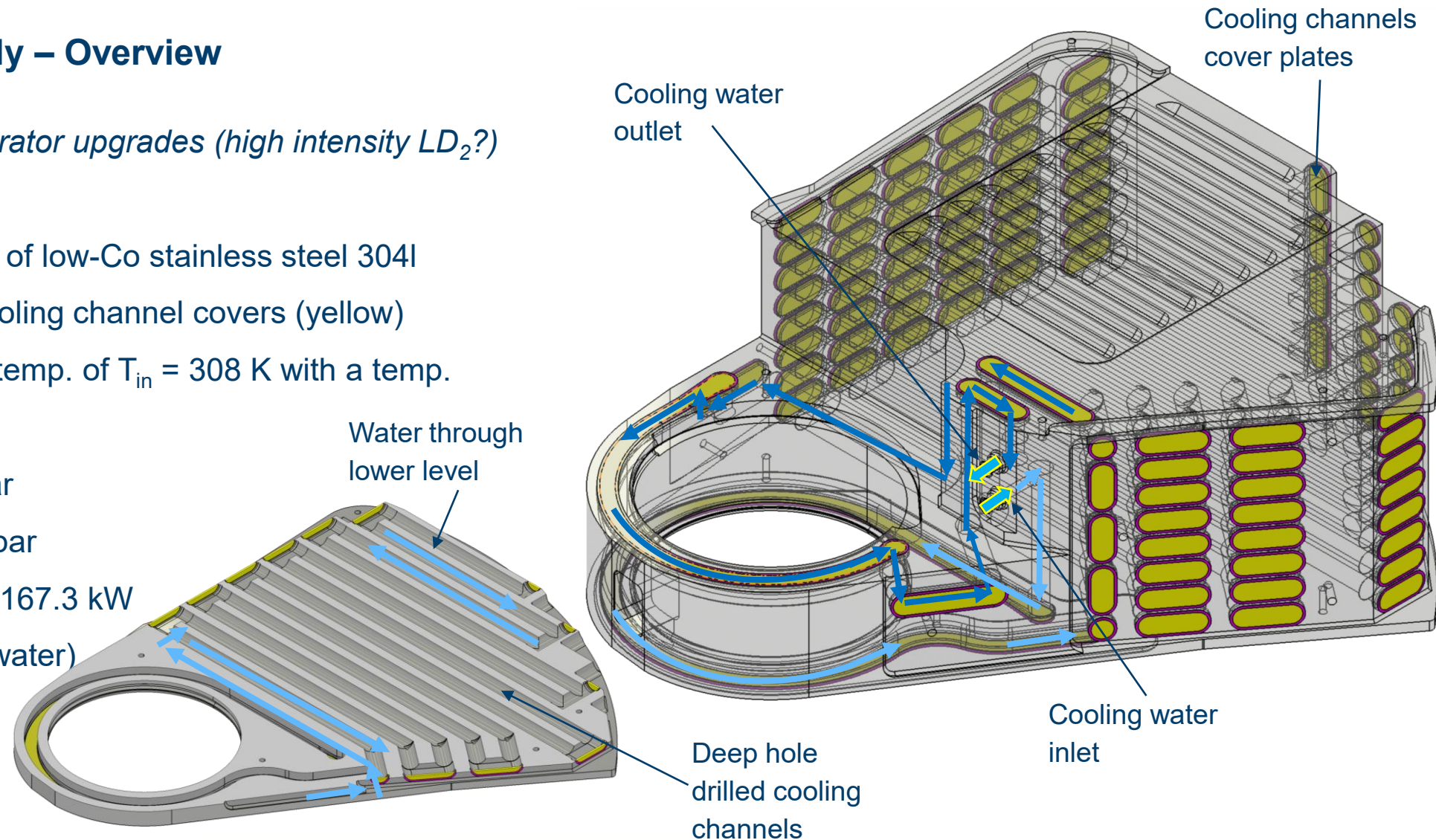


DESIGN SOLUTION MRP-II

Lower Frame assembly – Overview

➤ *Space for future moderator upgrades (high intensity LD₂?)*

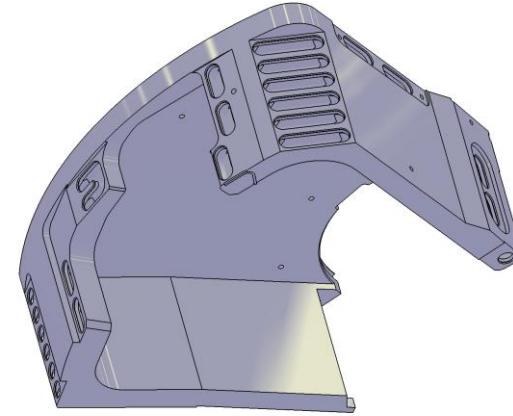
- Pressure vessel made of low-Co stainless steel 304l
- TIG & MAC welded cooling channel covers (yellow)
- Light water at an inlet temp. of $T_{in} = 308$ K with a temp. increase of $dT \leq 33$ K
- Design pressure 10 bar
- Operating pressure 8 bar
- Heat deposition of ca. 167.3 kW
- $m = 1890$ kg (without water)



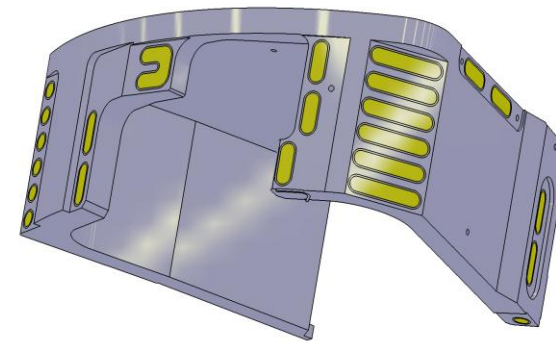
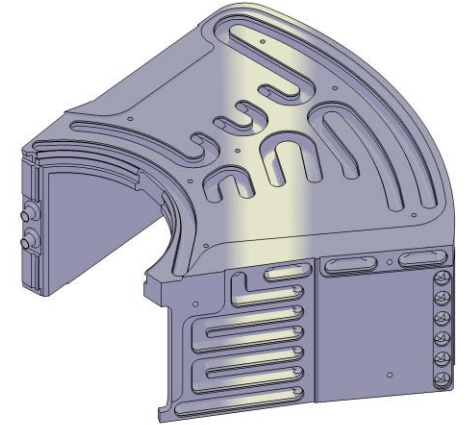
DESIGN SOLUTION MRP-II

Upper Frame assembly – Overview

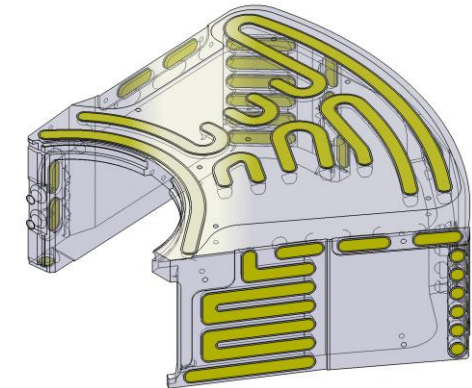
- *Housing of the moderator and reflector components or “outer reflector”*
- Pressure vessel made of low-Co stainless steel 304L
- TIG & MAC welded cooling channel covers (yellow)
- Light water at an inlet temp. of $T_{in} = 308\text{ K}$ with a temp. increase of $dT \leq 11\text{ K}$
- Design pressure 10 bar
- Operating pressure 8 bar
- Heat deposition of ca. 28.5 kW
- $m = 582\text{ kg}$ (without water)



Final machined Upper Frame



Final TIG/MAG welded Upper Frame

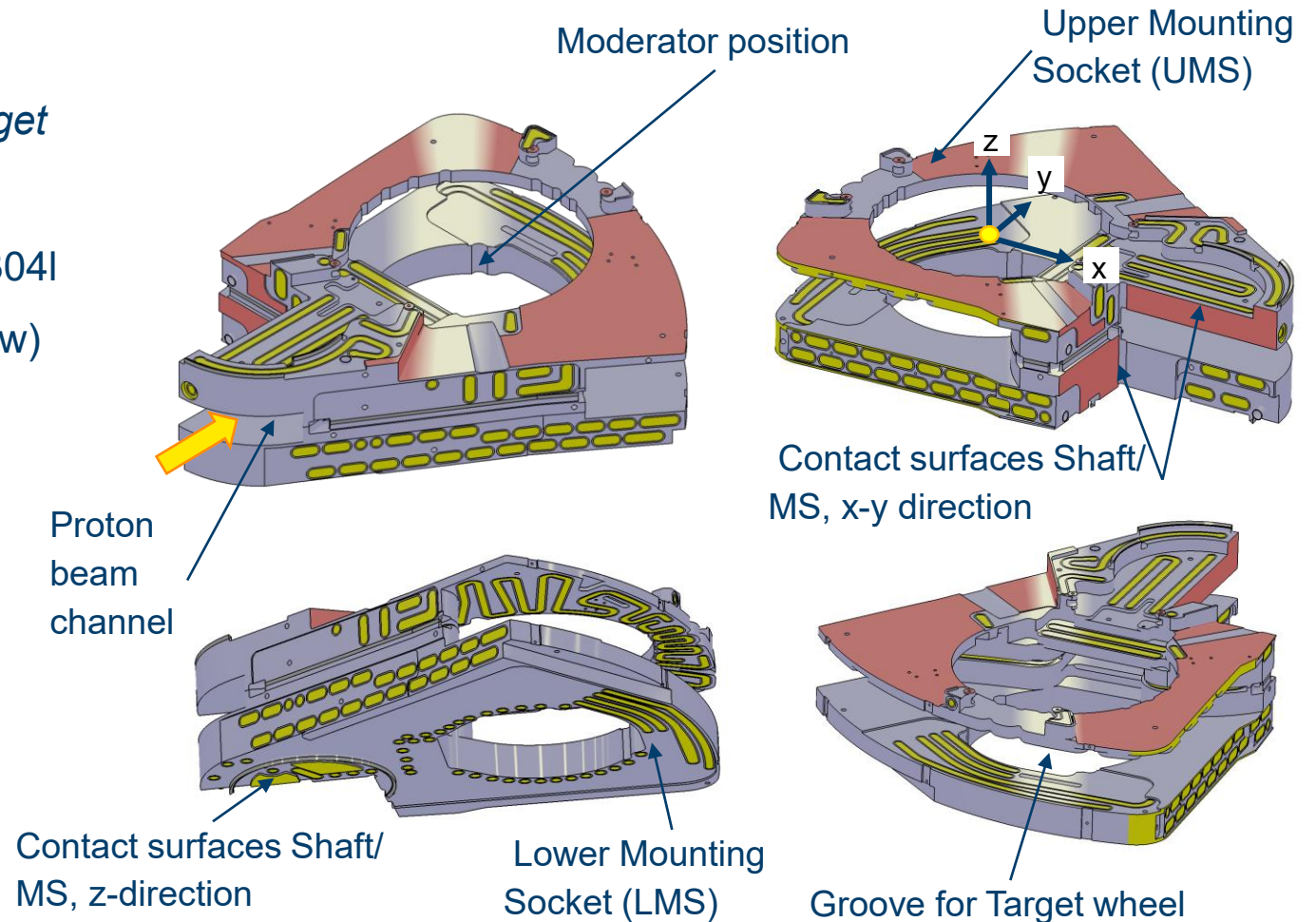


DESIGN SOLUTION MRP-II

Mounting Socket assembly – Overview

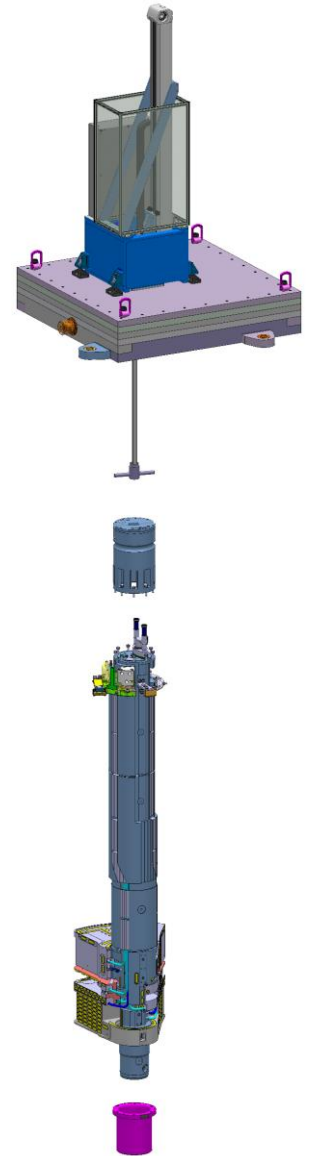
➤ Interface to Shaft, Moderators, Reflector and Target

- Pressure vessel made of low-Co stainless steel 304L
- TIG & MAC welded cooling channel covers (yellow)
- Two independent cooling loops
- Light water at an inlet temp. of $T_{in} = 308\text{ K}$ with a temp. increase of $dT \leq 15/26\text{ K}$
- Design pressure 10 bar
- Operating pressure 8 bar
- Heat deposition of ca. 71 kW / ca. 107 kW
- $m = 646\text{ kg}$ 242 kg+402 kg (without water)



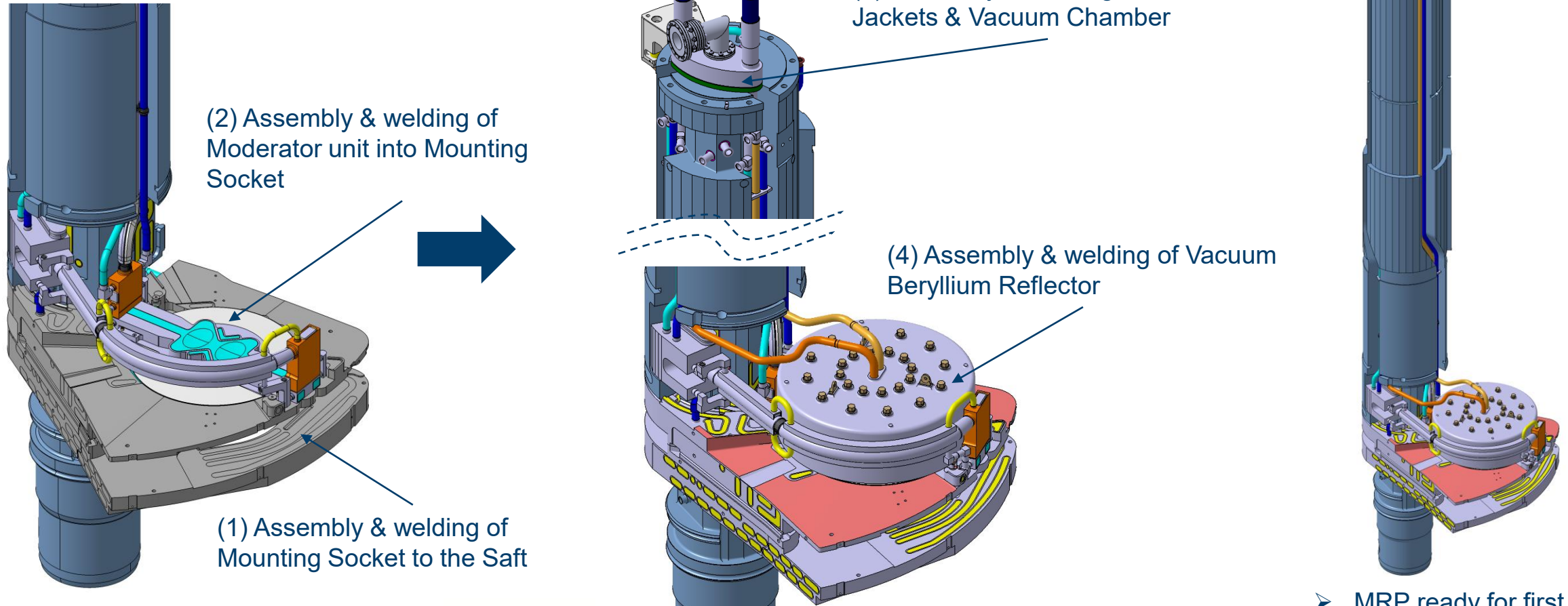
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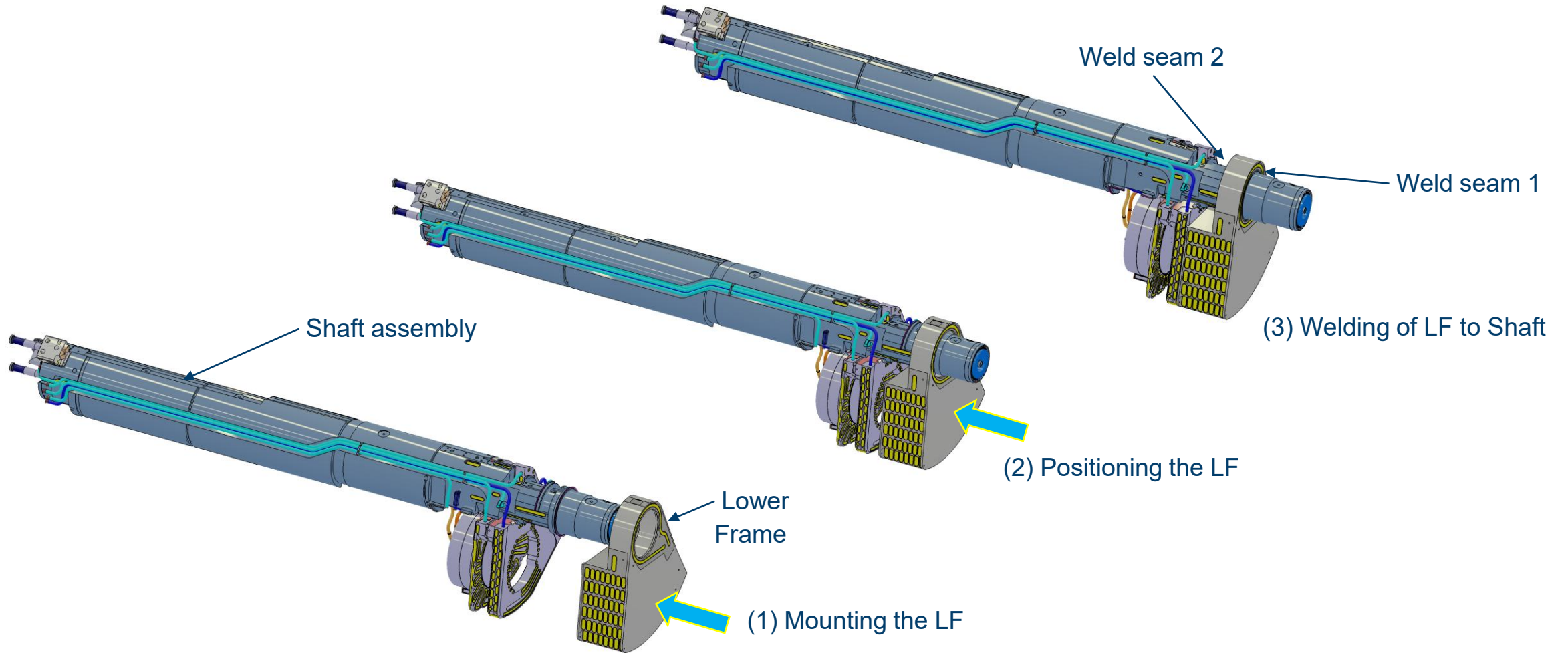
DESIGN SOLUTION MRP-II

Final assembly – Shaft, Mounting Socket and Moderators & Reflector assembly & welding



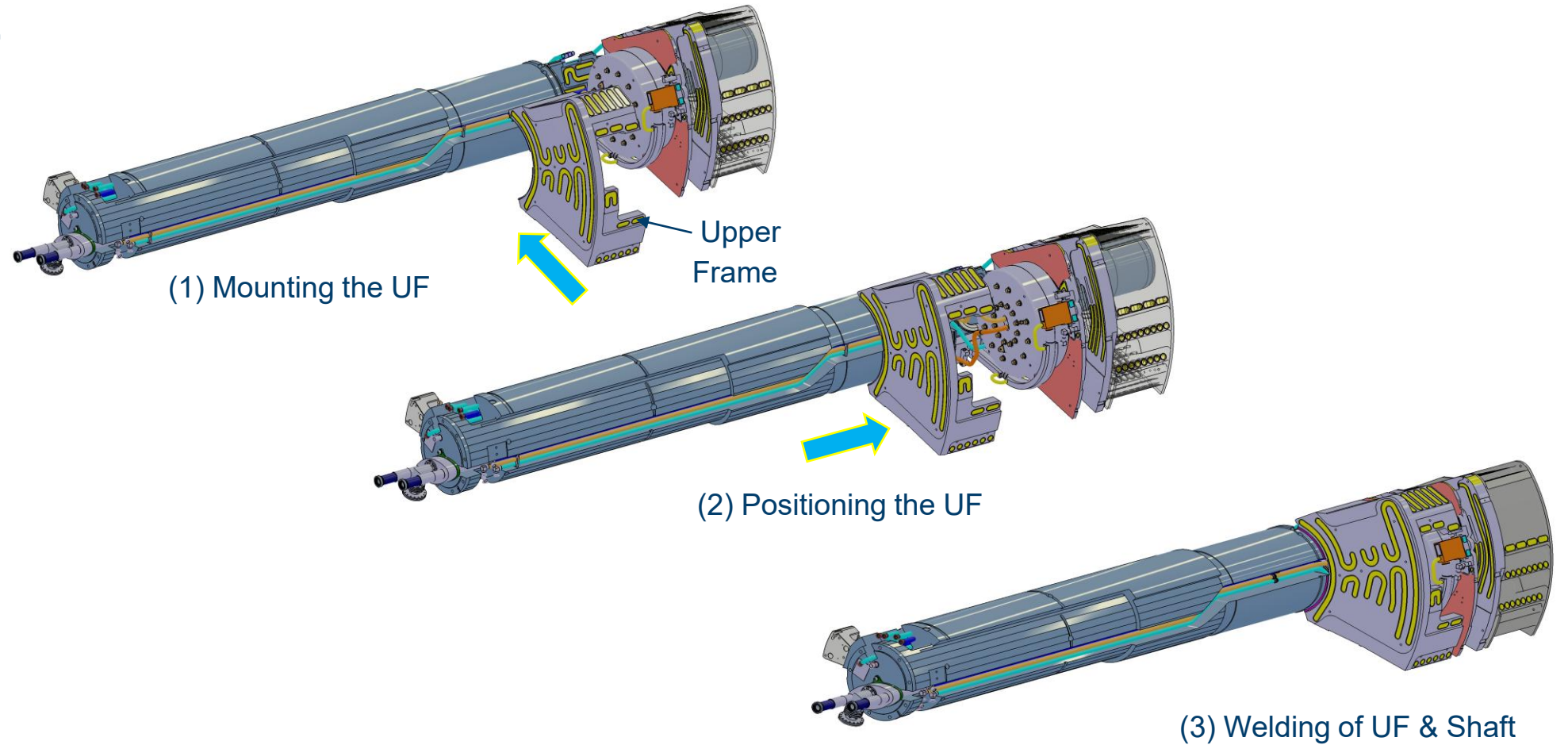
DESIGN SOLUTION MRP-II

Final assembly – Lower Frame assembly & welding



DESIGN SOLUTION MRP-II

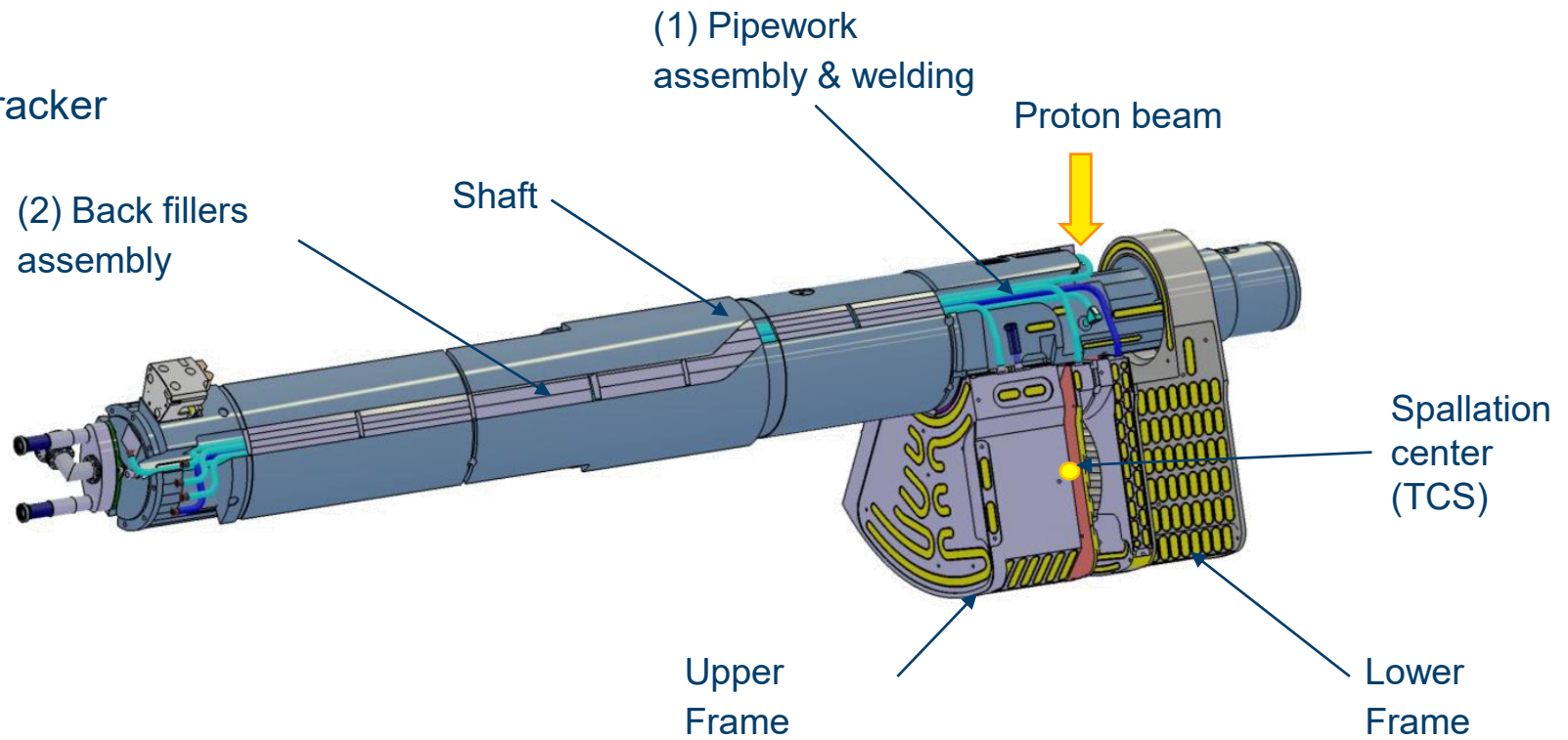
Final assembly – Upper Frame assembly & welding



DESIGN SOLUTION MRP-II

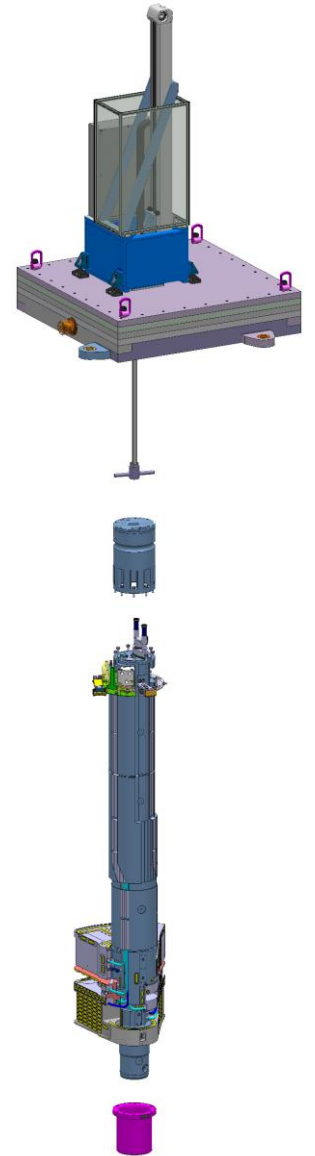
Final assembly

- (1) Assembly & welding of pipework
 - (2) Assembly of back fillers
 - (3) Final NDT
 - (4) Dimension check by laser tracker
 - (5) Final cleaning & packing
- Total weight 11.350 kg



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Production status

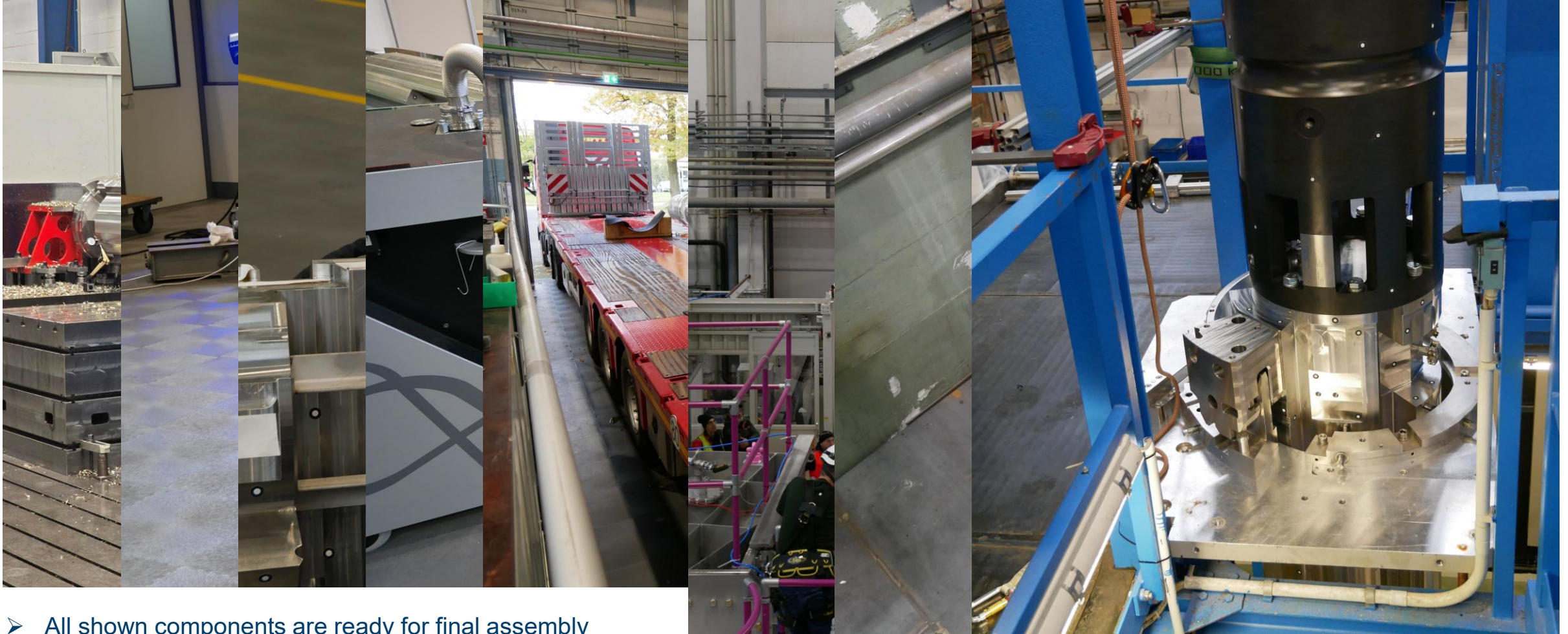
✓ Cold Moderator, Irradiation Module, thermal Moderator & Beryllium Reflector



➤ All shown components are ready for final assembly

Production status

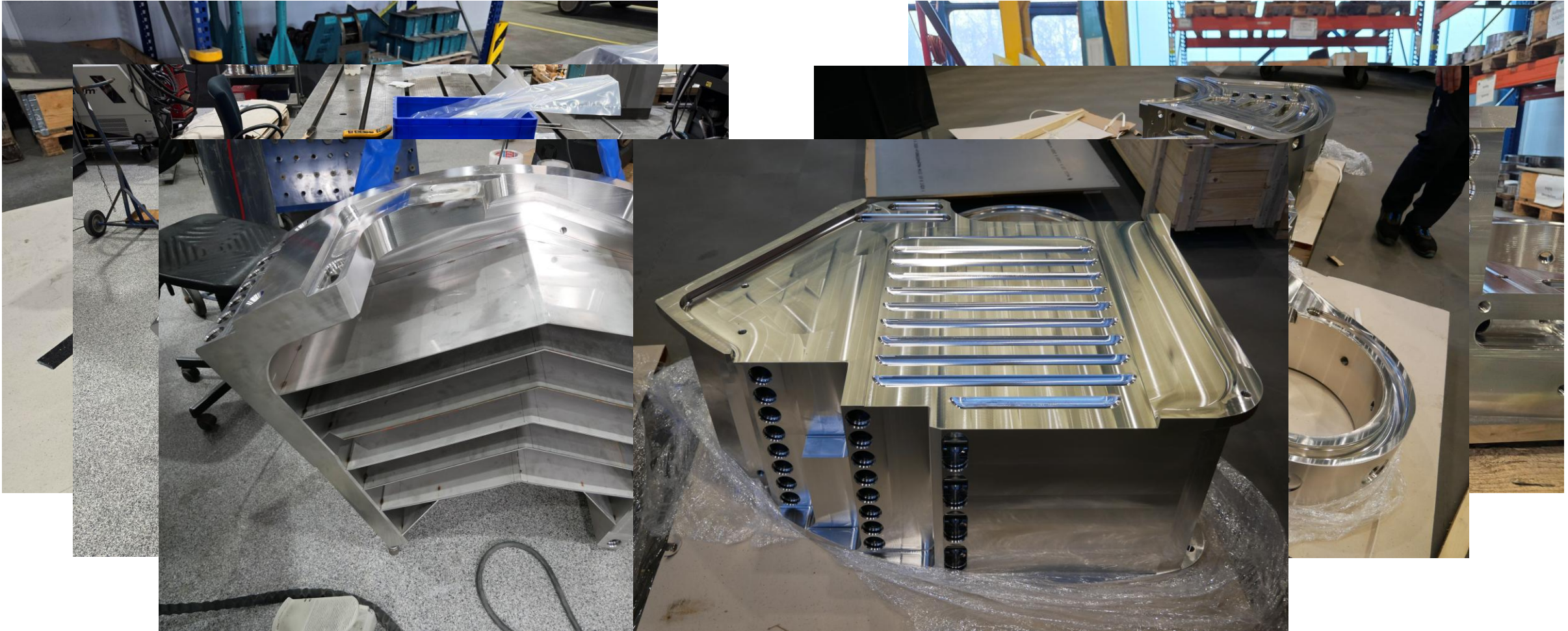
✓ Shaft & Crown assembly



➤ All shown components are ready for final assembly

Production status

In progress: Upper Frame & Lower Frame



➤ Upper Frame TIG welding ongoing (April)

➤ Lower Frame TIG welding in preparation (May)

Production status

In progress: Upper Mounting Socket & Lower Mounting Socket



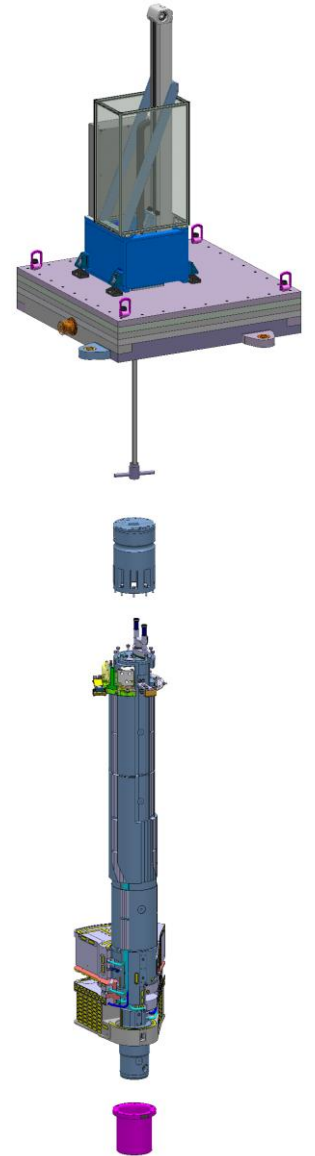
- Lower Mounting Socket ready for final assembly (March)

- Upper Mounting Socket TIG welding ongoing (April)

- Upper + Lower Mounting Socket TIG welding and final milling (May)

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SUMMARY & OUTLOOK

- Project intime!
- Completion at approximately >90%
- Most critical assemblies are finalized including NDT, cleaning and documentation:
 - Cold Moderator
 - Irradiation Module
 - Thermal Moderator
 - Beryllium reflector
 - Shaft assembly
 - Crown
 - Rotation Unit (final FAT is scheduled for CW 17 & 18)
- Cool down of cold moderator (with Nitrogen at FZJ) last critical/risky task scheduled for June
- Final assembly scheduled for July to August
- Dimension control, cleaning and packing scheduled for September
- Delivery to ESS mid. October!

THANK YOU FOR YOUR ATTENTION!

QUESTIONS?



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