

# Radiation challenges of primary cooling return water

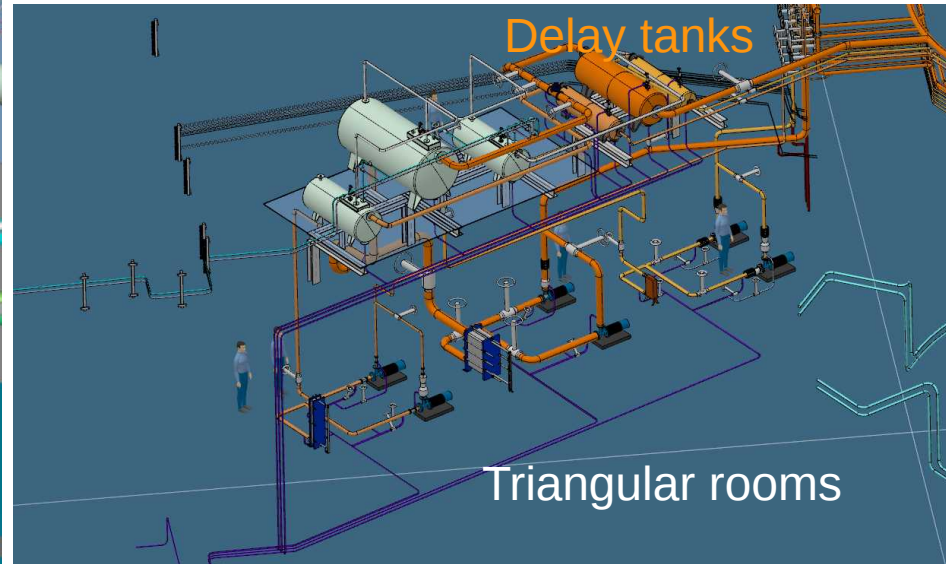
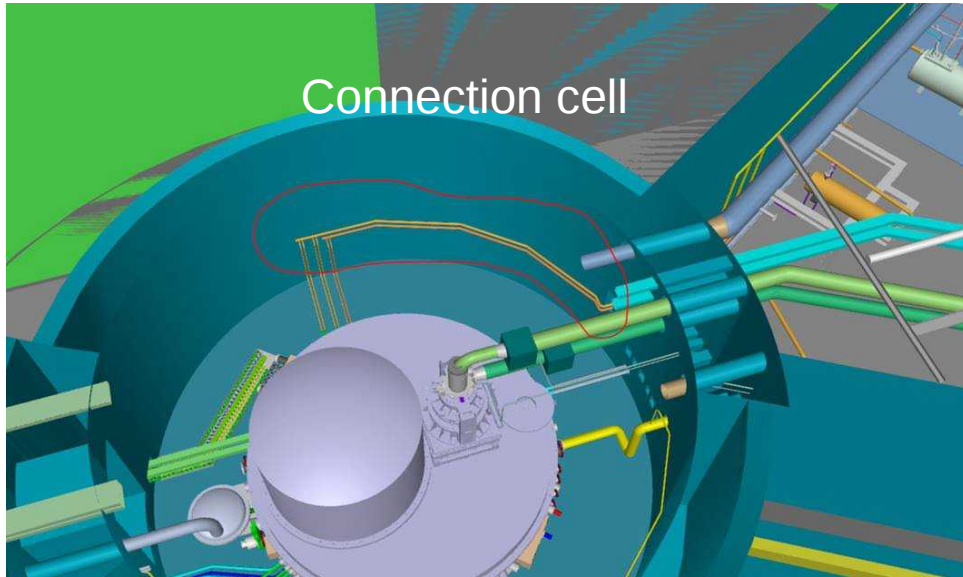
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ESS & DTU

TAC 14, Lund, 5<sup>th</sup> – 7<sup>th</sup> October 2016

# Motivation

- **Assess biological dose rates in:**
  - › **Connection Cell**
  - › **Utilities rooms (triangular rooms)**
  - › **Instrument hall****from activated primary cooling water**
- **Adjust shielding to meet requirements**

# Water circuit overview



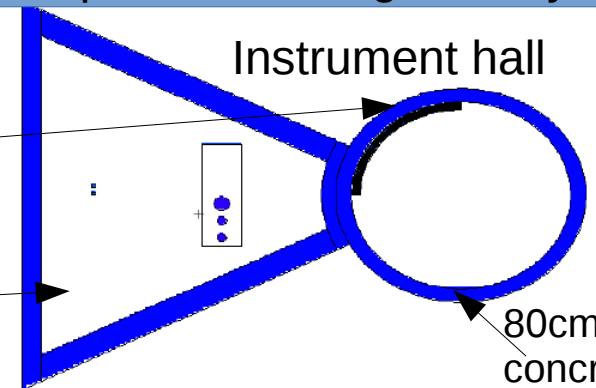
During operations, requirements on the biological dose-rate are:

- $3\mu\text{Sv/h}$  in the instrument hall
- $3\mu\text{Sv/h}$  at the "32m" wall
- $25\mu\text{Sv/h}$  adjacent the triangular rooms

3

Concrete wall, 32m

Simplified MCNP geometry



# Methods

- Using the *MCNP* Master Model, all water cells in the reflector plug are combined including impurities\*, and the activity is calculated at different times using CINDER'90 (v1.05)

## Irradiation history

### Time step

- 2700h: 2GeV, 2.5mA proton beam on target
- 1680h: Beam off.
- 2700h: 2GeV, 2.5mA proton beam on target
- 1680h: Beam off.
- 2700h: 2GeV, 2.5mA proton beam on target
- 1680h: Beam off.
- 2700h: 2GeV, 2.5mA proton beam on target

## Delay tank relevant

- 0s cooling time
- 30s cooling time
- 60s cooling time
- 90s cooling time
- 120s cooling time

## Maintenance relevant

- 1h cooling time
- 4h cooling time
- 1d cooling time
- 7d cooling time
- 1y cooling time

- Source term prepared for each time step using *gamma script*
- Gamma transport calculations results in biological dose-rate maps using ICRP-116 fluence-to-dose conversion factors*
- Full source term describes the total activity resulting from ~2years of running.
  - A good representation of the long lived isotopes.
  - Modeling is static => depending on subsystem: full source term is a poor representation of the short lived

# Inventory

Relevant for  
delay tank

Isotope	Half-life [s]	Decay mode	Time step 8 [0s]	Time step 9 [30s]	Time step 10 [60s]	Time step 11 [90s]	Time step 12 [120s]
$^3\text{H}$	3.89E8	$\beta$	621.3	621.3	621.3	621.3	621.3
$^7\text{Be}$	4.61E6	$\text{EC}\beta + \gamma[477\text{keV}]$	445.1	445.1	445.1	445.1	445.1
$^{11}\text{C}$	1223	$\beta$	1473	1449	1424	1400	1377
$^{14}\text{O}$	70.6	$\beta + \gamma[2.3\text{MeV}]$	92.3	69.4	51.7	38.5	28.7
$^{15}\text{O}$	122	$\beta$	4511	3827	3228	2723	2297
$^{16}\text{N}$	7.1	$\beta + \gamma[6.1\text{MeV}]$	4462	266.1	14.4	0.8	0.04
Total			12380	7161	6234	5657	5180

Relevant for  
maintenance

Isotope	Half-life [s]	Decay mode	Time step 13 [1h]	Time step 14 [4h]	Time step 15 [1d]	Time step 16 [7d]	Time step 17 [1y]
$^3\text{H}$	3.89E8	$\beta$	621.3	621.3	621.2	620.6	587.3
$^7\text{Be}$	4.61E6	$\text{EC}\beta + \gamma[477\text{keV}]$	444.9	444.2	439.4	406.4	3.9
$^{11}\text{C}$	1223	$\beta$	191.6				
$^{14}\text{O}$	70.6	$\beta + \gamma[2.3\text{MeV}]$					
$^{15}\text{O}$	122	$\beta$					
Total			1270	1070	1060	1030	592

Activities in Curie. Only main contributors listed - "Total" includes all

● The first few minutes,  $^{16}\text{N}$  is the most problematic nuclide. At later times  $^7\text{Be}$

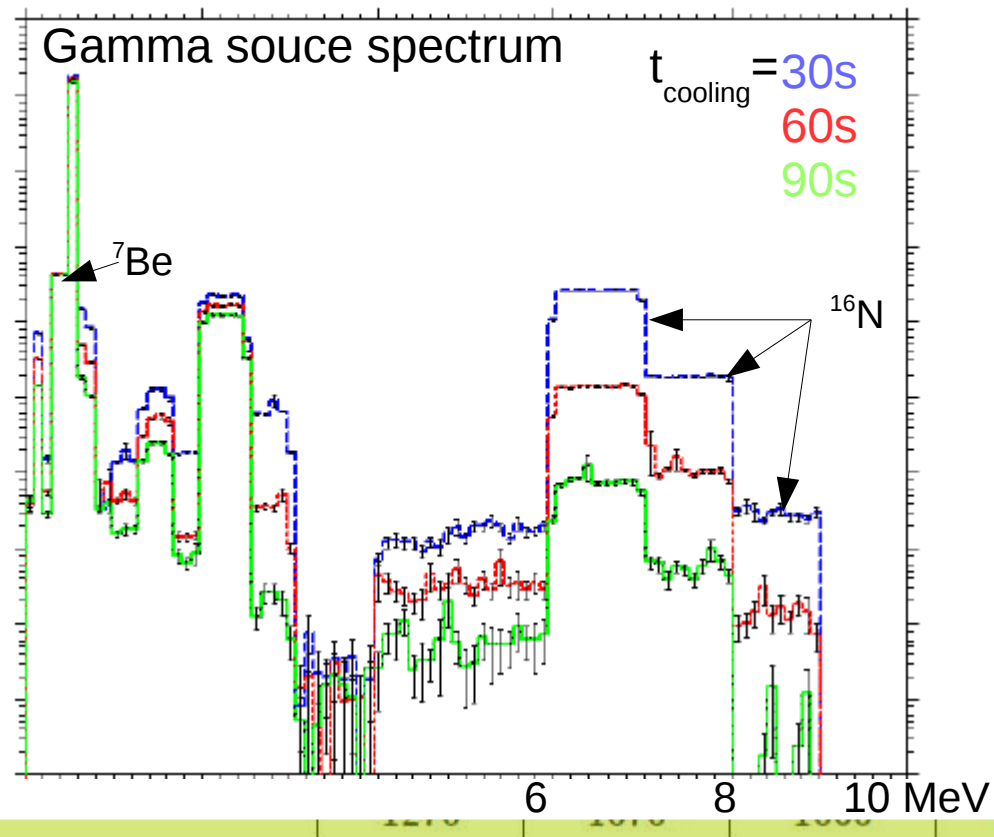
# Inventory

Relevant for  
delay tank

Isotope	Half-life [s]
$^3\text{H}$	3.89E8
$^7\text{Be}$	4.61E6
$^{11}\text{C}$	1223
$^{14}\text{O}$	70.6
$^{15}\text{O}$	122
$^{16}\text{N}$	7.1
Total	

Relevant for  
maintenance

Isotope	Half-life [s]
$^3\text{H}$	3.89E8
$^7\text{Be}$	4.61E6
$^{11}\text{C}$	1223
$^{14}\text{O}$	70.6
$^{15}\text{O}$ </td <td>122</td>	122
Total	



Time step [90s]	Time step 12 [120s]
521.3	621.3
445.1	445.1
1400	1377
38.5	28.7
2723	2297
0.8	0.04
5657	5180

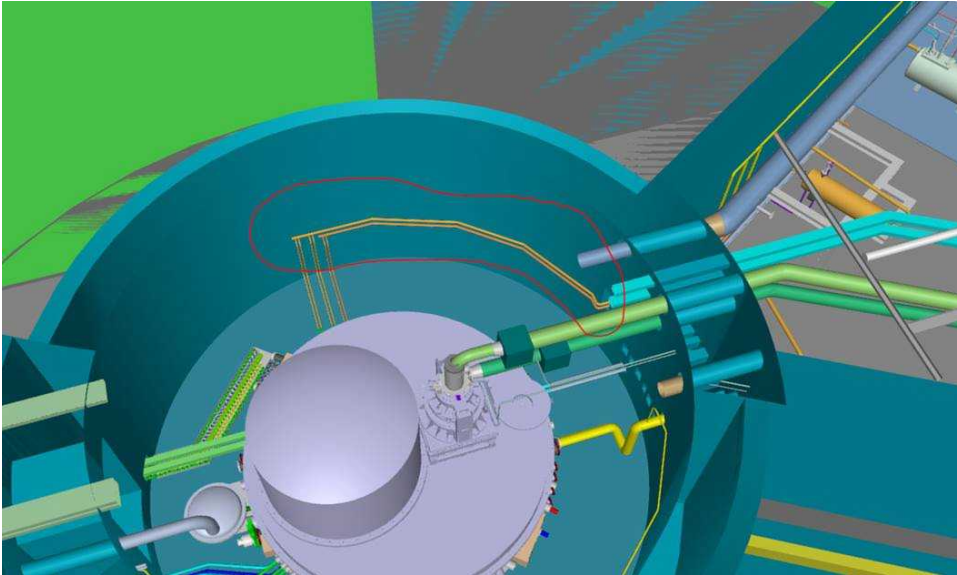
Time step 7d]	Time step 17 [1y]
0.6	587.3
0.4	3.9
1000	592

Activities in *Curie*. Only main contributors listed - "Total" includes all

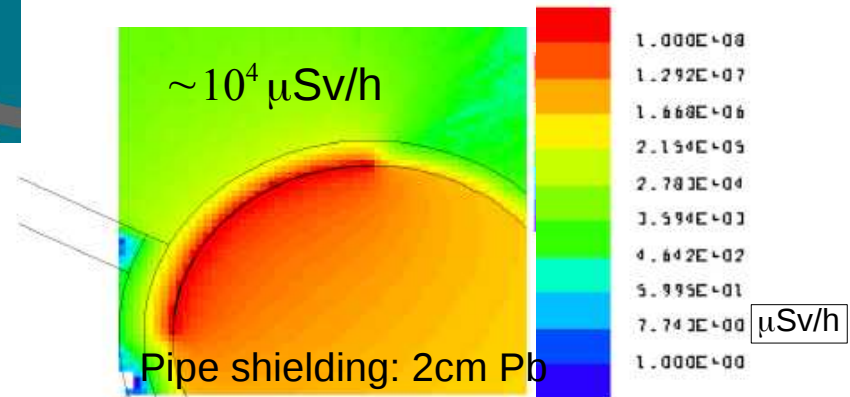
● The first few minutes,  $^{16}\text{N}$  is the most problematic nuclide. At later times  $^7\text{Be}$



# Follow the water: 1 – Connection Cell



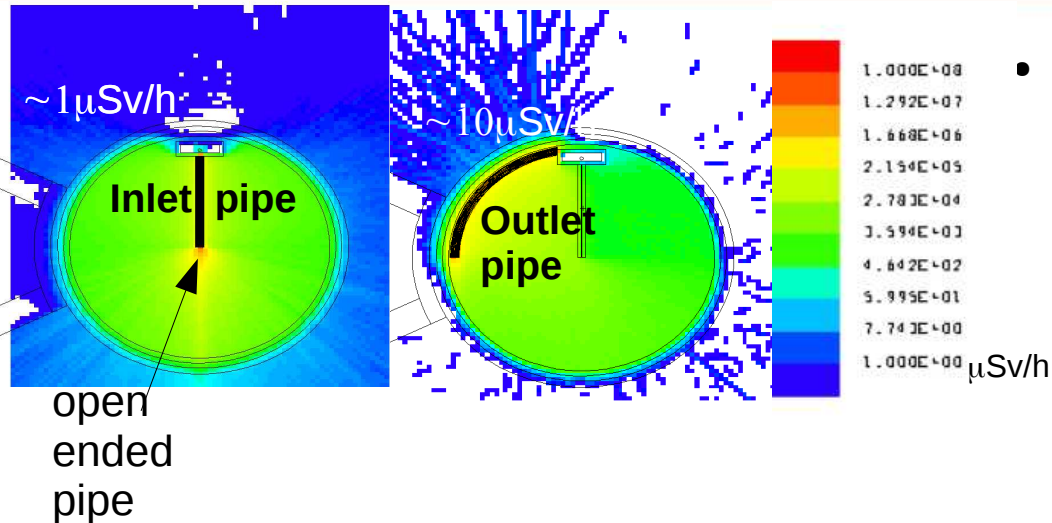
- Pipe at the thin instrument hall facing wall is problematic
- Impractical to shield
- Move delay tanks to Connection Cell



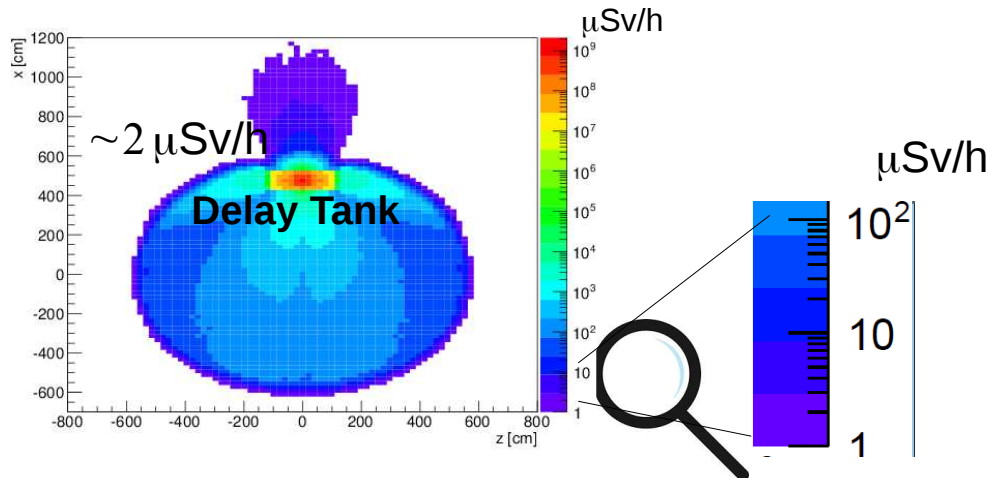
Conservative estimation:

- ▶ Overestimating water volume fraction,
- ▶ Underestimating cooling time

# Shielding in Connection Cell



- Limit in instrument hall: 3  $\mu\text{Sv/h}$  drives the shielding
  - ~12cm lead around Delay tank inlet pipe
  - ~18cm lead between delay tanks and instrument hall
  - 2cm lead around 90s delay tank outlet ← over conservative: Assumes  ${}^7\text{Be}$  built up in water, rather than in filters.

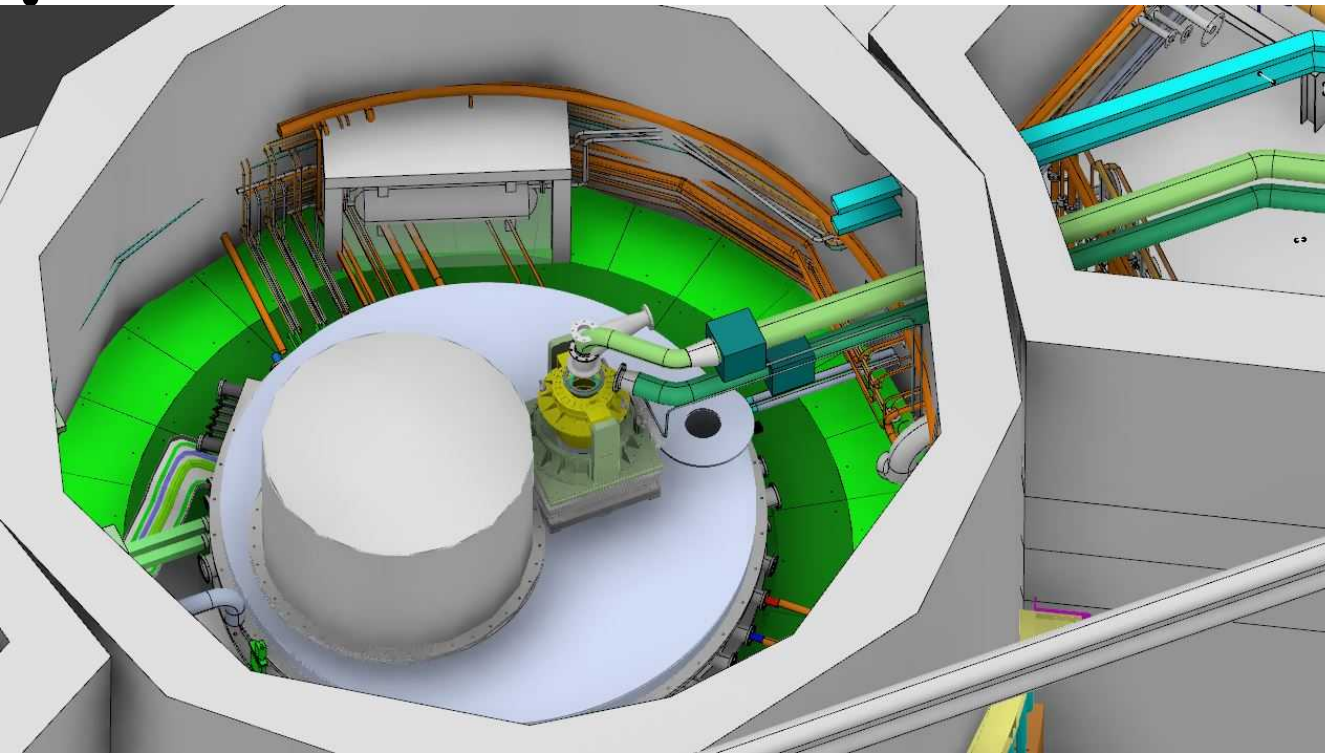




# Delay tanks – proposed solution

## Solution

- Move (Thermal Moderator Cooling + Reflector Cooling) - Delay Tanks into Connection Cell
- Lead shielding
- Shield inlet pipes to delay tanks
- Avoid shielding of outlet pipes:
  - Use delay time 90 s
  - Remove conservatism in calculation for pipes inside connection cell



# Delay tanks – proposed solution

## Issues/Risks

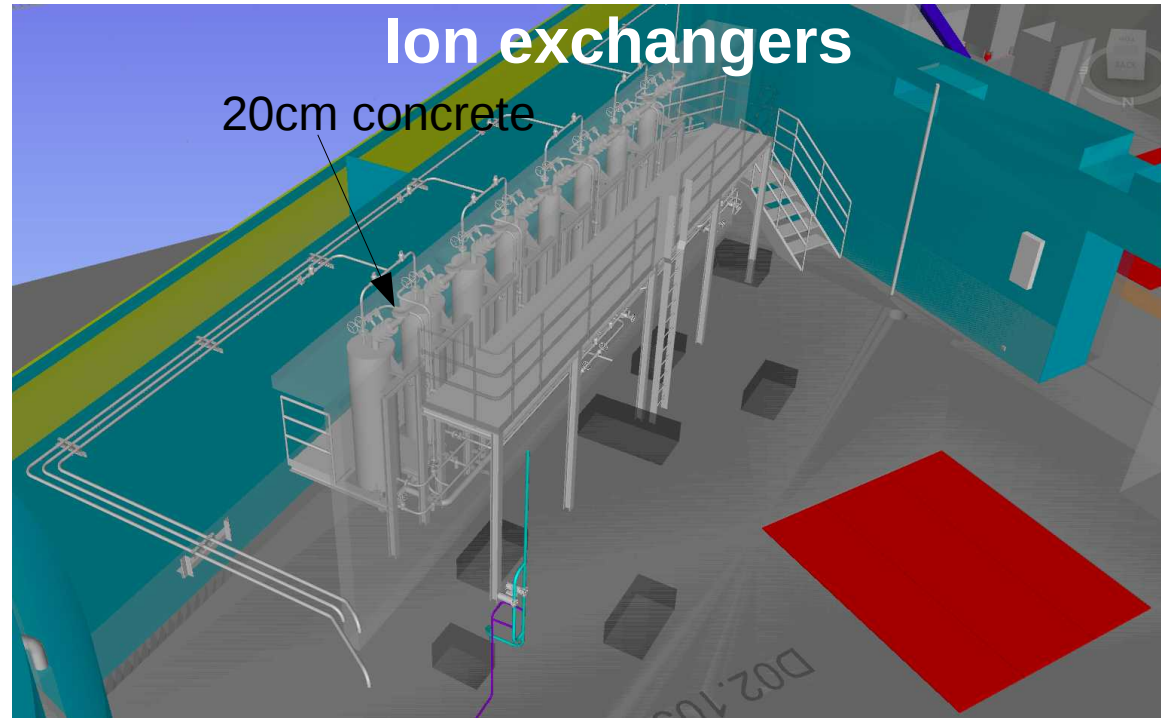
- Radiation resistance of electronics and drive unit
- Shielding of pipes within monolith vessel

## Next steps

- Remove conservatism in calculations
- Alternative solution:
  - Replace monolith shielding blocks with delay tanks
  - Issue:** High point in piping system could lead to H<sub>2</sub>-pockets

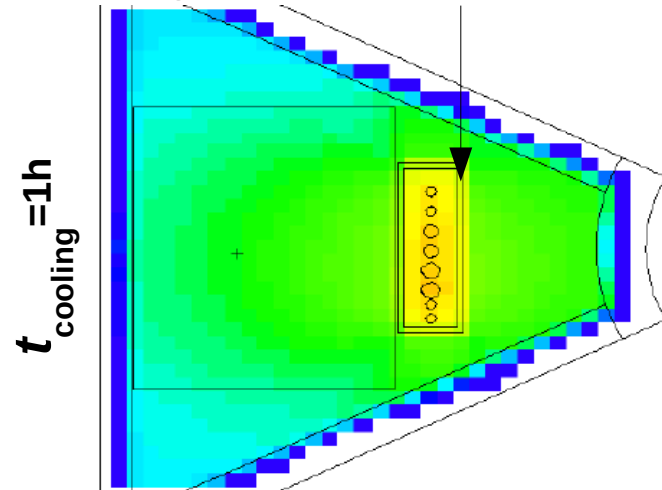
# Triangular rooms: maintenance

- After ~few hours,  $^7\text{Be}$  in ion exchanger columns dominates
- Ion exchangers, situated behind 20cm concrete
- Optionally, unproblematic to add 10cm lead

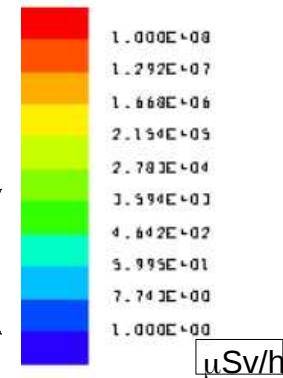
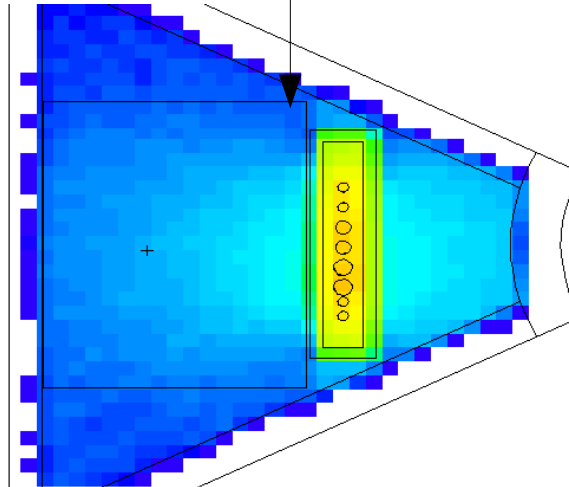


# Triangular rooms: maintenance

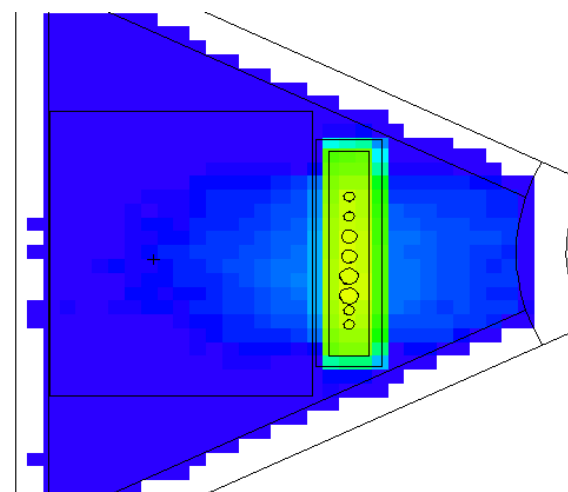
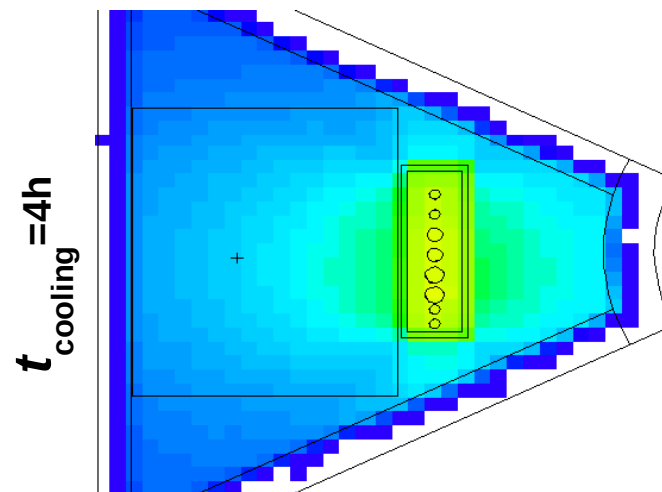
Shielding: 20cm concrete



40cm concrete



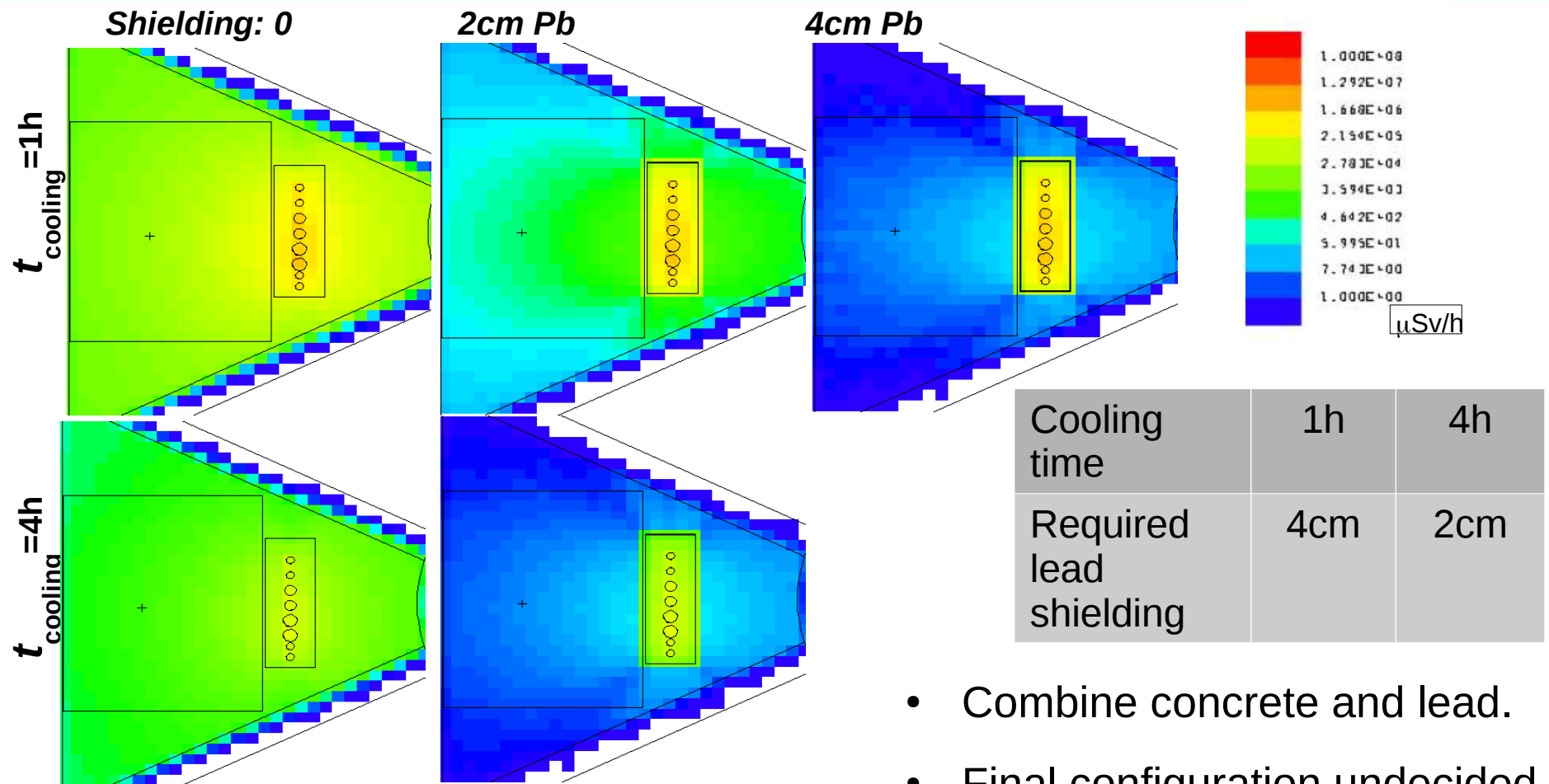
- Dose limit for radiation workers:  $25\mu\text{Sv/h}$



Cooling time	1h	4h
Required concrete shielding	>40cm	40cm

- >40cm concrete walls are impractical => consider lead

# Triangular rooms: maintenance



- Combine concrete and lead.
- Final configuration undecided

# Conclusions

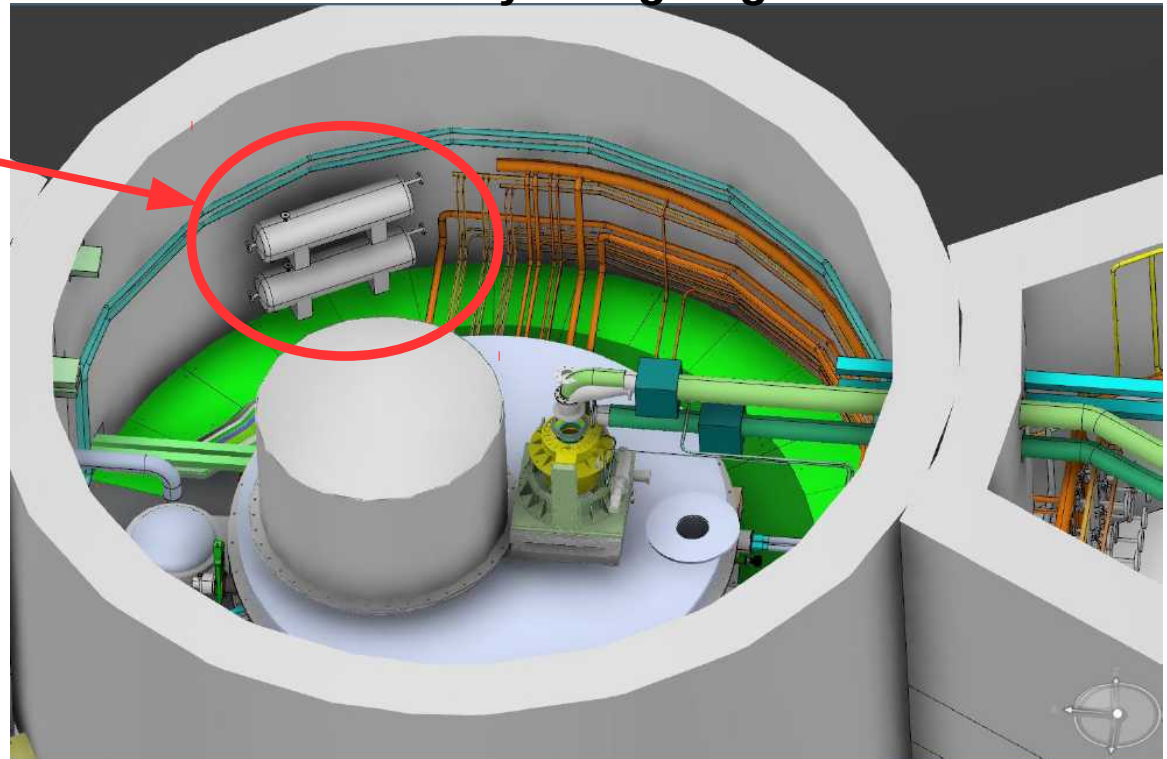
- The radiation from primary cooling water circuit is modeled in a simplified geometries.
- For each subsystem of the circuit the shielding needed to reach the required biological dose limits are calculated
- Under the assumption that the delay tank is moved into the connection cell, the results can be summarized as follows:
  - Delay tank inlet pipe Pb shielding : ~12cm
  - Delay tank Pb shielding : ~18cm
  - Delay tank outlet pipe Pb shielding : ~2cm [for 90s DT] ← over conservative. Likely not needed
  - Pipe Pb shielding in triangular rooms : ~0cm [for 90s DT]
  - Shielding in triangular rooms  
required for maintenance : 1 hour cooling: >40cm concrete / 4cm lead  
: 4 hour cooling: 40cm concrete / 2cm lead
- Final note: Ensure all contributors are accounted for:  $3\mu\text{Si/h}$  /  $25\mu\text{Si/h}$  is for everything



# Next steps

- Engineering redesign:
  - Place delay tank in connection cell
  - Add shielding to pipes and ion exchanger
- Neutronics:
  - Remove over-conservatism: model  $^7\text{Be}$  as (mostly) filtered in ion exchanger
  - Model electronics in connection cell
  - Refine neutronics models according to updated engineering

## Preliminary – ongoing work



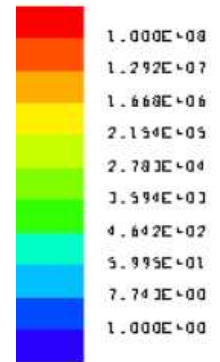
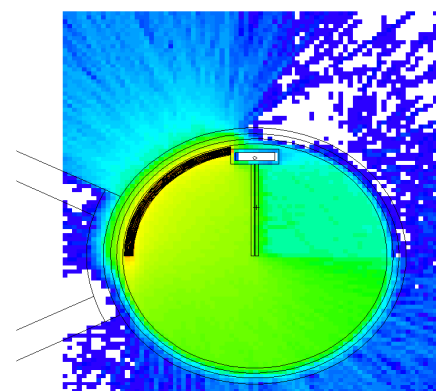
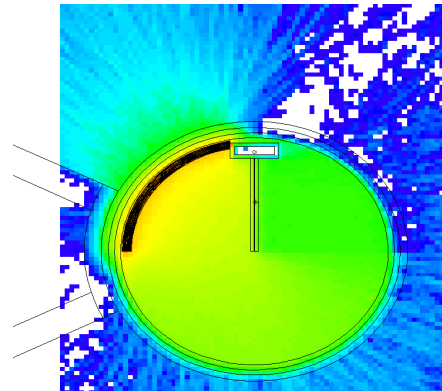
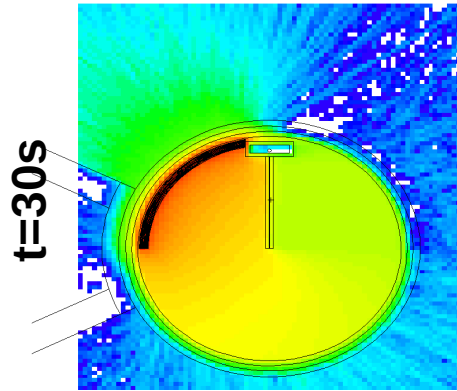
# Backup slides

# 4 – delay tank outlet pipe - extra

Pipe shielding: 0

Pipe shielding: 2cm Pb

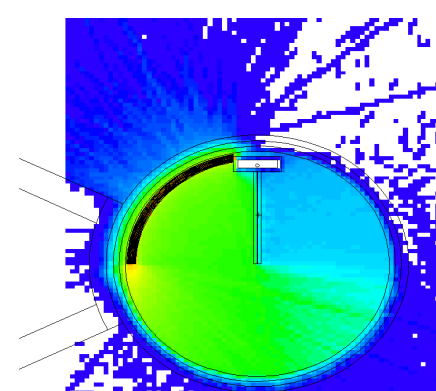
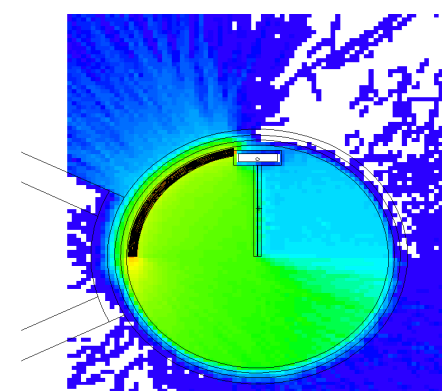
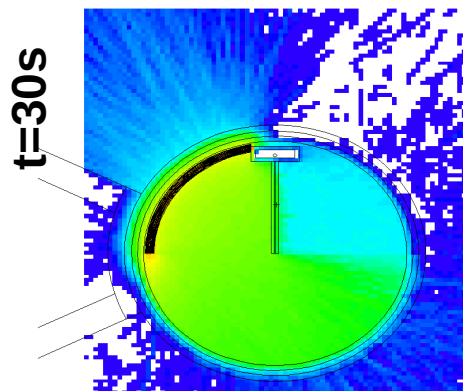
Pipe shielding: 4cm Pb



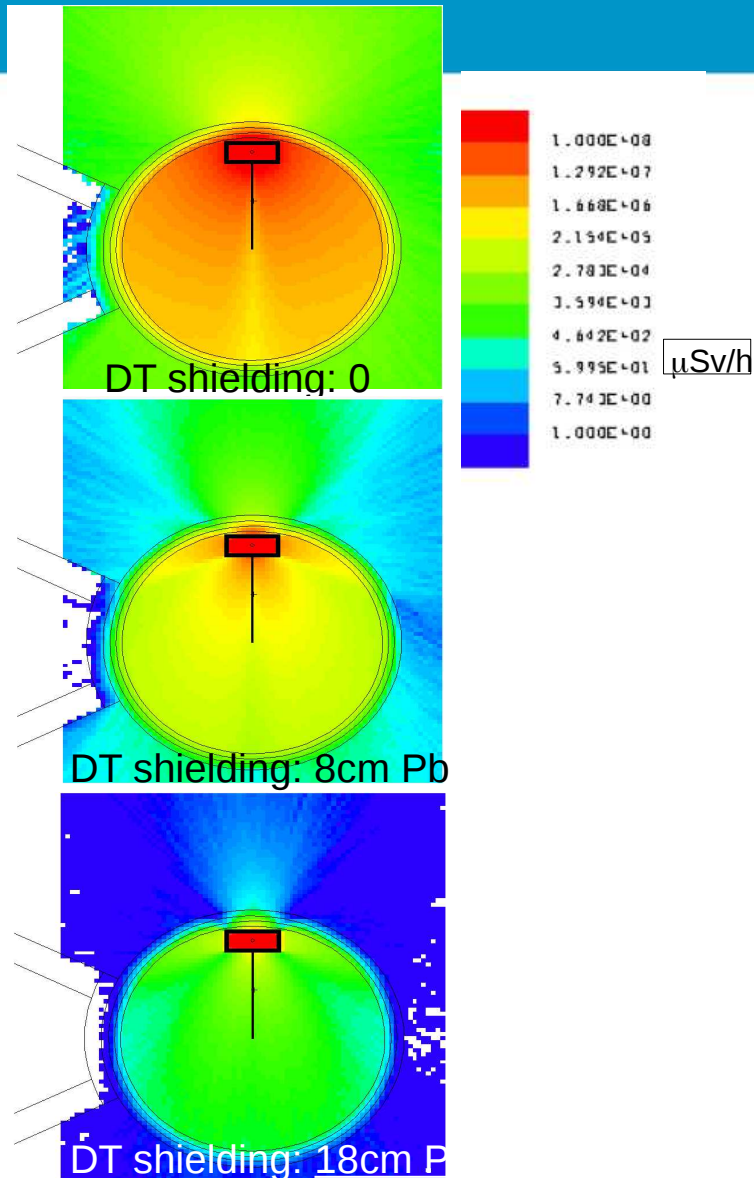
Pipe shielding: 6cm

Pipe shielding: 8cm Pb

Pipe shielding: 10cm Pb



# 2 – delay tanks



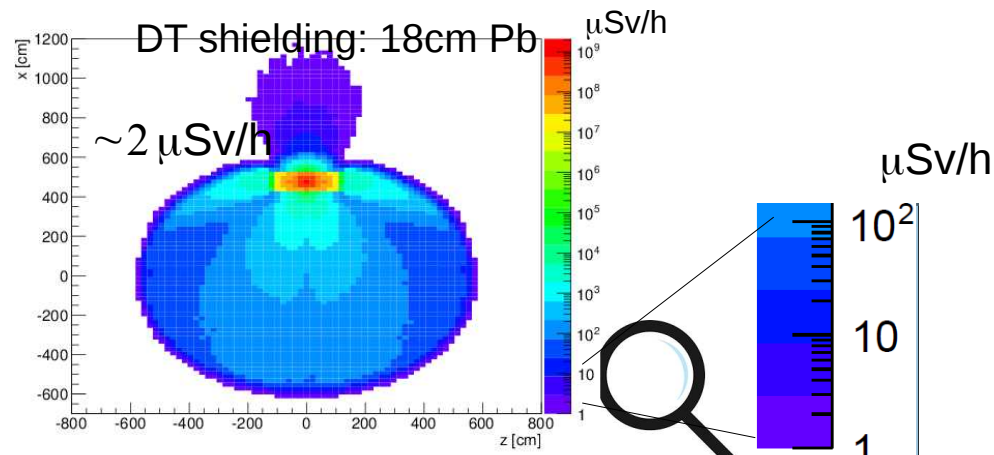
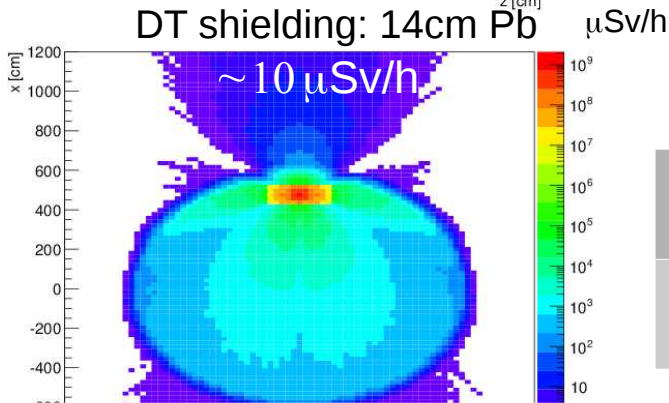
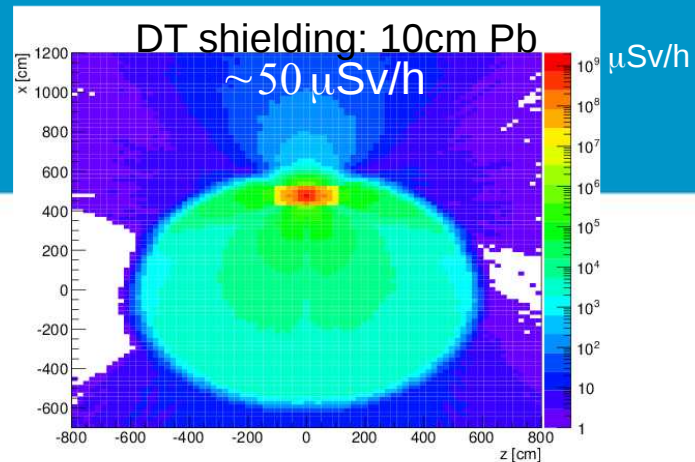
- Alternative approach : *Full source term* at  $t_{\text{cooling}}=0$  is placed in the delay tank
- Conservative: neglects delay, water volume fraction
- The shielding on the room-facing size, may be relaxed – from a solid angle consideration ~ the dose level in the instrument hall is  $\sim(1\text{m}/10\text{m})^2$  lower, corresponding to  $\sim 4\text{cm}$  lead

# 2 – delay tanks

- 9L of water in the moderator. Exhaust speed 0.6L/s => average cooling time at exit: 7.5s.
- 5m vertical + 5m horizontal: 5s
- Starting at  $t_{\text{cooling}}$ : 7.5s+5s = 13s, the delay tank is modeled:

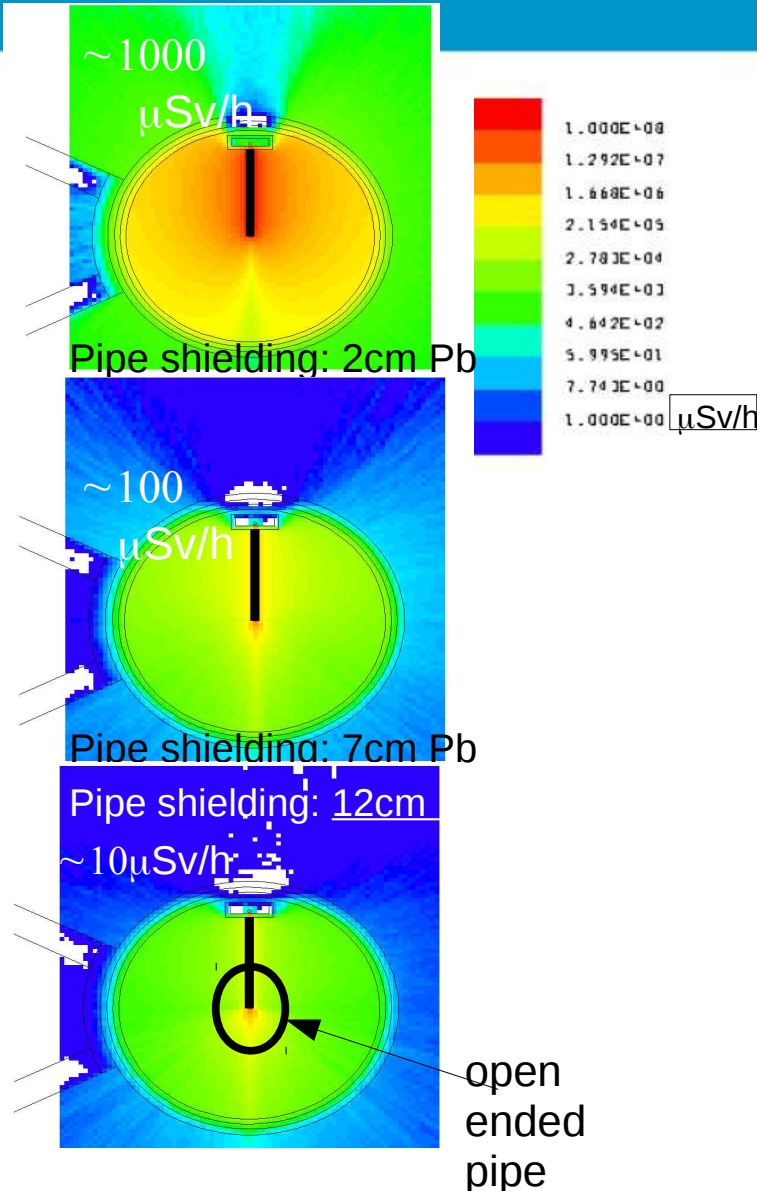
Cooling time [s]	13	16	19	22	25	28	31	34	37
Source weight [%]	12	12	12	12	12	12	12	12	4

- I.e. CINDER'90 is re-run, to prepare source definitions. For each shielding geometry, 9 separate MCNP simulations are performed and the resulting dose-rate maps added
- ~18cm lead needed to reach dose-level requirements in the instrument hall





# 3 – delay tank inlet pipe



- Volume in pipe  $\sim 1/6$  moderator volume  
 $\Rightarrow 1/6 \times$  *Full source term* at  $t_{\text{cooling}}=0$  is placed in the pipe
- Conservative: no cooling
- $\sim 12\text{cm}$  lead needed to ensure sufficiently low dose levels in the instrument hall

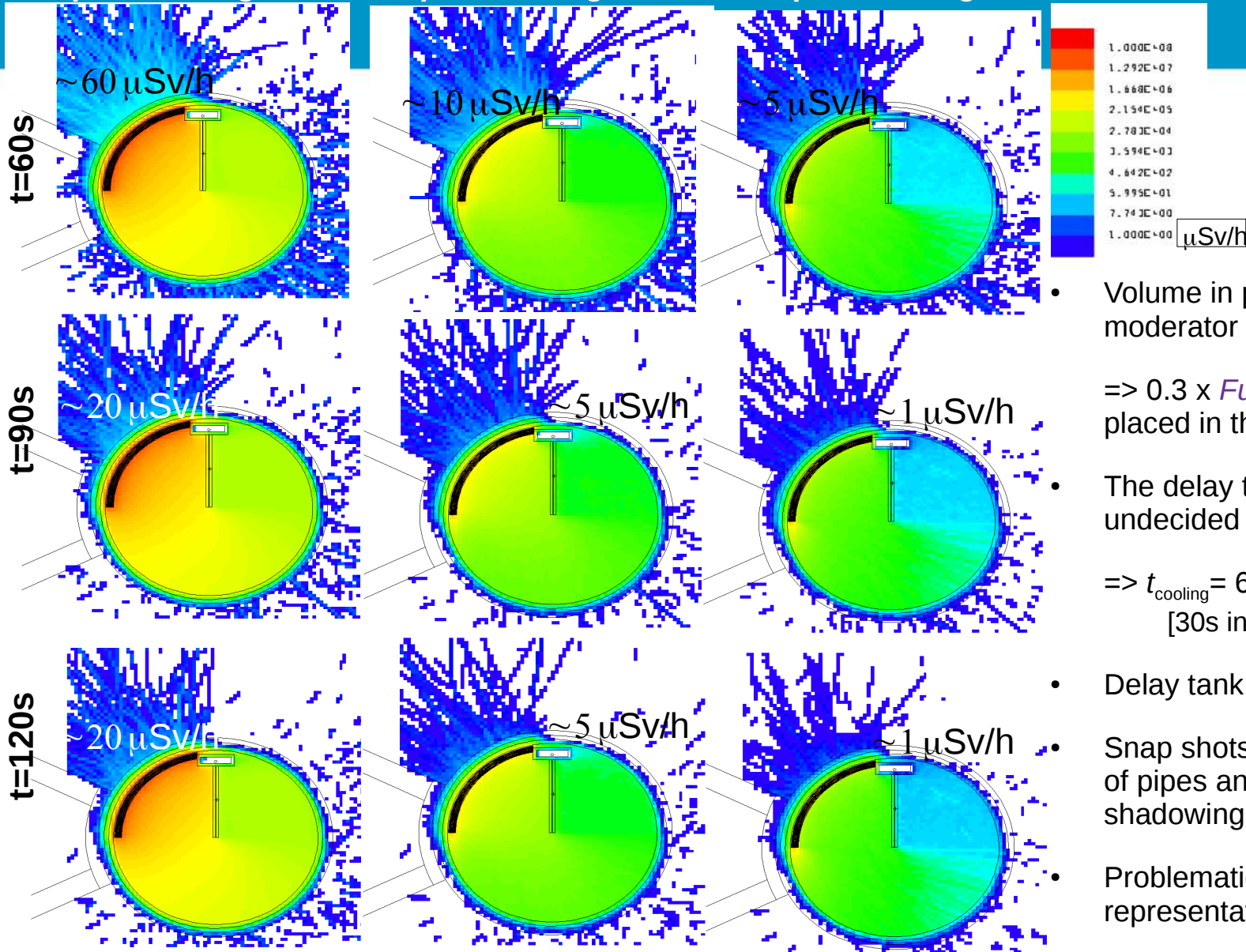


# 4 – delay tank outlet pipe

Pipe shielding: 0

Pipe shielding: 2cm Pb

Pipe shielding: 4cm Pb



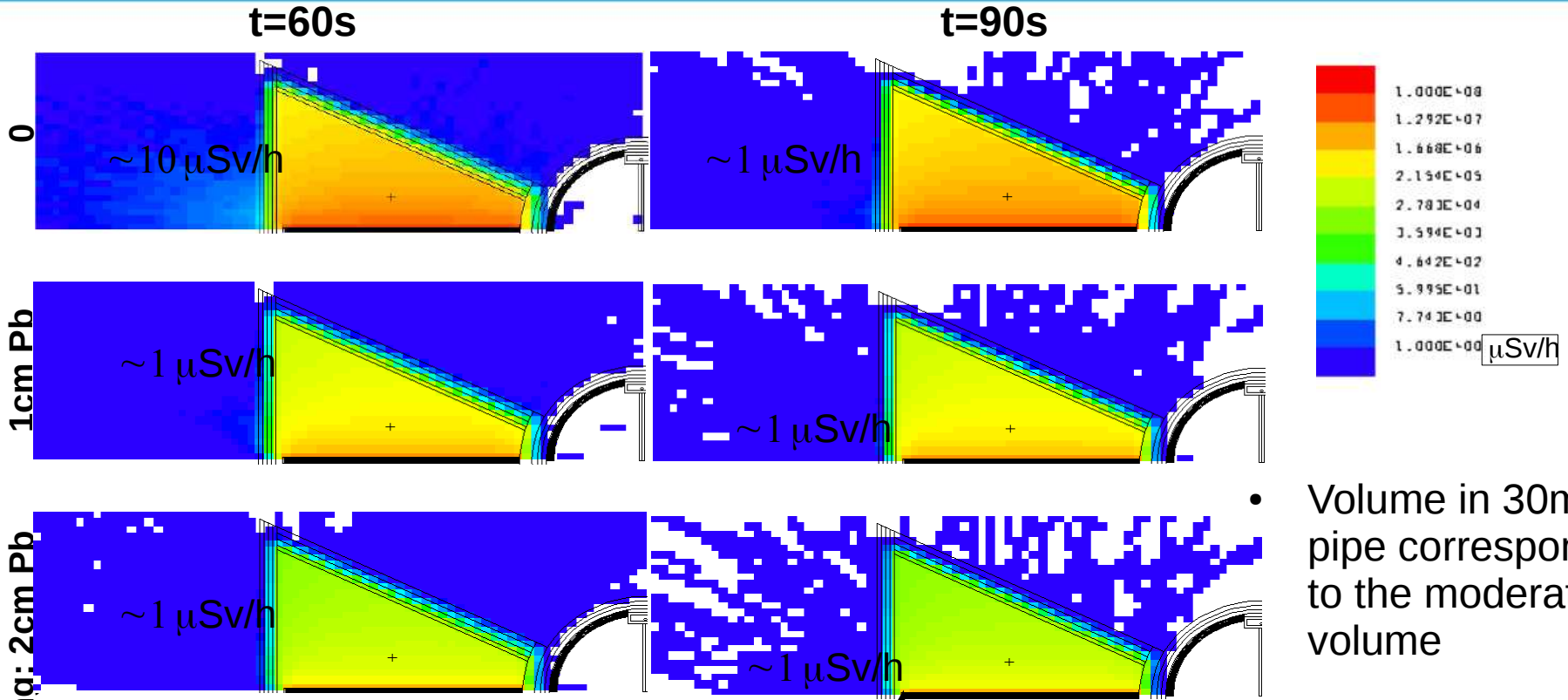
- Volume in pipe  $\sim 0.3 \times$  moderator volume  
 =>  $0.3 \times$  *Full source term* is placed in the pipe
- The delay tank size is undecided  
 =>  $t_{\text{cooling}} = 60\text{s}, 90\text{s}, 120\text{s}$   
 [30s in backup slide]
- Delay tank + pipe in place
- Snap shots are in the plane of pipes and delay tank => shadowing is over estimated
- Problematic region representative

# 4 – delay tank outlet pipe

- Shielding requirements on the outlet pipe depend on the size of the delay tank

Delay tank size	30s	60s	90s	120s
Outlet pipe shielding	10cm	4cm	2cm	2cm

# 5 – triangular rooms: pipes



Pipe shielding: 2cm Pb

1cm Pb

0

t=60s

t=90s



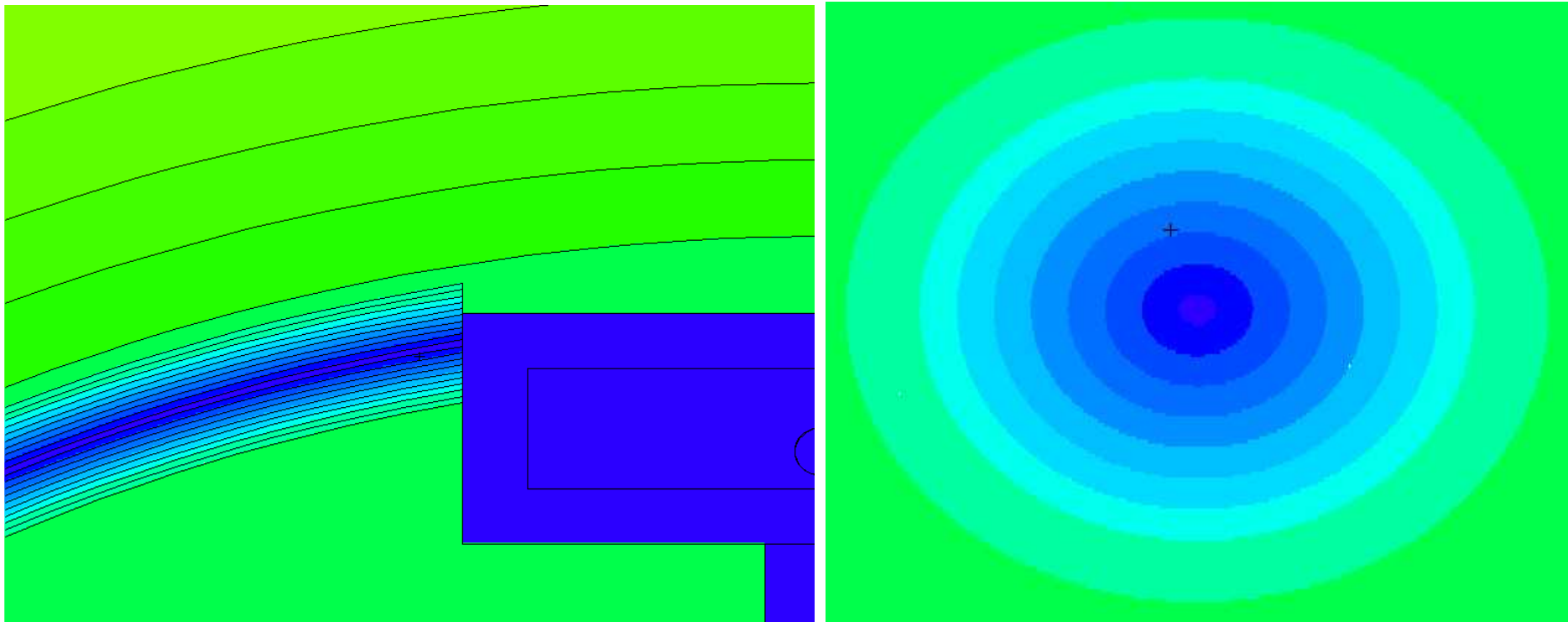
Pipe plugged by 10cm Pb

Delay tank size	60s	90s
Triangular room pipe shielding	1cm	0cm

- Volume in 30m pipe corresponds to the moderator volume
- Approach: Place *Full source term* at  $t_{cooling} = 60s, 90s$  is placed in a pipe in the triangular room

# Importance biasing

- Importance doubled every 2cm in lead and 25cm in concrete



Zoom in of delay tank and outlet pipe[left] and pipe cross-section [right].  
Colored by gamma importance.