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Concepts Of Operations for CSPEC, the cold chopper spectrometer of the ESS

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1. INTRODUCTION

The purpose of this ConOps document is to provide a brief description of the cold chopper spectrometer instrument at the ESS, CSPEC. The description includes both a high level introduction to the science case of the instrument as well as providing the framework and context within which the instrument will be designed, operated and maintained through its life-cycle. The document does not represent a detailed design which will be provided during the detailed engineering phase, phase 2.

The intended audience for this document includes all those involved in the construction and operation of CSPEC. It will also serve as a quick overview of the instrument's purpose, construction and operation for person/-s familiar in the field of neutron science. This document will be frequently updated.

2. HIGH LEVEL SCIENTIFIC REQUIREMENTS

The high level scientific capabilities of the cold chopper spectrometer CSPEC are based on the spatial and dynamic capabilities outlined in the CSPEC STAP report May 2014. In the CSPEC proposal, the long pulse structure and enhanced brilliance of the ESS have been exploited to develop a high performing cold chopper spectrometer that will gain an order of magnitude in neutron counting rate with respect to existing cold chopper spectrometers. It will probe low-lying excitations and relaxation processes in materials ranging from hydrogenous materials, polymers to strong electronic correlations, to name a few. A main focus of CSPEC is to enable routine in-situ or time dependent experiments that will open new scientific frontiers.

CSPEC high level scientific requirements:

1. Wavelength range = 2 – 20 Å.
2. CSPEC shall probe excitations up from 0.005 up to 20 meV.
3. CSPEC shall measure in repetition rate multiplication configuration.

4. CSPEC shall be capable of energy resolutions down to $\Delta E/E = 1\%$ in the cold regime for wavelength greater than 4 Å.
5. CSPEC shall be capable of spatial resolution $\Delta Q/Q = 2\%$.
6. CSPEC shall provide a signal to noise of 10^4 at 5 Å. Signal to noise is defined as the peak intensity of the elastic line of a vanadium sample versus background obtained far away at a time of flight when the background level has been reached.
7. The chopper cascade shall ensure that each incident wavelength arrives when the scattering from the previous incident wavelength has reached background levels.
8. The neutron beam at the sample position shall illuminate a sample area ranging from 4 x 2 cm^2 to 1 x 1 cm^2.
9. CSPEC should follow kinetic processes with time steps of one minute.
10. The detectors provide a detectable range between 5 – 140^o with a sample to detector distance of 3.5 m and a vertical detecteable range of +/- 26.5^o.
11. CSPEC shall probe magnetic excitations in magnetic fields up to 12 T.
12. CSPEC shall ensure the possibility to perform polarization analysis in the future.
13. The systems design shall provide the space and flexibility necessary to host and drive future developments.
14. Sample environment for the wide range of scientific cases studied on CSPEC must be consistent with the demands of signal to noise.

3. SUPPORTED SPECTROSCOPY MODALITIES:

3.1 Quasielastic scattering (non-crystalline condensed matter, powders, soft matter liquids)

Quasielastic scattering probes dynamics on the pico- to nanosecond scales and includes diffusion processes, tunneling, librational and rotational motions. The aforementioned motions are typically found in hydrogenous materials, soft-matter, biological systems and glassy compounds. Typically, these materials have very broad spatial correlations and as such the Q-resolution can be degraded to improve flux, or focus the neutron beam on a smaller sample (with the resultant degradation of divergence profiles). In contrast, the energy resolution must be freely tunable, from 5 µeV upwards, to adjust the experimental time window to the time scales of the motions of interest. The data that one extracts in a quasielastic experiment lie very close to the strong elastic line and any deviation from a conventional shape (a Gaussian or Lorentzian, in energy) of the elastic line makes it difficult to extract the information required. It is imperative that the signal to noise is optimised (10^4 at 5 Å) and the background is minimized and well understood. The neutron beam spot size for quasielastic scattering of non-crystalline materials must be able to vary from large, 4 x 2 cm^2, thereby optimizing the scattering intensities of dilute but abundant samples, to 0.5 x 0.5 cm^2 for compounds with small sample volumes.

3.2 Quasielastic scattering (Single crystal)

The comments made in the previous section remain true for quasielastic scattering from a single crystal except that the Q-resolution, which is closely matched to the energy transfer, must remain adequate to determine the lifetimes and spatial correlations across the entire S(**Q**, ω). The scientific interest in quasielastic scattering of single crystals is rooted firmly in hard condensed matter, typically magnetism or glassy behaviour of functional materials. Novel materials in these scientific domains are difficult to synthetize and result in small crystals as small as mm^3 size. It is therefore important to be able to focus the neutron beam to a small spot size while maintaining a clean divergence profile that can adequately probe S(**Q**, ω).

3.3 Inelastic neutron scattering (non crystalline condensed matter, powders, soft matter liquids)

Inelastic scattering occurs due to processes with discrete energy steps. These include collective excitations such as vibrational modes, stretching modes, density of states and spin waves. A powdered sample will scatter broadly (in Q) due to the almost isotropic texturing of the sample. As such the scattering profiles are broadened and the instrumental background must be minimal, well understood and free from spurious scattering. To gain optimal information from the scattering profiles it will be imperative to have access to theoretical models convoluted with the instrumental resolution and powder averaged.

3.4 Inelastic neutron scattering (Single crystal)

Inelastic scattering profiles from single crystals on CSPEC will provide 4 dimensional S(**Q**,ω) profiles across 8-10 incident wavelengths. Single crystal excitations are of most interest in the field of hard condensed matter. The single crystal sample will be rotated to provide the extra **Q** dimensions and it will be possible to measure S(**Q,** ω) in event recording as the sample is continuously rotated. To gain optimal information from the scattering profiles it will be imperative to have access to theoretical models convoluted with the instrumental resolution.

3.5 Kinetic measurements for all modes

A combination of the high flux and the multi-energy mode makes CSPEC most suitable for experiments that investigate time resolved kinetic phenomena, including pump-probe experiments and out of equilibrium behaviour. The high flux (potentially further enhanced by combining several pulses within the ESS timeframe) will enable monitoring of transient phenomena with a time resolution of minutes. For cyclic processes, time-resolved stroboscopic measurements will benefit both from the high flux and the multi-energy mode to probe the dynamic response of a compound to an external trigger with a time resolution in the order of seconds.

4. SYSTEM CHARACTERICS

4.1 System purpose

CSPEC is a cold chopper spectrometer that will extract cold neutrons ($2 < \lambda < 20$ Å) from the 3 cm butterfly moderator. The ~159 m, moderator to sample, distance enables measurements across a

~1.75 Å wavelength bandwidth using Repetition Rate Multiplication within each ESS frame. By rephasing the choppers the energy transfer range measured by CSPEC will cover 3 to 4 orders of magnitude, from few μeV (quasielastic scattering) up to 20 meV (inelastic scattering). The chopper cascade, optimised for energy resolutions down to $\Delta E/E = 1\ \%$, must ensure that each incident wavelength arrives when the scattering from the previous incident wavelength has reached background levels, irrespective of the scattering power of the sample. This is especially pertinent in a scientific age where the well-defined scattering features have been probed and the exciting science lies in scattering functions that are typically weak and broad in energy and reciprocal space. The technique is therefore highly background sensitive. The instrument must be considered and designed with signal to noise in mind. Special care has been focused in the design to minimize the background generated by the source, the primary and secondary spectrometer components. Sample environment for the wide range of scientific cases studied on CSPEC must be consistent with these demands of signal to noise. The neutron beam at the sample position will illuminate a sample area ranging from $4 \times 2\ \mathrm{cm}^2$ to $1 \times 1\ \mathrm{cm}^2$. The detectors will ensure the Q and E requirements (including ΔE and ΔQ) outlined in the CSPEC proposal.

The science case for CSPEC is very broad and will satisfy communities who study systems as diverse as strongly correlated physics to life sciences. A few examples include:

- Spin wave excitation spectra of novel materials, such as those with strong spin-orbit interactions that may lead to novel nanodevices.
- Magnon-phonon interactions in magnetothermal or multiferroic materials.
- Time dependence of the rotational or translational diffusive processes in enzyme catalysis.
- Dynamics of hydration processes and the structural relaxation of the glassy water.
- Time dependent phenomena of hydrogen storage in clathrates.
- Proton diffusion in metal organic frameworks.
- Diffusion dynamics and the relation to the ordering mechanism of solidification.
- Studies of in-operando proteins such as those involved in photosynthesis: light-induced dynamics of the antenna pigment/protein complexes.

4.2 System overview

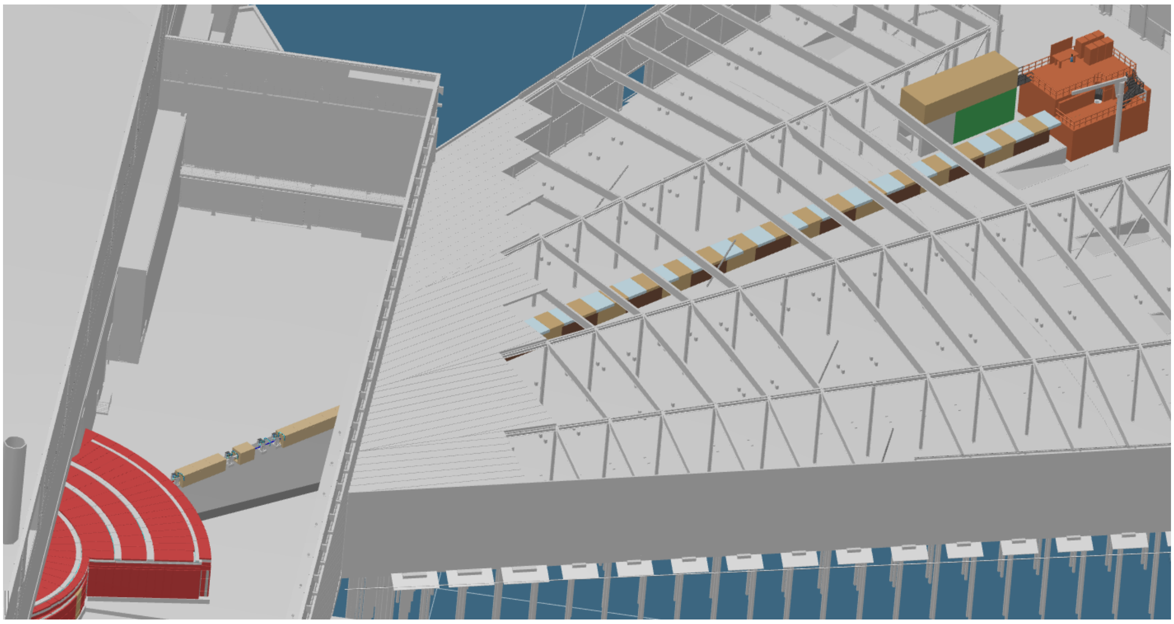
The conceptual CSPEC instrument is subdivided into the following main functional blocks:

- Neutron optics
- Chopper system
- Shielding
- Shutters
- Detector tank
- Detectors
- Sample environment
- Beam monitoring
- Beam stop
- Control hutch

- Instrument control

Personnel Safety System, PSS. All components have to be defined and designed to fulfill the high level requirements as the basis for the detailed functional and non-functional instrument and component requirements.

4.3 General



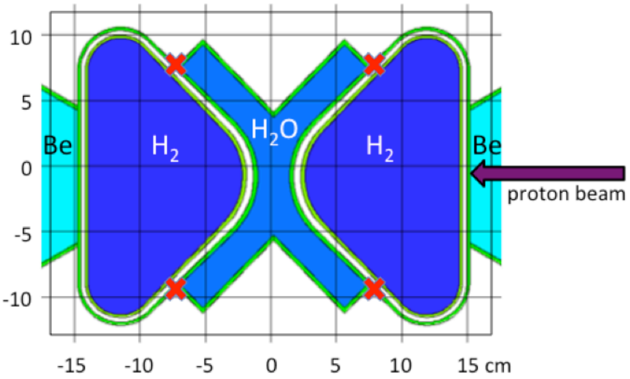


Figure 1: Engineering drawing of the CSPEC layout from moderator to sample cave.

Figure 2: Cold and thermal moderators. Beam port axis is marked with a red x.

CSPEC is positioned in the west sector on beamport W3. The spectrometer will extend over three different buildings – experimental hall 2 with building designation D03, the guide hall with building designation E02 and finally the experimental hall 3 with building designation E01, see Figure 14.

4.4 Beam extraction

The guide begins at 2 m and will view the cold moderator of the top butterfly moderator. CSPEC requires extraction of a broad divergent (+/- 1^{o} @ 3Å) cold neutron beam ranging from 2 to 20 Å. It should be noted that time of flight spectroscopy is a very flux intensive technique that is rarely Q limited. As such it is important to extract and transport a wide divergence. For example, scattering from soft matter compounds, typically with $\lambda > 5$ Å, can accept a divergence of ± 2^{o} due to the broad features in the Q-dependence of the scattering profiles. The beamport axis lies at the point between the cold and thermal moderators, marked by a red x in Figure 2. The guide must rotate 1^{o} and translated slightly with respect to the beam port axis to uniquely view the cold moderator. Figure 3 shows the beam extraction under current consideration by the ESS. The beam extraction unit will be equivalent for all instruments.

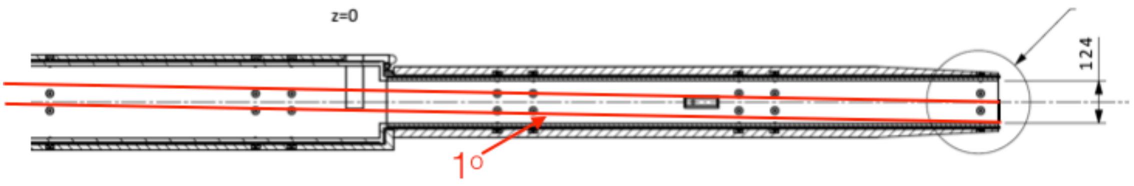


Figure 3: Beam extraction unit under ESS consideration. The red lines demonstrate a rotation of 1^{o} of the guide to uniquely view the cold moderator.

4.5 Neutron optics

The instrument length, ~159 m, provides a 1.75 Å wavelength bandwidth. The beam transportation system shall transport cold neutrons in the range from 2 to 20 Å with a broad divergence. The guide concept is driven by requirements

- to optimised cold flux with the divergence requirements outlined in the high level scientific requirements.
- to curve twice out of line of sight within the bunker.
- to take advantage of the self shielding properties of the target below the moderator that provides a low background region.
- to ensure the guide width does not exceed 8 cm at the pulse shaping chopper and 1.8 cm at the monochromating chopper .

These requirements will optimise signal and mimise noise.

McStas simulations have been performed to validate the guide concept. Guide simulations, inclusive of gaps for choppers and realistic guide lengths (0.5 & 2 m), ensure that the correct flux and divergence profiles are represented. The guide begins at 2 m and will view the cold moderator of the top butterfly moderator. CSPEC requires extraction of a broad divergent (+/- 1^{o} @ 3Å) cold neutron beam ranging from 2 to 20 Å.

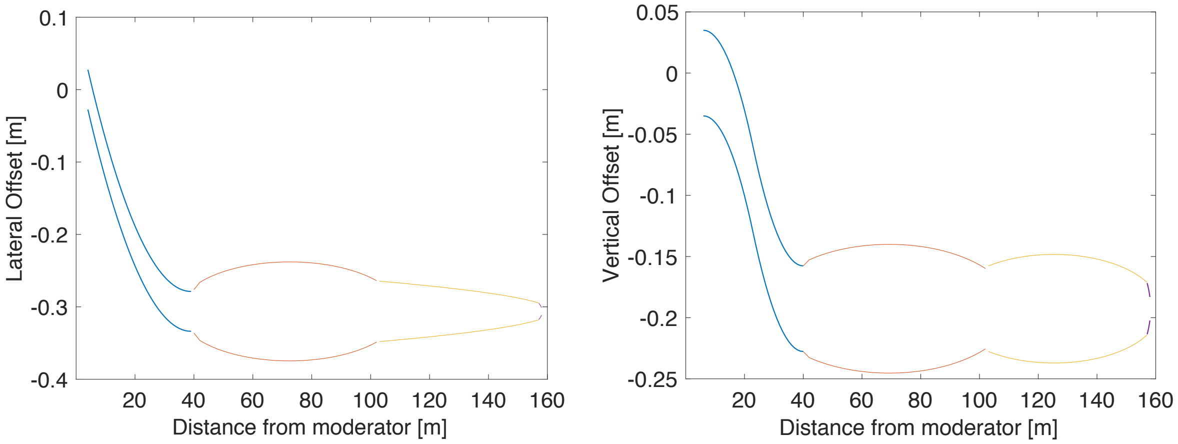


Figure 4: Overview of the guide (left) in the horizontal direction, and (right) in the vertically direction.

The guide is curved out of line of sight in the vertical direction with an s-bender, radius of curvature of 2000 m, that curves the guide out of line of sight within the bunker. The decision to curve out of line of sight in the vertical direction is based on (a) the self-shielding properties of the target and (b) to curve out of line of sight vertically is easier (considering the 3 cm high moderator) than curving out of line of sight of the broad horizontal moderator. The rotation of the guide to view the cold moderator is corrected with a horizontal curvature of the guide, radius of curvature = 2000 m. The beam is approximately horizontal after 40 m from the source, shifted 30 cm horizontally and 19 cm vertically from target center line, see Figure 4. The guide, although shifted horizontally, remains within the piled section of the guide hall, E02. The sections after the curvature are two elliptical sections punctuated by the choppers. An elliptical guide is able to transport, from focal point to focal point, almost a full brilliance across large distances while maintaining a clean divergence profile. The guide width at the pulse shaping chopper does not exceed 8 cm. The final section of the second elliptical guide focuses on the monochromating chopper so that the guide exit width is reduced to 1.8 cm, required to access the minimal burst times for high energy resolution measurements. The final guide component is a variable focusing nose that will enter the sample area, part of the evacuated detector tank, to minimize further background scattering and finish 0.2 m from the sample. In the case of large sample environment a part of the final section can be removed. As such there will be 4 interchangeable guide components: (1) Unfocussed up to 20 cm from sample (2) Focussed up to 20 cm from sample (3) Unfocussed up to 50 cm from sample (4) Focussed up to 50 cm from sample. The beam spot size at the sample position with the nominal focussing nose is 4 x 2 cm^2, the focusing nose will provide a beam spot of 1 x 1 cm^2 at the sample position. The size of the flux on sample for the focussed beam is 1 x 1 cm^{2,} as opposed to point like, to ensure that the divergence profile remains acceptable for single crystal measurements. The CSPEC team are currently working on further investigations with guide manufacturers to finalise the exact details of the guide. These should be completed in the next few months.

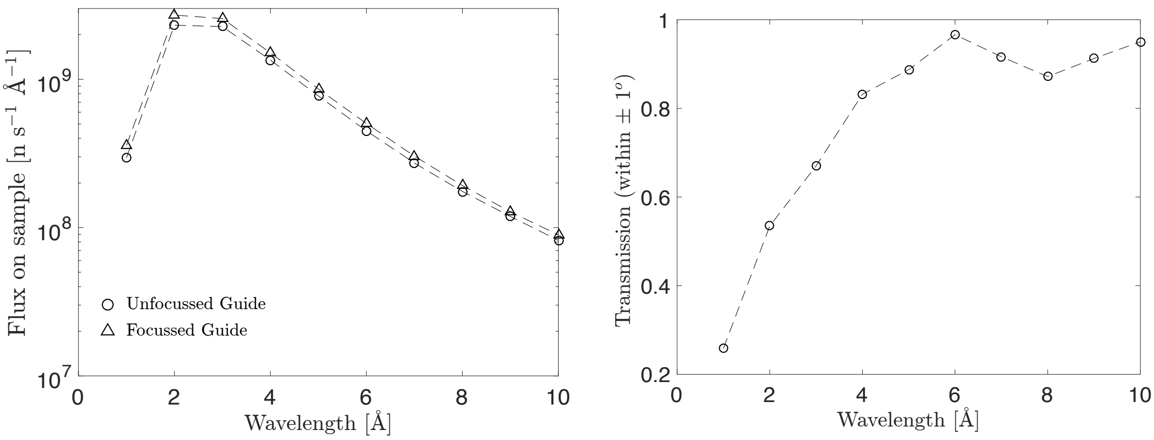


Figure 6: (left) Flux on the sample as a function of wavelength for the unfocussed guide (end of guide - sample = 20 cm) and with a focussed final section. (right) Transmission of neutrons through the guide, within +/- 1° divergence, as a function of wavelength.

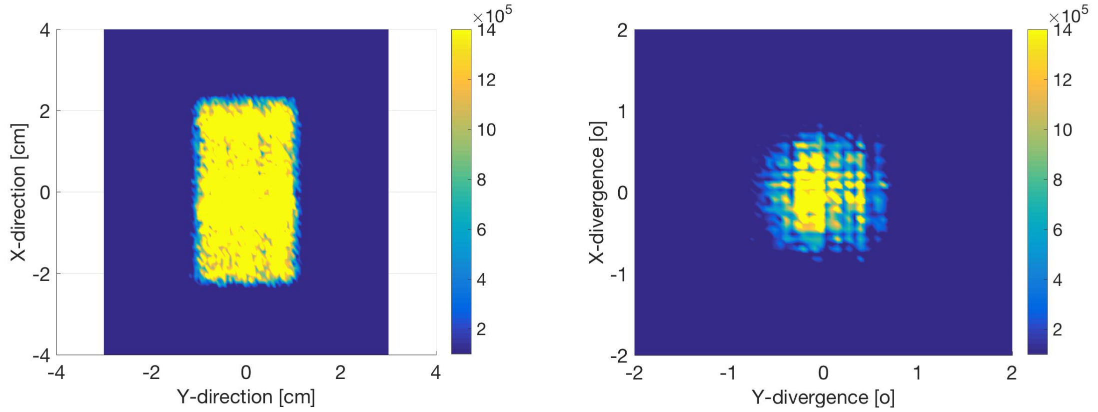


Figure 7: Unfocussed guide (left) Flux profile at the sample position and (right) divergence profile at the sample position. λ = 3 Å.

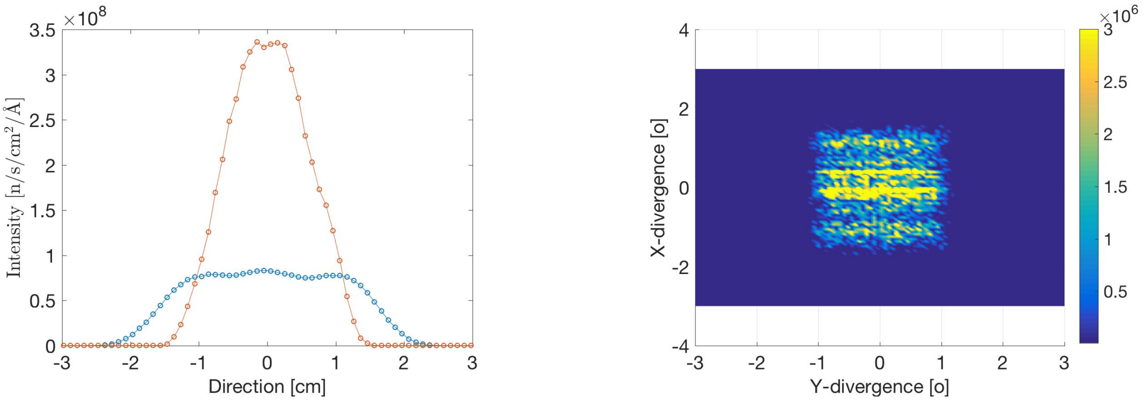


Figure 8: Comparison of the flux at the sample position for the focussed nose and the unfocussed nose (left) Flux profile at the sample position and (right) divergence profile of the focussed nose at the sample position. λ = 3 Å.

Component	Information
1st section	Starts at 1.9 m, 0.5 m piece. WxH = 0.055x 0.07. 1 channel, m = 3 Rotated by 1^{o} and translated to focus on cold source
Curving section 1	34 straight pieces (0.5 m each). RoC1 = 2000 m, RoC2 = 1475 m, WxH = 0.055x 0.07. 1 channel. Rotated by (-(Length/RoC1) rad,(- Length/RoC2) rad,0) w.r.t previous guide piece, m = 3
Curving section 2	39 straight pieces (0.5 m each). RoC1 = 2000m, RoC2 = 1475 m, WxH = 0.055x 0.07, 1 channels. Rotated by ((Length/RoC) rad, (- Length/RoC) rad,0) w.r.t previous guide piece, m = 3
Elliptical section 1	Length: 66.03 m, Focussing parameters = w_in x h_in = 3 x 10 m from end of guide = w_out x h_out = 2 x 3 m from end of guide, m = 2.5-4.
Elliptical section 2	Length: 52 m, Focussing parameters = w_in x h_in = ∞x10 m from end of guide = w_out x h_out = 0.5x0.5 from end of guide, m = 2.5-4.
Elliptical section 3 (approaching monochromating chopper)	Length: 0.525 m, Focussing parameters = w_inxh_in = ∞x∞ m from end of guide = w_out x h_out = 8x10 from end of guide unfocussed nose = w_out x h_out = 0.5x0.5 from end of guide focussed nose, m = 2.5-5.
Focussing section (2 x 4 cm^2)	Length: 1.3 m, m = 4, 2 channel, Focussing parameters = w_in x h_in = 0.8 x 1 m from end of guide
Focussing section (1 x 1 cm^2)	Length: 1.3 m, m = 2, 1 channel Focussing parameters = w_in x h_in = 0.1 x 0.05 m from end of guide

Table 1: Guide component parameters. RoC = Radius of curvature (m). WxH = width x height (m)

The entire guide will be held in vacuum housing. Alignment procedures as advised by the guide manufacturers will be followed. ESS Optics group will monitor the beam performance and realign when needed.

4.6 Choppers

The choppers cascade, in conjunction with the guide and detectors, must access the energy resolutions outlined above and in the CSPEC Proposal. In addition, the chopper cascade must ensure that the instrumental background is reached between adjacent incident pulses. The technical choice for choppers considers, as a high priority, reliability. It is for this reason that

- Low speed choppers will be optimized to absorb high energy neutrons and are positioned outside the bunker with easy access to the chopper pits.
- High speed choppers are all positioned outside the bunker with easy access to the chopper pits.
- The high speed choppers are symmetric.
- The chopper blade diameter does not exceed 700 mm.
- Frequencies do not exceed 350 Hz (most experiments will run at frequencies of 250 Hz or less.

Table 2 gives an overview over the chopper system and the characteristics of the various axes. The absolute positions may change slightly when engineering realities are considered.

Chopper Name	Position (m)	Single Blade (SB) or Counter Rotating (CR)	Diameter (mm)	Number of openings & slit width (cm)	Max Frequency (Hz)	Absorber	Bearing
BandWidth 1	(-0.37,0.13,31.93)	SB	700	1 & 81°	14	Steel (B coated)	Hybrid ball bearings
BandWidth 2	(-0.37,0.13,39.44)	SB	700	1 & 99°	14	Steel (B coated)	Hybrid ball bearings
BandWidth 3	(-0.37,0.13,43.44)	SB	700	1 & 111°	14	Steel (B coated)	Hybrid ball bearings
BandWidth 4	(-0.37,0.13,45.45)	SB	700	1 & 116 °	14	Steel (B coated)	Hybrid ball bearings
Pulse Shaping	(-0.37,0.13,105.6)	CR	600	3 & 23°	350	Carbon fibre (B coated)	Magnetic
Mono_RRM	(-0.37,0.13,158.45)	SB	600	1 & 2.6°	350	Carbon fibre (B coated)	Magnetic
Monochromating 2 x(double Slit)	(-0.37,0.13,158.5)	CR	600	1 & 2.6°	350	Carbon fibre (B coated)	Magnetic

Table 2: Overview of the chopper cascade with relevant parameters.

The system is comprised of four bandwidth choppers (BW) that define the useful wavelength band at the detector position, a pulsing chopper pair at 2x/3 m and a monochromating chopper pair at x m (x = distance from the source to the monochromating chopper). A pulse removal chopper just in front of the monochromating chopper pair will ensure the clean separation of pulses in repetition rate configuration.

It is currently unclear what the signal to noise at the sample will be. In particular, there is substantial concern about the high energy prompt pulse resulting from the protons on the target. These high energy particles are observed on all chopper spectrometers at spallation facilities with varying degrees of intensity. Curving the guide twice out of line of sight in conjunction with the long instrument length should limit the prompt pulse. However, due to the substantial uncertainty there should be a mitigation strategy. A T0 chopper at 28 m rotating at 14 Hz will allow the transmission of 2 Å neutrons while reducing the prompt pulse feature by an order of magnitude.

4.6.1 Bandwidth choppers

BW choppers ensure that only the required wavelength bandwidth is transmitted through the guide to the sample. The BW choppers will rotate at the ESS source frequency, 14 Hz. Although certain instruments are able to function without BW choppers, albeit at a reduced capability, a chopper spectrometer loses all capability without these choppers. The BW choppers will be steel disks with B4C coating. The steel thickness of these choppers will be enhanced to reduce the effect of the prompt pulse, although not to the extend that a T0 chopper would. At the time of the CSPEC scope setting meeting the CSPEC team presented a solution with two BW chopper in the bunker. This is a very clean solution with respect to the long ESS time pulse. However it caused considerable consternation with respect to the reliability of the instrument since the bunker is a very complicated structure to access and work in. Considerable time has been spent to position the BW choppers outside the bunker providing easy access to the choppers during commissioning and in case of failure. In this case 4 BW choppers are required. In the following figures a configuration is shown with choppers at 32, 39 and 42 and 45 m. Figure 9 shows the transmission of the 4 BW choppers as a function of wavelength up to 100 Å.

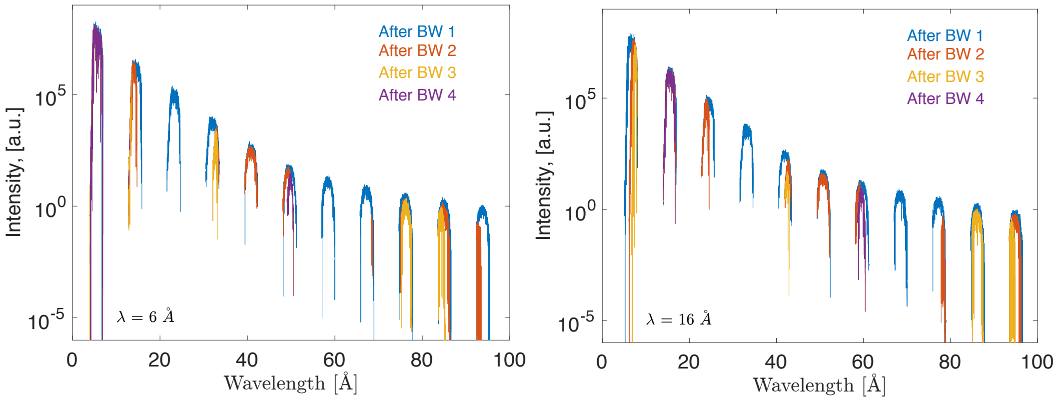


Figure 9: Effect of the bandwidth choppers, positioned outside the bunker, on the transmission of neutrons through the CSPEC guide for wavelength bands around $\lambda_{central}$ = 6 and 12 Å, McStas simulations.

Figure 9(left) shows the transmission of the BW choppers when the required bandwidth at the sample is around 6 Å while Figure 9(right) shows the required bandwidth at the sample around 16 Å. Figures 9 show that the required bandwidth is transmitted correctly without any extra spurious scattering up to 50 Å. At 50 Å the flux is at least 10^{-5} with respect to the principal bandwidth and therefore will provide an acceptable background.

4.6.2 High speed choppers

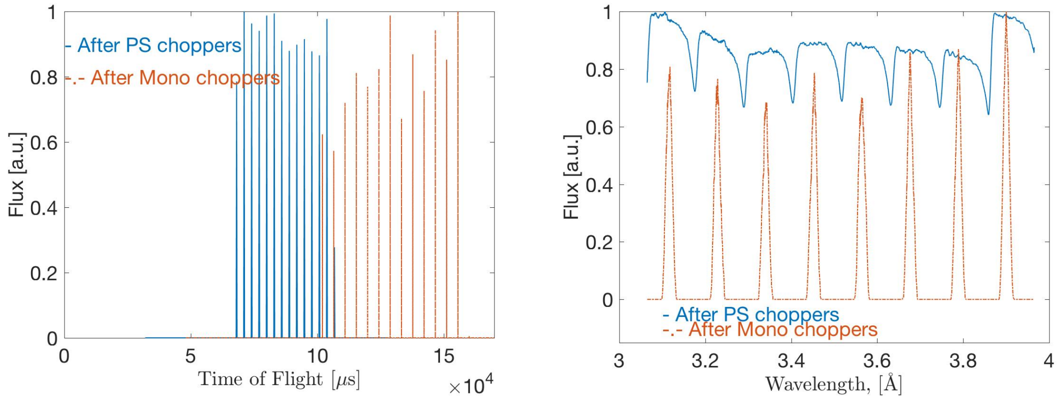


Figure 10: McStas simulations: (left) time of flight dependence and (right) wavelength dependence of neutron flux profiles after the pulse shaping and monochromating choppers for $\lambda_{central}$ = 3 Å with pulse shaping choppers rotating at a frequency = 112 Hz and monochromating choppers rotating at a frequency = 224 Hz.

The high speed choppers are the pulse shaping, RRM and monochromating chopper pair with frequencies up to 350 Hz. The pulse shaping choppers blades have 3 symmetric windows and run at a frequency of 1/2 "F" ensuring that the total frequency is a multiple of the ESS source frequency. The monochromating choppers run at a frequency "F", again ensuring a multiple of the ESS source frequency.

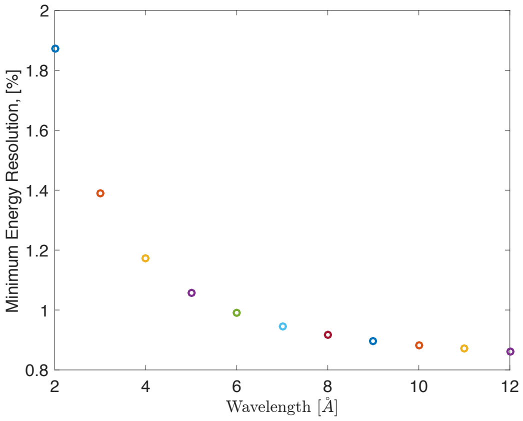


Figure 11: λ dependence of the miminum energy resolution on the CSPEC chopper spectrometer with the monochromating chopper frequency at 300 Hz.

The narrow bandwidth of CSPEC, in conjunction with the cold nature of the neutron spectra, means that the time required to reach background levels, between subsequent pulses, does not vary substantially. An optimised solution to vary the time between pulses is therefore not required. Frame overlap of RRM pulses is avoided via the use of the RRM chopper, an extra blade before the monochromating choppers (within the same housing) rotating at a frequency "F"/n (with n = integer) of the monochromating chopper frequency.

Figures 10 shows a McStas simulation of the clean separation of the pulses, in time and wavelength, on CSPEC with the pulse shaping chopper frequency at 112 Hz and the monochromating choppers frequency at 224 Hz.

In Figure 11 the chopper configuration that are presented provide a minimum energy resolution of ΔE/E < 1 % for λ > 5 Å with a 300 Hz chopper frequency and 700 mm disks as required from the high level scientific requirements.

4.7 Shielding

4.7.1 Guide shielding

The shielding will satisfy the biological safety requirements in and around the length of the instrument for those operating in the vicinity with beam on sample.

The shielding beyond line of sight is designed to shield against gamma flux only. These flux estimates are obtained by considering that all the neutrons escaping from the guide or absorbed are converted to 4.4 MeV photons, the photon energy of the gamma resealed after the interaction between the neutron and a glass guide substrate.

In addition, extra care will be taken to limit any fast neutrons that have been able to stream through the guide housing by using steel shielding closely placed around the guides at relevant positions as illustrated in Figure 12.

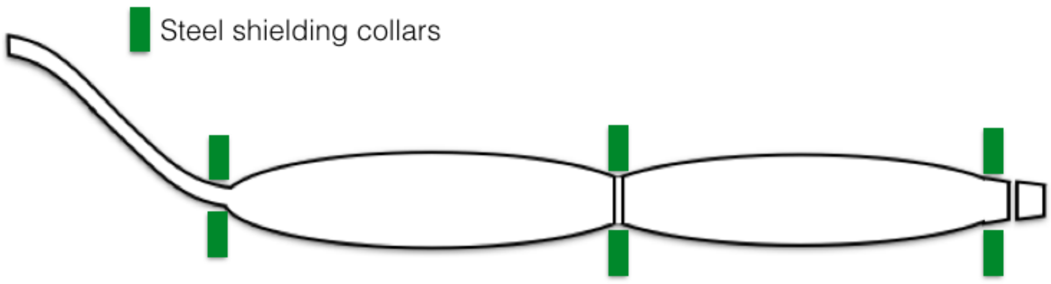


Figure 12: Cartoon of the shielding collars around the guide.

The chopper pits will be used to enable maintenance work but also to create large volumes in which multiple scattering events of the incident beam will reduce the intensity and energy of high-energy particles derived from the prompt pulse.

4.7.2 Detector tank shielding

The flux estimates for the detector tank are obtained by considering that all the neutrons absorbed by a hydrogen sample release 2.31 MeV gamma photons. Secondary scattering effects that will increase the background levels of the experiment are however of great concern. The floor beneath the detector tank will consist of boronated concrete to limit floor shine. Skyshine will be limited by a polyethelene/B4C laminate cover that will cover the detector tank.

The shielding will also ensure that the signal to noise (signal = elastic line) on the sample is at least 10^4 for a typical vanadium sample, with signal determined by the elastic intensity and the noise measured at a time of flight position where the signal has decayed to background levels. The calculations performed to achieve this signal to noise should include all components on CSPEC and scattering background contributions from nearby instruments.

It should be noted that although we are now costing HD concrete for shielding purposes, it is more likely that a laminate of other materials (boronated PE, steel cans containing Fe_3O_4 nanoparticles and a hydrogen rich fluid or wax) will be employed to optimise shielding and cost.

4.7.3 Beam stop

CSPEC will require to access low Q regions to deliver its scientific case. A beam tube around the incident beam at $2\theta = 0$ deg will be provided in the detector wall, covered in a lithium based compound, that will end in an opening surrounded by concrete.

4.8 Sample environment:

The science case for CSPEC covers a broad user community. The ESS science case strongly focuses on the ability to probe time dependent phenomena. Equally, the science case for CSPEC has a strong component that focuses on time dependent phenomena and in-operando experiments. The sample environment, which includes the sample environment pot, must provide for such experiments.

The area for sample environment is integral in the design of the detector tank and is designed with a broad range of apparatus in mind. Sample environments will be optimized for the instrument with stringent signal to noise requirements and, where possible, the tails of cryostats and furnaces will be removed to limit background contributions.

To address the scientific questions as outlined in the CSPEC proposal the following sample environments will be available from day one, as outlined in the minutes of the Scope Setting Meeting.

- Cryofurnace (3-600 K, $\Delta T = 0.1$ K) (CSPEC),
- multiple sample changer (up to 8 samples), possible collaboration between ESS and TUM (CSPEC),
- sample rotation stage and goniometer (CSPEC),
- Dilution capabilities and access to a 12 T magnet (ESS Pool).

- In-situ capabilities (In-kind).

In-situ environments will be provided by in-kind contributions and collaborations. A current collaboration with J. Pieper (University of Tartu) will develop the technical requirements for a pump probe experiment on biological systems.

The sample environment from the sample environment pool will be available for use on CSPEC, principally a high field magnet (12-15 T) and dilution capabilities We will provide input to the design and manufacturing details of the high field magnet.

4.9 Sample and Detector vessel:

The secondary spectrometer is a 3.5 m flight path and the detector tank will accommodate the detector range with an angular range of 5° ➔ 140° horizontally and ± 26.5^{o} in the vertical direction (total detector height: 3.5 m). To minimize secondary scattering, the internal walls of the detector tank will be covered in a neutron absorbing material, such as Cd, that does not strongly degas. Vertical vanes between detectors columns will eliminate secondary scattering effects from the detectors and the housing. An oscillating radial collimator will further reduce background from bulky sample environments.

The sample environment area, 1000 mm in diameter, will permit sample environment to be mounted and operated from the top aswell as from the side. The side opening will also enable the user to view the sample environment. Non-standard equipment can also be aligned using a 6 axes goniometer positioned on the floor of the sample environment area.

The sample and detector vessel will be evacuated to cryogenic pressures (10^{-6} mbar). This allows one to minimise the thickness of any tails on cryogenic equipment and thus any scattering from it. The cryogenic evacuation will extend to the monochromating chopper at which position there is an Al window.

The sample area can be separated by the rest of the detector tank to facilitate the exchange of sample environments. The sample area will be separated from the main detector vessel by an Al window that can also be used for experiments requiring ambient pressure conditions. Separating the sample area from the rest of the detector vessel also makes it possible to reduce the Al windows required before a ^{10}B-multigrid detector, which is the technology we are pursuing at this stage, since then the detector vessel vacuum can be considered as static. A technical solution to separate the sample environment area from the rest of the detector vessel is under consideration and is presented in the Preliminary System Design Description.

Special care is taken to ensure a non-magnetic vessel that enables high magnetic field measurements (up to 12 T) and polarization analysis as planned for the upgrade stage of the instrument.

4.10 Detectors

The detectors will cover an angular range of of 5° ➔ 140° horizontally and ± 26.5^{o} in the vertical direction. Assuming a minimum flight path uncertainty of $\Delta L = 15$ mm, the time resolution of the detector is matched to the primary spectrometer. In the scope setting meeting the CSPEC team agreed to provide a path forward with respect to detector technology. The CSPEC team are committed to the development of ^{10}B multigrid technology under the understanding that the responsibility is shared between all the partners of the instrument, TUM, LLB and ESS. We would like to clarify that if the technology does not meet the high level scientific requirements then an alternative will be pursued. Results from the position sensitive multigrid ^{10}B demonstrator, installed in the detector tank of the cold chopper spectrometer of the SNS, CNCS, adjacent to ^{3}He detectors, remain very convincing.

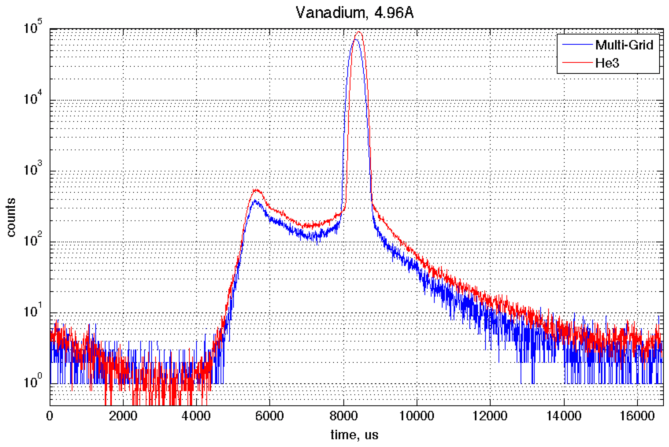


Figure 13: Comparison of the scattering from an isotropic scatterer (Vanadium) onto the ^{10}B multigrid detector demonstrator and He^{3} detectors. Counts normalised to peak.

Comparisons between two the ^{3}He and ^{10}B detector technologies show very similar signal to noise and energy resolution across the time-of-flight of the detectors, Figure 13. The latest results are shown on the ESS Wiki Detector group page and will be available in the Arcxiv paper provided by the ESS detector group. A ^{10}B multigrid detector, 2.8 m high and at least 50 cm wide, will be installed on TOFTOF at TUM for further tests.

4.11 Shutters

A light shutter is provided by the ESS at the guide entrance. This shutter will be a 50 cm thick steel absorber and used only during beam shutdown to stop the photons from activated components in the monolith. An additional light shutter will be placed shortly after the bunker wall. The combination of the two shutters will enable the team to enter the chopper pits when analysis and maintenance of the choppers are required.

4.12 Beam monitoring

Beam monitoring will be essential both for commissioning and calibration purposes. Neutron flux beam monitors will be positioned after each chopper and after the slit system. The monitors that determine the transmission profile of the sample, just after the slit system and after the sample, will resolve the incident wavelengths in rate repetition configuration. Whether the monitors remain in place for the duration of the experiment or can be remotely removed is not yet clear.

4.13 Vacuum monitoring

The ESS vacuum team are responsible for monitoring of the instrument vacuum. This includes the guide vacuum (10^{-3} mbar) and the detector tank vacuum (10^{-6} mbar). It does not however include the vacuum of the chopper systems which is included in the chopper design and implementation.

4.14 Technical laboratories.

CSPEC requires a laboratory for maintenance work and basic sample preparation. Ideally this is positioned close to the control hutch. Some preparation space can be on top of the detector tank. Further preparation space, at least 20 m^2, is required and contains basic equipment with access to a glovebox for moisture and air sensitive materials, space for handling of powders and liquids, a balance (0.1 mg precision), microscope, sample holders and a furnace for drying materials. A range of crystal mounts and standardized Al and Cu sample cells should be available at the instrument to meet the needs of the experimental team. The instrument will rely on the availability of a sample alignment station to ensure that single crystal experiments do not waste a substantial amount of time in the case of misaligned crystals. Storage space for samples before and after the experiment will be provided close to the instrument for samples with low radiation levels, and in the ESS sample storage area for high doses.

4.15 Personnel Safety System, PSS

Personal safety systems will be put in place as defined by ESS in line with Sweden's radiation safety regulation.

4.16 Control hutch

The control hutch must provide a good working environment that optimises the users ability to perform the experiment, from scientific discussion to data analysis. The work environment must provide natural light, thermal comfort, sufficient space to enable a team of 6 to work, reduced noise and limited vibrations.

4.18 Instrument control and data collection and processing

The instrument control, data storage and processing is provided by DMSC and is not part of the CSPEC instrument workpackage. It is therefore not costed. Extra manpower will be needed in phase 4, cold commissioning, to optimise instrument control and data reduction. The instrument control shall enable to remote control of all necessary technical parts, i.e. the chopper parameters, motors, such as the slit systems and the focussing guide, and sample environment.
For commissioning and instrument control, monitor counts after each chopper set should be available and the time-of-flight and position profiles on the detectors. These data must be available in minimal time to limit delays in the commissioning process.

Count rates:

CSPEC expects to have a flux on the sample up to 9e7 n/s with $\Delta E/E = 3\%$ at 3 Å. A sample that scatters 10 % of incident neutrons, results in ~ 9e6 n/s in 4π for a spin incoherent isotropic scatterer and therefore 2e6 n/s in 2.65 Steradian as a global rate. For an isotropic scatterer this will provide ~ 10 n/s per pixel (2.5 x 2.5 cm) however a Bragg peak from a compound with high crystallographic symmetry can give rise to $1\text{x}10^4$ n/s across a few pixels. The resultant data collected rises to ~ 20/30 MB per second (12 bytes per neutron stamp) corresponding to 14.4 TB data collected daily at 1MW ESS beam power. Current day experiments on cold chopper spectrometers already struggle to extract and process data, with processing times up to 10 minutes. It will be essential for the ESS to process data on minute timescale, such that a data set can be viewed in minimal time, thereby enabling in-situ and time dependent experiments, a main scientific goal, on CSPEC.

For the data collection and processing, all instrument parameters are recorded in event mode. It is essential to provide software at the instrument that enables time-of-flight and absolute detector positions to be transformed to $S(\mathbf{Q},\omega)$ for each incident wavelength. The primary data analysis considers instrumental resolution. For operations it is essential to provide theoretical software to analyse the data extracted.

5. OPERATIONAL CONCEPTS CSPEC

5.1 Operational environment

CSPEC is positioned in the west sector on beamport W3, see Figure 14. CSPEC will extend over three different buildings – experimental hall 2 with building designation D03, the guide hall with building designation E02 and finally the experimental hall 3 with building designation E01. The instrument will be operated in a controlled environment with a temperature of 22±2 °C all year round.

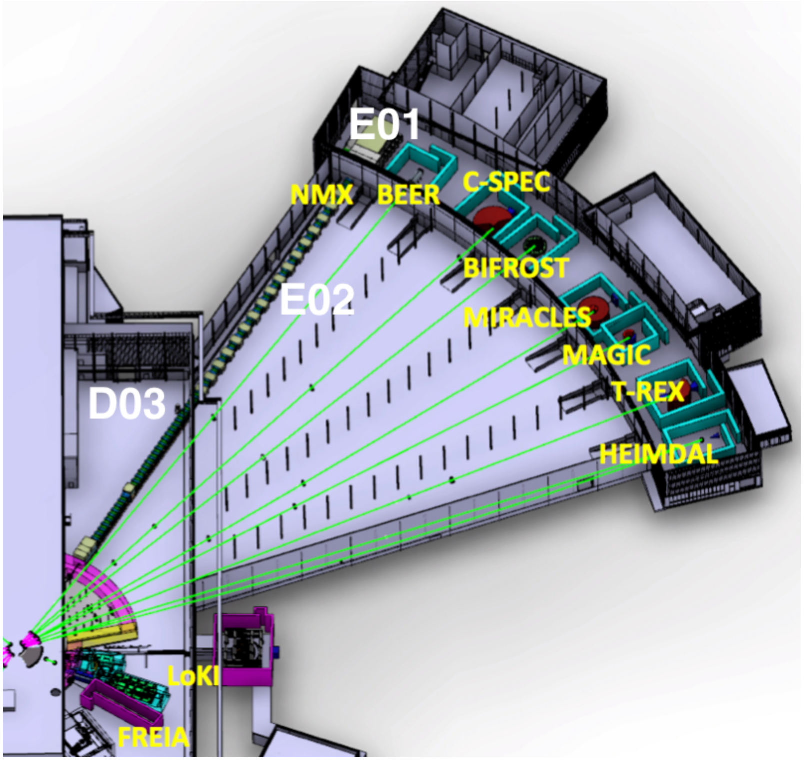


Figure 14: Beamport allocation in the west hall

The floor height in D03 is 2 meters below target centerline. The floor in the E02 is 1 m below target centerline and in E01 it is 3 m below target centerline. Floor loading in the D03 and E01 as well as the guide hall must not exceed 20 tonne/m^2. Floor stability in the halls is specified to be maximum 3 mm w.r.t elastic movement and another maximum 3 mm due to creep/deformation.

The crane in D03 and E01 is a 10 tonne crane that extends throughout the hall. The detector vessel is approximately 30 tonne and therefore a solution for the installation of the detector vessel needs to be found. The hook heights are 7 and 10 m in D03 and E01 respectively, with respect the to floor. In E02 a gantry crane extends along the hall.

Utilities and media are brought to the instrument from the gallery in case of D03 and along the wall separating D03 and E02. Media include: DIH_2O, N_2, instrument grade compressed air, cooling water low. Utilities include: office IT, office comms, power, MPS, PSS, DMSC and ICS. For detailed and updated listing of requirements and/or specifications related to operational environment see the System Requirements Document.

The ESS facility has 5 different operating modes, ref [ESS-0003640 Conops]: Shutdown, Studies, Studies on Target, Startup and Production. These modes have various impact on instrument operations. Pure experimental work can only be conducted during ESS-mode Production. Access to instrument equipment for maintenance, calibration, cold commissioning is mainly done during Shutdown, Studies and Studies on Target – naturally after due safety assessment and still possibly with some restrictions. During Startup instrument operations is limited to alignment, commissioning and calibration runs.
When ESS has entered into a steady-state operations phase the following principal schedule may apply:

- 200 days/year of neutron Production for the ESS users after 2026,
- Proton beams will be on target for ~225 days/year,
- Two long Shutdowns, one in winter (~6 weeks) and the other in summer (~10 weeks) followed by Studies and Studies on Target periods,
- A series of Studies days to allow for fine-tuning of accelerator and target systems.

One goal of ESS is to ensure that at least 90% of the users receive a neutron beam allowing them to execute the full scope of their experiments. This is in accordance to the availability and reliability assessments made in ref [ESS-0017709 and ESS-0008886].

The CSPEC instrument is foreseen to be managed and operated by a team of 2 (Instrument scientists)+1 (SA) scientists and 1 technician in steady state operations. The technicians might split their time with other instruments. ESS will be manned 24 hours/day and such a model will provide flexibility for users before and during experiments in addition to time required to analyse results. Data collection, storage and analysis are provided by DMSC, physically located in Copenhagen. Currently it is foreseen that a DMSC member of staff will be an instrument team member, local contact for the users and focus on data analysis. This person must be fully integrated into the CSPEC team at frequently be on-site.

5.2 Operational scenarios

The beamtime for user experiments is allocated in a peer-review process based on scientific merit and feasibility. Proprietary access for industry is also envisaged. In order to partake in spectroscopy experiments the users will have employed bulk measurement techniques to characterize their samples.

The typical users of the CSPEC instrument are scientists, specialized in hard or soft condensed matter physics, material or biological science. The user team would typically consist of 1-4 scientists (PhD level, doctoral students and principal investigator) who perform the experiment within the allocated beamtime. Most users should be able to operate the instrument independently after a 2 hour introduction by the ESS instrument team. The less experienced users, who would require more support, would be expected to establish a collaboration with ESS scientists. Users will either bring their samples with them, ship them beforehand, or prepare them using ESS support facilities. After the experiment, the samples should be returned to the users, after clearance through radiation protection. The users will process the data at the ESS by at least up to a point where it can be input to third party software.

Outline of an experiment on a cold chopper spectrometer at the ESS.

A typical experiment at the direct geometry time-of-flight spectrometer CSPEC consists of the following steps:

Beam shaping and choice of energy resolution:

The energy resolution of the primary spectrometer is determined by the choice of the chopper rotation speed and phasing of the pulsing and the monochromating chopper pair. These parameters will be adjusted for each energy and energy resolution required. Similarly, the rotation speed and phases of the pulse removal choppers have to be set to select the time interval of the subpulses during the ESS time frame, according to the requirements of the experiment. The exchange guide (last piece of the beam transportation system) has to be chosen and moved into position to either measure with a standard extended beam, or a focussed beam. A slit system in front of the sample should adjust the beam dimensions to fit to the sample dimensions. The oscillating radial collimator will be functioning .

All of the above steps shall be executed remotely via the instrument control software that is common to all time of flight instruments. The settings shall be available as metadata for each data collection run.

Preparation and mounting of samples:

Typical samples may consist of powders, liquids, layers on a substrate, and single crystals. For most standard experiments, they are packed into a container (mostly Aluminium, but other materials might be used according to pressure / magnetic field and temperature requirements). Laboratory space close the instrument will be used for the filling and preparation of the sample containers, including access to a glovebox for moisture and air sensitive materials, a balance and a furnace.

Powder samples can be attached to the end of the sample stick and positioned inside the sample environment, at the sample position, via the sample chamber top opening. An automatic thermalized sample changer will enable up to 5 sample changes without opening the sample chamber. Single crystals samples, held by a goniometer mount, or positioned on an alignment device attached to a goniometer head, can be attached to an in-situ 6-axes remote controlled goniometer. A range of crystal mounts should be available at the instrument to meet the needs of the user.

CSPEC will accommodate standard sample environments including cryostats, dilution stages, furnaces, and magnets that can be installed from the top of the sample area tank. A variety of non-standard sample environments will be available at CSPEC to accommodate *in-situ* and *in-operando* experiments. These non-generic sample environment can employ a 6 axis goniometer stage positioned below the sample position.

It is crucial for the long-term scientific productivity of the instrument that the spectroscopy experiments are as streamlined as possible. There must be flexibility to install a wide range of standard sample environments available in the ESS sample environment pool to cover temperature, magnetic and electric fields, pressure or humidity. It will be possible to study samples in more specialised sample environments, such as gas pressurisation equipment, levitation equipment, or perform complementary measurements such as optical spectroscopy (Raman or infrared spectroscopy) or specific heat measurements on the sample during the experiment. The use of such equipment will have to be agreed well in advance with the ESS instrument team. As a general principle the user team is expected to be responsible for bringing in such special equipment and the ESS instrument team will provide support with mounting and integrating it at the instrument. For equipment developed by the ESS as part of an in-house research program the users are expected to establish a collaboration with ESS scientists.

The sample environment area can be operated under cryogenic vacuum, under ambient conditions or under gas pressure. An aluminium window will separate the detector vessel, at 10^{-6} mbar, from the higher pressures, up to 1 bar, in the sample environment area, the gate will be remotely controlled.

For the installation of the sample environment and sample changes, safe access to the sample stage is required when the accelerator is on and the two light shutters are in the closed position.

Multiple scattering shall be kept to a minimum, this implies that the transmission of the scattering must be greater than 90%. In-situ checks of the sample transmission will be possible via incident and transmitted beam monitors, after the slit component and after the sample respectively. If the beam is collimated then a monitor at the entrance of the beam stop tube will be able to provide information on the sample transmission. A test beamline will be highly beneficial to determine sample transmissions as a function of sample rotation prior to the experiment, thereby improving the resultant data analysis.

Once the sample is mounted, the control of the sample environment should be remote. The control parameters (e.g temperatures, magnetic fields) shall be monitored continuously and available as time stamped meta-data for each measurement. Event recording will be the normal mode of operation.

Depending of the type of sample and the experimental questions, the frequency of sample changes might be as often as one sample change every 15 minutes and this will require an automatic sample changer.

Data collection runs

A single measurement consists of the registration of the scattered neutrons as function of (uniquely identified) detector voxel and arrival time at that position, for the duration of a preset time or a preset number of ESS source pulses. Data recording in event mode shall be standard. Typically, one sample is measured at different settings of the control parameter, e.g. at different temperatures, magnetic fields, orientations or at different energy resolutions. The instrument control software shall allow the change of these parameters to be included in an automated measurement script that should be easily modified during the experiment. The samples will be rotated to provide a fully consistent $S(\mathbf{Q},\omega)$ map in the case of highly textured samples and in the case of single crystals. The length of time that the samples are illuminated depends on the scattering strength of the sample constituents and the chosen instrument settings, the central wavelength and the energy resolution.

Besides the sample (+ container) run, each data collection run shall be complemented by (a) an empty container run and cadmium samples for background substraction (at correct temperatures) and transmission purposes and (b) a vanadium calibration run at identical instrument settings to determine detector efficiencies and absolute scattering cross sections.

Data processing

Four dimensional energy/reciprocal space maps, $S(\mathbf{Q},\omega)$, will be generated in the case of single crystal measurements while 2 dimensional energy/reciprocal space maps $S(Q, \omega)$ will be provided for the case of non-crystalline or powdered materials. For each detector voxel and registered neutron, the energy transfer to the sample is calculated from the neutron velocity after scattering, i.e. via the time-of-flight needed to cover the known sample-to-detector distance. The neutron energy of the incoming pulses is known from the chopper parameters, and the time-of-flight of the elastically scattered neutrons can be either taken from geometry or determined from the vanadium calibration runs. During the data collection runs, data processing should allow the on-line display in the appropriate form $S(\mathbf{Q},\omega)$ to check and monitor the running experiment.

As previously stated the amount of data gathered on a chopper spectrometer at the ESS will exceed the data on todays instruments by one to two orders of magnitude. It is thus

essential that data visualization and analysis tools must be fast enough to make decisions while running the experiment. The tools must be ready to handle large complex data sets both during the experiment (on-line) and for the final data analysis.
It is imperative that there is a close collaboration between the instrument team, users, DMSC and theory groups. Theoretical expectation of the scattering must be available to compare data with expectation. Data processing requires software tools to perform profile fitting, scaling and comparison to basic models (e.g.SpinW, DFT, molecular dynamics). ESS scientists will support specific data processing and non-standard software (available at DMSC and with the DMSC instrument scientist) necessary to visualize and analyse data. The success or failure of the chopper spectrometers will depend on the ability of the user to extract data in a timely manner and to understand the results.

Sample handling.

After the experiment the sample will be stored according to the safety and radiation requirements. There will be some space provided on the instrument for sample storage.

5.3 Maintenance philosophy

CSPEC's maintenance philosophy aims to utilize condition based preventive maintenance as much as possible. In order to minimize time spent and increase efficiency when performing maintenance, accessibility is a requirement that requires a good deal of attention in the design work.

In general, access to instrument equipment along the beam guide shall be from the top, especially in the bunker region. In this area the aim is to utilize remotely operated vehicles to do the maintenance work, to the greatest possible extent. Further downstream, as the allocated beam line sector widens, more space will be available facilitating access from the sides for inspection and maintenance.

In the following a brief outline of the CSPEC components and the foreseen monitoring is given:

Guide and beam conditioning system:

(i) Operational parameters recorded
  a. Pressure in vacuum guide housing
  b. Regular checks of transported beam intensity (incident beam monitor)
  c. Focussing guide configuration
  d. Beam aperture configuration
(ii) Regular maintenance required for
  a. Vacuum pumps and gauges
  b. Guide alignment: beam monitor at dedicated locations along the guide

Regular maintenance will be done during shut down periods. Realignment of guide sections requires removal of shielding blocks and (optical) access to the laser-tracking reference points. Maintenance and repairs of the focussing guide lift system requires access to the sample area as part of the detector tank.

Chopper system

(i) Operational parameters recorded for each chopper axis include:
  a. Cooling water temperature
  b. Cooling water flux
  c. Vacuum (Pressure, Vaccum pump on/off)
  d. Status of the magnetic bearing
  e. Vibration
  f. Rotation speed
  g. Temperature of the disks

(ii) Regular maintenance required for
  a. Vacuum pumps and gauges
  b. Cooling water circuit (filters etc.)

Preventive maintenance of each chopper axis can be done during regular shut-down periods. Chopper maintenance and repairs that require access to the chopper axis/disk will be possible since all choppers will be housed in large shielding housing with direct access (door) This provides a two fold advantage. First, visual and direct access to the choppers will limit down time and help in the commissioning phase. Second, large shielding housing around the choppers will provide secondary scattering opportunities for high-energy neutrons that will thereafter not continue their trajectories down the guide. CSPEC has no fast rotating disk choppers up to 100 m from the moderator.

Sample Environment:

Sample environment can always be removed from the beamline and all maintenance and repair is performed in dedicated workshops.

Detector tank:

(i) Monitoring includes:
  a. Vacuum (Pressure)
  b. Positioning and movement of radial collimator

(ii) Regular Maintenance:
  a. Pumps and pressure gauges

Detectors:

The regular vanadium calibration runs allow for a continuous monitoring of the performance. Maintenance will need access to the detector tank inside the experimental cave and will be done by ESS detector group.

6. CONSEQUENCES OF THE CONCEPTS

6.1 General design considerations

6.1.1 Upgrade options

The scope setting meeting for CSPEC allocated 16.5 M€ from preliminary design, phase 1, to installation and cold commissioning, phase 4. The preliminary design phase, phase 1, has focussed on budget realities within the constraints of the science case presented in the STAP and SAC report of 2014.

Costing of the components has been in close collaboration with companies providing optics, shielding, chopper, detector tank and detector components. Prices are outlined in the budget document and presented in Figure 3. A chopper spectrometer does not have a great number of features that can be discarded. All components in the primary spectrometer are required for a functioning instrument. Some secondary spectrometer components may be considered for staging plans. The upgrade path for CSPEC include

Detector bank completion.

Sample environment.

Polarisation analysis.

T0 chopper (if required).

6.1.2 Robust design

Due to the hostile environment along the entire beamline, in particular inside the target monolith insert and the common shielding bunker area, design solutions should be made as robust as possible. Robust should be regarded in terms of e.g. minimizing number of components, moving parts (reducing maintenance efforts) and maximizing structural strength. Robust design solutions should also support the ability, where possible, to enable a degraded performance mode in case a failure or an unintentional misalignment occurs. Robust design applicability could include:

- Optics in the extraction system
- Monolith light shutter - position repeatability and optics
- Neutron guide – mounting arrangement, components misalignment
- Chopper design solutions

Mitigating measures elsewhere along the beamline should be investigated should some of the issues/problems above occur.

6.1.3 Coordination with other systems

Close monitoring and continuous coordination with the following interfacing systems is critical:

- CSPEC, BIFROST and TREX all have a great interest in the procurement of a high field magnet. Significant collaboration is envisaged.
- TREX and CSPEC may have the same detector technology. This has implications for the detector electronics and the detector vessel.
- Sample environments. Although slightly different in concept both TREX and CSPEC would like to be able to bring the sample space up to vacuum without evacuating the entire detector vessel. Significant collaboration is expected.
- Neighbouring beamlines, BIFROST and BEER – especially the first 30 m from target center. Compromises cannot be ruled out possibly affecting design and performance of the CSPEC instrument. This should be kept in mind and possible scenarios of how to mitigate such compromises should be considered. Outside the bunker space monitoring of allocated space is mainly required for upstream chopper locations and various expected maintenance activities.
- Target monolith insert – optics alignment, cooling solution, The insert is provided by Target System to NSS design specification.
- Light shutter – optics alignment, position repeatability and beam guide gap. The light shutter is provided by Target System to NSS design specification
- Bunker system – alignment components in the bunker, optics insert in bunker wall. The bunker is provided centrally by NSS based on requirements from the instruments.

7. PRELIMINARY BUDGETS

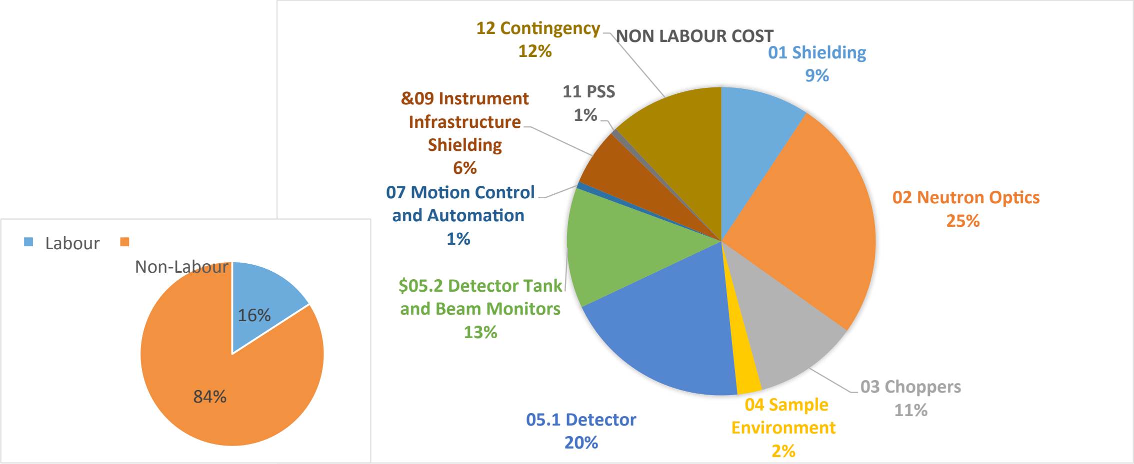
A budget has been generated and agreed with ESS management as part of the scope setting meeting. The budget covers phase 1 - 4 and includes all of the main components outlined in this document. Manpower required for the 4 phases is included. The costing is based on a bottom-up calculation of the procurement costs and manpower required for the tasks needed to deliver the higher-level PBS items. Vacuum equipment and data management requirements are not included in the cost as this is expected to be delivered from outside the CSPEC budget.

Components have been costed with the help of the manufacturers to provide realistic quotes.

Table 3: Costing devised for the CSPEC Scope Setting meeting. Preliminary world class configuration with no VAT on components, prices in k€. The functioning detector coverage on day 1 is 50%.

	01 Preliminary Design (k€)	02 Engineering Design (k€)	03 Procurement & Start of Installation (k€)	04 Installation and Start of Cold Commissioning (k€)	Total (k€)
01 Shielding	0	0	1129	0	1129
02 Neutron Optics	0	0	3097	99	3196
03 Choppers	0	0	1480	0	1480
04 Sample Environment	0	0	375	0	375
05 Detector (B10)	0	300	4979	0	5279
05.1 Detector set (33m²)	0	0	3853	0	3853
05.2 Detector Tank and Beam Monitors	0	300	1126	0	1426
06 Data Acquisition and Analysis	0	0	0	0	0
07 Motion Control and Automation	0	48	33	19	101
08 Instrument Team	484	937	528	375	2323
09 Instrument Infrastructure (Cave and Shielding)	0	0	867	0	867
10 Vacuum	0	0	0	0	0
11 PSS	0	33	33	33	100
12 Contingency	0	0	0	0	1650
Total	**484**	**1318**	**12521**	**527**	**16501**

Figure 15: Relative costs contributing to CSPEC. (left) Labour to non-labour costs (right) non-labour costs. From the CSPEC Scope Setting Meeting.



An updated risk analysis has been performed and can be found in the “Work Package Specifications.”

8. LIFE CYCLE OF THE CSPEC INSTRUMENT.

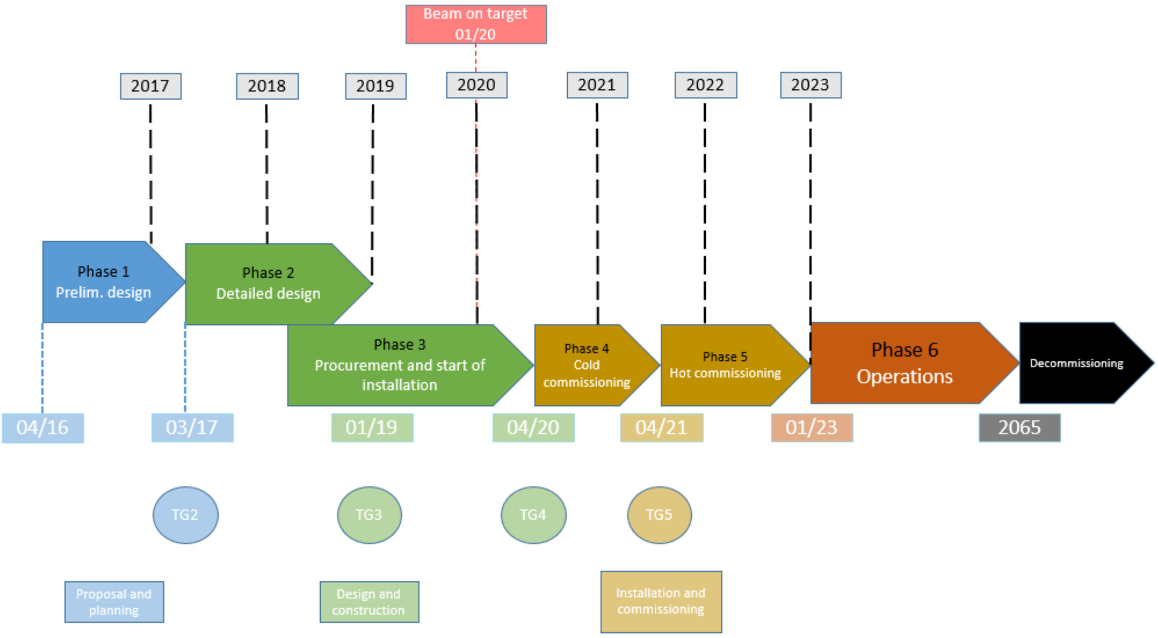


Figure 16: Timeline derived from the Work Breakdown Structure (WBS) of CSPEC.

In order for the timeline to remain current it is imperative that the CSPEC are able to start the procurement process within phase 2.

9. GLOSSARY

Term	Definition
BW	Bandwidth Chopper
RRM	Repetition Rate Multiplication
ConOps	Concepts of Operations
FOC	Frame Overlap Chopper
IRR	Installation Readiness Review
ORR	Operational Readiness Review
PDR	Preliminary Design Review
PPSC	Prompt Pulse Suppression Chopper
PSC	Pulse Shaping Chopper
PSS	Personnel Safety System
SAR	Safety System Acceptance Review
TG	Toll gate

10. REFERENCES

[1] Process for Neutron Instrument Design and Construction: ESS-0051706
[2] Concepts of Operations for the ESS system: ESS-0003640
[3] Concepts of Operations for the NSS system: ESS-0005817

DOCUMENT REVISION HISTORY

Revision	Reason for and description of change	Author	Date
1	First issue	Pascale Deen	2016-08-30